## Dratile iron pipe systems CATALOGUE

## Our company

## TRM develops, manufactures and markets highquality systems for the transport of water and for deep foundation of structures - made of ductile iron.

We see ourselves as a Tyrolean manufacturer with a long-standing tradition specializing in pipe and pile systems made of ductile iron for the water industry and for deep foundation engineering. We operate worldwide and have our core market in Europe. Since 1947, we have focused our activities on quality, safety, mutual trust and respect.

We see ourselves as a reliable and competent partner in a wide range of applications within our industry; a view that is shared by our partners.

Our products are high-performance, sustainable and robust. They stand out particularly due to their ecological and economical benefits. The features of ductile iron and our expertise in all fields of applications enable us to overcome even extreme challenges.

The sustainable properties of ductile iron combined with innovative technologies and professional expertise in all fields of application make us a leading partner in the water industry and deep foundation.

Due to our high competence, willingness and reliability, we are a powerful and long-term system partner.

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Products:
Pipes according to EN 545 and EN 598 of nominal sizes from DN 80 to DN 1.000 and piles


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## 1 - ADVANTAGES OF DUCTILE IRON PIPE SYSTEMS



## Production

Only the highest quality raw materials are used for making TRM ductile iron piping. Scrap iron and steel are used exclusively to produce the pig iron. Ductile iron piping is particularly sustainable, economically efficient and environmentally friendly as it is made using recycled material, has an extremely long service life and is almost fully recyclable.

The used scrap metal is smelted together with coke and other aggregates in a cupola and then treated with magnesium. The chemical composition and the mechanical properties of the pig iron and the treated iron are checked at specific, frequent intervals.

After treatment with magnesium, the ductile iron is cast into "cast iron pipe blanks" in various centrifugal casting machines using the "De Lavaud" process. To form the internal contours of the sockets, a sand core is used in the centrifugal casting mold, which varies depending on the type of connection. The pipes are then annealed at around $960^{\circ} \mathrm{C}$, which finally gives them their ductile properties. When the annealed pipes are tested, it must be ensured that the characteristics of the material comply with EN 545 (for drinking water pipes) and EN 598 (for sewage pipes).

The cleaning and test area is connected to the annealing furnace. This is where the pipes get their zinc or zinc and aluminum coating, are examined in meticulous detail and are individually checked for any leaks by means of a pressure test. Material samples are taken at regular intervals and checked to make sure that they comply with the specified parameters. The process continues with weld bead being applied to pipes with a VRS ${ }^{\oplus}-\mathrm{T}$ connection.

Cement mortar lining
A cement mortar lining is added to every pipe. This is carried out in accordance with ÖNORM B 2562. The lining is subject to rigorous quality controls - as well as checking the source materials and the fresh mortar, the stipulated thickness must be observed, depending on the nominal width.

## Outer coating

The standard external coating consists of a PUR coating, or a finishing layer of epoxy. Alternatively, however, a cement mortar coating (ZMU) can be applied to the zinc-coated pipe. Pipes with this ZMU coating can subsequently be used in soils with grain sizes of up to 100 mm or in soils of any level of corrosiveness, or can be used for trenchless installation. A further benefit of the ZMU is that it extends the expected technical service life to up to 140 years.

In the final part of the production process, markings are applied, caps are fitted to drinking water pipes, the pipes are bundled, and a final quality control is carried out. The parallel, curved grooves some 3 mm deep in the front of the socket further identify the material as "ductile iron".

Manufacturing a high quality product and achieving customer satisfaction are TRM's main corporate goals. We operate a quality management system which is certified according to EN ISO 9001. The products and production processes are monitored by the inspection, monitoring and certification body in Vienna (MA 39).


## Certificates

Naturally, all TRM products are certified for the supply of drinking water by the Austrian Association for Gas and Water (ÖVGW). All the materials used by us in the manufacturing process that will subsequently come into contact with drinking water, such as the antiseize agents, gaskets and cement mortar, have been tested in accordance with the relevant guidelines or have been approved under ÖNORM B5014 part 1, or KTW UBA. The possibility of the quality of drinking water being adversely affected can therefore be ruled out. Our ductile iron pipes with VRS ${ }^{\circledR}$-T plug-in socket connections, in nominal sizes DN 80 to DN 500, also have FM approval, which means that these pipes can be used for fire extinguishing systems.

Our fittings are coated internally and externally with an epoxy finishing layer according to EN 14 901. This coating also meets the stringent requirements laid down by the Quality Association for Heavy Duty Corrosion Protection (Gütegemeinschaft Schwerer Korrosionsschutz, GSK). This means that our fittings that are certified according to EN 545 can be installed in soils of any corrosivity. A selection of the most important certificates is available for download at www.trm.at.

Texts for use in invitations to tender
Texts for use in invitations to tender conforming to the current EN 545 for pipes and fittings are available to download at www.trm.at in a variety of formats (Word, PDF and GAEB).


## Materials

The first known ductile iron pipes were used in 1455 to supply water to the castle of Dillenburg and they remained in operation for more than 300 years. Over the course of the following centuries, the development of ductile iron as a material continued in line with the increasing demands being placed upon it. Since the 1960s, pipes have no longer been made of the previously traditional grey ductile iron (GG), but have instead been constructed from ductile iron (GJS, formerly GGG). The word "ductile" comes from the Latin verb ducere (= to lead or reshape) and means able to be stretched or shaped into a new form. This highlights one of the key properties of ductile cast iron piping: its ability to be deformed under load and thus withstandvery high stresses caused by traffic or internal pressure, for example.

Ductile iron is a tough iron-carbon material in which the carbon content exists predominantly as graphite in a free form. The main difference between grey ductile iron and ductile iron is the shape of the graphite particles. Treatment of the molten iron with magnesiumcauses the carbon to crystallize in a largely spheroidal form as solidification takes place. This results in a considerable increase in strength and malleability compared with grey ductile iron. The so-called spheroids of graphite have only a minor effect on the properties of the microstructure of the metal. In the formerly used grey ductile iron, the graphite lamellae decreased the relatively high strength of the microstructure because of its notch effect.

Whereas in ductile iron with lamellar graphite the stress lines become highly concentrated at the tips of the graphite lamellae, in ductile iron they flow round the graphite which has separated out in spheroidal form almost undisrupted. This is why ductile iron is able to deform under load. In static terms, ductile iron pipes and fittings are considered to be flexible pipes.

Characteristics of the material
In accordance with EN 545, tensile strength and elongation after rupture can be tested on test bars.

The table below provides an overview of the characteristics of ductile iron:

| Characteristic values | Units | Value |
| :---: | :---: | :---: |
| Tensile strength | $\mathrm{N} / \mathrm{mm}^{2}$ | 420 |
| $0.2 \%$ proof stress | $\mathrm{N} / \mathrm{mm}^{2}$ | 300 |
| Elongation after rupture | $\%$ | $\geq 10$ |
| Compressive strength | $\mathrm{N} / \mathrm{mm}^{2}$ | 900 |
| Modulus of elasticity | $\mathrm{N} / \mathrm{mm}^{2}$ | 170.000 |
| Bursting strength | $\mathrm{N} / \mathrm{mm}^{2}$ | 300 |
| Compressive strength at crown | $\mathrm{N} / \mathrm{mm}^{2}$ | 550 |
| Longitudinal bending stiffness | $\mathrm{N} / \mathrm{mm}^{2}$ | 420 |
| Oscillation bandwidth | $\mathrm{N} / \mathrm{mm}^{2}$ | 135 |
| Mean coefficient of thermal expansion | $\mathrm{m} / \mathrm{mK}^{2}$ | $10 \times 10-6$ |
| Thermal conductivity | $\mathrm{W} / \mathrm{cmK}^{\mathrm{JmK}}$ | 0,42 |
| Specific heat | $\mathrm{J} / \mathrm{gK}$ | 0,55 |

The mechanical properties of a metallic material like ductile iron are maintained for the whole of its service life. That is why ductile cast iron pipes are still able to withstand loads and remain safe even after decades of use.

## Made in Austria

The expertise for our ductile iron pipe systems comes from Hall in Tyrol. The majority of our products are also manufactured at our production site in Hall. This ensures consistently high quality and short distances and times for delivery, while also safeguarding jobs in Austria.


Path followed by the stress lines in with spheroidal graphite (right) ductile iron with lamellar graphite (left)

Bound by tradition
We have been producing ductile iron piping since 1947. Over the years and the decades, the production processes, the types of internal and external protection for the pipes, and the connection systems have been developed and refined to an ever higher standard. Today we can look back on our many years of experience and invest our knowledge in the ongoing development of products for the benefit of our customers.

## Service

Our company headquarters are located in the heart of Europe, which not only enables us to keep the distances for transport short, but also ensures that our applications engineers and field sales staff can be at your service promptly to provide advice and assistance throughout the sales area. We have an experienced team of technicians, engineers and salesmen ready to support you with help and advice.

## Hygiene

One of the primary tasks of our civilization is always to get water reliably to its destination. For generations, our ductile iron pipes have set the standard for quality in water supply. Water is the most important natural resource on our planet and for this reason it has to be protected against contamination and the effects of chemicals while it is being transported through pipelines.

Our ductile iron pipes are provided as standard with a cement mortar lining. Pipelines almost 100 years old lined with cement mortar have shown that as a mineral lining cement mortar is superior for working life and effectiveness to all the other materials which have been used to date. The cement mortar lining has both an active and a passive protective action. The active action is based on an electrochemical process. Water penetrates into the pores of the cement mortar
and dissolves free lime and this raises its pH to a level of more than 12. With a pH of this level, it is impossible for ductile iron to corrode. The passive action results from the physical separation which exists between the pipe's ductile iron wall and the water.

The cement mortar lining consists of a mixture of sand, cement and water which is introduced into the pipe as the latter rotates and which is then flung against the internal surface of the pipe by centrifugal force. The centrifuging process powerfully drives out the water mechanically and compacts the cement mortar (water/cement ratio > 0.35:1). What this gives is firstly high strength for the cured cement and secondly extremely high resistance to any possible corrosive attack by water as a medium. For drinking water supply, the cement used is principally blast furnace cement or Portland cement. High-alumina cement is used for sewage disposal.

## Diffusion seal

Ductile iron pipes are sealed - and in more than one way. As an inorganic material, the ductile iron of the pipe wall is impervious to diffusion. This means that nothing can penetrate through the pipe wall from the inside outwards or vice versa. For the ductile iron piping, this means that no pollutants can find their way into the drinking water, which is important, especially when pipes are laid in contaminated soils.

Resistant to root penetration
The connection is proven to prevent plant roots from penetrating the ductile iron pipe, which is a frequent problem with other types of connections, over several decades.

One pipe - many possibilities
Our ductile iron pipes have a variety of uses.

## Typical areas of application of the $\mathrm{VRS}^{\oplus}-\mathrm{T}$ system include:

- Supply of drinking water
- Disposal of sewage
- Snow-making systems
- Turbine pipelines
- Fire-extinguishing pipelines (FM and German Federal Railways approved)
- Replacement of concrete thrust blocks during conventional laying techniques
- Bridge pipelines/above-ground pipelines
- Temporary pipelines (for a temporary water supply)
- Trenchless installation techniques (HDD, burst lining, press-pull technique, pipe relining, floating-in etc.)
- Laying on steep slopes
- Use in regions at risk of earthquakes or settlement
- Water crossings/culvert pipelines
- Building installations


## Complete system engineering

In addition to our pipes, we have an extensive range of fittings for use with $\mathrm{VRS}^{\circledR}-T$ connections and TYTON ${ }^{\oplus}$ connections. Almost all the fittings available are listed in this catalog and others are available on request. All our fittings are produced specifically for us by prestigious German foundries.

Over mountains and through valleys - pipeline stability Thanks to their long overall length of 5 to 6 m , ductile iron pipes are largely unaffected by changes in position caused by settlement or by an uneven supporting layer. Because of their high longitudinal bending stiffness, pipes are able to bridge faults in the supporting layer without being overloaded and suffering damage as a result.

Furthermore, depending on the nominal width and the type of connection, our plug-in socket connections can be bent to angles of up to $5^{\circ}$. For a 6-meter-long pipe, for example, this is equal to a deflection of about 50 cm from the axis of the socket of the previous pipe or fitting. This means that even extensive settlement cannot impair the impermeability of the system and no unwanted restraints are passed on from one pipe to the next.

In the event of settlements, landslides or earthquakes and, therefore, changes in the length of the pipeline, the VRS ${ }^{\oplus}-\mathrm{T}$ connection also safeguards pipes and fittings against longitudinal forces and stops them from being pulled apart.

Not to be underestimated - structural safety/laying on
cradles carried on piles
Ductile iron pipes are equal to almost any load. For example, given the right nominal size, wall thickness and conditions of installation, our pipes can be laid with only 30 cm of cover and withstand a traffic load conforming to the SLW 60 load model (heavy goods vehicle applying a total load of 600 kN ). This is achieved thanks to the high diametrical stiffness and longitudinal bending stiffness.

It is also possible to vary the wall thickness in cases where there are elevated stress levels due to traffic, top cover, internal pressure, etc. In static terms, ductile iron pipes can be considered a flexible system. Evidence of their serviceability can be obtained from the allowable deformation or stresses and from the checks made on fatigue strength. Our application engineering unit therefore offer verifiable pipe stress analyses. Nor are there usually any stress-related problems with laying pipelines on cradles carried on piles. Because of the high loadbearing capacity of the pipes, in many cases only one cradle per pipe is required.

## Safety margins

When it is a question of supplying our most precious commodity, drinking water, safety should be a primary concern. All of our pipes, without exception, are therefore tested for leaktightness at our production site. Ductile iron pipes have triple protection against internal pressure.

## Sustainability

Ductile iron pipes have been laid for more than 550 years for the purpose of transporting liquids. Even back in the early days, the potential of this material was recognized. Outstanding standards of performance have been achieved thanks to the constant ongoing development of the production processes, the material itself and the joining techniques used.

The long life of the ductile iron pipes takes the strain off future renovation budgets, and the very low damage rates also help to cut operating and maintenance costs. Experience from the past six centuries bears witness to the extremely long technical service life offered by ductile iron pipe systems.

## Economical

To assess the economic efficiency of pipeline systems, more than just the price of the pipe material has to be taken into account. The costs of installation, the damage rate and the technical service life must also be considered.

Ductile iron pipes are well known for the quick and easy way in which they can be laid and for how forgiving they are of mistakes in the laying. Our VRS ${ }^{\oplus}-$ T and TYTON ${ }^{\star}$ connecting systems can be assembled extremely quickly without the need for any expensive special tools. Most only require a square timber crowbar or an excavator, and costly and periodic training or certification is not necessary. The following formula is a simple way of estimating the average annual cost of a pipeline in euros per meter.
$\emptyset K=I_{*}(1 / n+p / 200)$
ØK = average annual cost of the pipeline in EUR/m
I = investment costs (cost of production) in EUR/m
$n=$ technical service life in years
$p=$ interest in\%

Using this formula, it is very easy to see that the average annual cost of a pipeline depends principally on its technical service life. Consequently, high production costs due to the use of high grade materials for the pipeline are therefore perfectly economical when viewed across the entire lifetime. And this is true even before allowing for the advantages offered by ductile iron pipes in terms of operating and damage-related costs.

Environmentally friendly
TRM ductile iron pipes are a model of environmental performance.
This is primarily due to four factors:

1. We use only scrap steel and iron - i.e. recycled material - to produce the molten pig iron. This not only saves valuable iron ore resources but also saves energy. Unlike crude oil, there is still an infinite supply of scrap metal.
2. Because ductile iron pipes consist essentially of iron and cement mortar, they are almost fully recyclable.
3. The main waste products generated in our production, such as slag and sand, are used and recycled in cement works and in road building.
4. Ductile iron pipe systems have an extremely long technical service life of up to 140 years. Calculated over their life span, this minimizes the $\mathrm{CO}_{2}$ and other emissions released during production.

## Quality

Manufacturing a high quality product and achieving customer satisfaction are TRM's main corporate goals. We operate a quality management system which is certified according to EN ISO 9001. The products and production processes are regularly monitored by external material testing institutions. This ensures that our products are made to a consistently high quality and creates and safeguards jobs.


## Ductile iron pipe systems are technically superior

- Corrosion resistant thanks to the inner and outer coating
- Secure external protection for all soil types and installation methods
- Linings that are resistant to aggressive media
- High static load-bearing capacity
- Break-proof
- High safety margins (with regard to pressure fluctuations, static overload and external influences)
- Patented restrained connections
- Deflection angle of up to $5^{\circ}$
- Suitable for trenchless installation
- Impermeable even when exposed to high internal pressures, negative pressure and high groundwater levels
- Pipe material with a diffusion seal
- Resistant to root penetration
- Constant material properties (long-term durability)


## Ductile iron pipe systems are economically superior

- Faster and easier, cost-effective assembly
- Narrower trenches thanks to thinner pipe walls
- Excavated material is mainly reusable
- No welding necessary (extremely simple socket connection)
- Installation in all weather conditions
- Ideal for trenchless laying
- Material resistant to ageing
- Long service life
- Complete system engineering through fittings and accessories
- Efficient and cost-effective planning with TRM application engineering
- Extremely low damage rates


## Ductile iron pipe systems - designed with the environment in mind

TRM ductile iron pipes are a model of environmental performance.
This is primarily due to four factors:

- Inorganic material
- Made of recycled iron and fully recyclable
- Satisfies the highest sanitary requirements
- The sand used for the cement mortar liningis free from binding agents and chemical additives
- Completely impermeable pipe wall
- Lifespan of up to 140 years

Environmental sustainability criteria for ductile iron pipe systems

| Diffusion seal | safeguards drinking water in all soil types and installation conditions as well as groundwater when <br> sewage is being transported |
| :--- | :--- |
| Linings | ensure hygienic and environmentally safe transport of drinking water approved to food hygiene <br> standards |
| Scrap as the raw material | minimizes the use of primary and fossil raw materials |
| Ductile iron | saves resources for present and future generations through recycling |
| Low maintenance and repair costs <br> and a long service life | minimizes the consumption of resources and reduces $\mathrm{CO}_{2}$ emissions |

Economic sustainability criteria for ductile iron pipe systems

| Plug-in sleeves make for <br> highly productive installation | reduces labor costs |
| :--- | :--- |
| No welding required | saves time and subsequent costs, e.g. waiting times and weld seam testing |
| Installation in all weathers | reduces labor costs |
| Sand bedding often not required | reduces materials, logistics and labor costs |
| Concrete thrust blocks not needed when connections are <br> restrained | reduces materials, logistics and labor costs |
| Bendable connections | reduces materials and labor costs; ensures availability in case of <br> faults or alterations |
| Wide range of fittings available <br> so custom-made designs are not required | reduces repair and maintenance costs |
| Extremely low damage rates | keeps the renovation budget to a minimum |
| Lifespan of more than 100 years |  |

## Technical sustainability criteria for ductile iron pipe systems

| Strong material | allows operating pressures of more than 100 bar |
| :--- | :--- |
| External protection | protects against mechanical and chemical attack |
| Static load-bearing capacity | allows very high stresses in the transverse and longitudinal directions |
| Connection | is resistant to root penetration which stops it becoming clogged |
| Ductile iron | is non-combustible; high operational reliability in unplanned loading conditions |
| Installation | is possible without special equipment in all climates and weather conditions |
| Restrained connections | allow very high tensile forces and are therefore ideal for trenchless installation |
| The material has superior properties | which allow special applications in mountainous regions, in areas at risk of earthquakes or settlement <br> and for fire-extinguishing pipelines and hydroelectric power stations |

## 2 - THE POSITIVE LOCKING SYSTEM

## Introduction

This chapter deals only with restrained push-injoints where the restraint is based on a positive locking interengagement. Positive locking push-injoints can always be recognised by a welded bead on the spigot end and a retaining chamber. The positive locking interengagement between the welded bead and the retaining chamber is obtained by inserting locking segments. This enables forces to be transmitted mechanically between the spigot end and the socket of the next pipe or fitting.


An example of a positive locking joint (VRS ${ }^{\circledR}-T$ joint)

Forces may be generated by internal pressure or external tractive forces. Allowable operating pressures (PFA) and allowable tractive forces are specified on the pages 71 ff as a function of nominal size. Higher pressures and tractive forces are possible; please check with our Applications Engineering Division.

## TRM supplies the following positive locking

push-in joints for pipes and fittings:

## The VRS ${ }^{\text {®-T }}$ joint (DN 80 to DN 500)

This joint has been a success for decades and can be assembled with a TYTON ${ }^{\circledR}$ or the $\mathrm{VRS}{ }^{\oplus}-\mathrm{T}$ gasket. Depending on the nominal size and the nature of the application, locking is from 2 to 4 locks. It is notable principally for its easy and quick assembly, the reliable high operating pressures and tractive forces and the versatility with which it can be used. A clamping ring can be used on cut pipes. This enables the on-site application of a welded bead to be dispensed with in most cases. Pipes with VRS ${ }^{\circledR}$-T joints are available in laying lengths of 5 m and 6 m . You will find further information on the VRS ${ }^{\oplus}$-T joint from p. 18 on.

The BLS ${ }^{\text {® }}$ joint (DN 600 to DN 1000)
In this case a TYTON ${ }^{\star}$ gasket is used. The joint is locked by 9 to 14 locking segments which are inserted through openings in the socket and which are distributed round the circumference of the pipe. Pipes with BLS joints are available in a laying length of 6 m . You will find further information on the BLS ${ }^{\oplus}$ joint from p .19 on .

## Fields of use/advantages

There are almost no limits to the versatility with which pipes and fittings with VRS ${ }^{\oplus}$-T joints can be used. The quick and easy assembly and the very high allowable operating pressures and tractive forces for which they can be relied on make them suitable for virtually any conceivable application in the laying of pressure pipelines (for water or sewage).

- urban water supply
- replacement of concrete thrust blocks in conventional open trench laying
- bridge pipelines/above-ground pipelines
- temporary pipelines (for temporary water supplies)
- trenchless installation techniques (HDD, burst lining and press-pull techniques, pipe relining, floating-in, etc.)
- snow-making systems
- turbine pipelines
- laying on steep slopes
- fire-fighting and fire-extinguishing pipelines (FM Approval)
- crossings below bodies of water/culvert pipelines
- building services
- use in regions at risk of earthquakes or settlement

The very high angular deflectability of up to a maximum of $5^{\circ}$ and the rotatability through $360^{\circ}$ make these joints suitable even for the laying of complicated and demanding intersections.

## PFA

Under EN 545, the allowable operating pressures (PFA) of the VRS®-T joints have to be stated in manufacturers' catalogues. See the following pages.

PMA $=1.2 \times$ PFA (allowable maximum operating pressure for a short period, e.g. the period of a pressure surge).
PEA $=1.2 \times$ PFA +5 (allowable site test pressure).

The classification into C classes under EN 545 does not apply to positive locking joints. The minimum wall thicknesses therefore differ from those in Table 17 of EN 545 (which applies to non-restrained joints).

## Compatibility

There is no compatibility with the positive locking systems used by other manufacturers. For possible solutions in this regard, please get in touch with our Applications Engineering Division.

E-mail address: anwendungstechnik@trm.at

## Clamping ring

The use of clamping rings is possible in the majority of cases on pipes of nominal sizes from DN 80 to DN 500. For details of the fields of use of the rings see p. 17 and for installation instructions see p. 72 on. By using clamping rings it is possible to dispense with the retrospective application of welded beads to pipes which are cut on site.

### 2.1 Positive locking joints and pipes

Overview


| DN | PFA ${ }^{1}$ [bar] | Allowable tractive <br> force $^{3)}[\mathrm{kN}]$ | Max. angular <br> deflection [^$]$ |
| :---: | :---: | :---: | :---: |
| $80^{2)}$ | 100 | 115 | 5 |
| $100^{2)}$ | 75 | 150 | 5 |
| $125^{2)}$ | 63 | 225 | 5 |
| $150^{2)}$ | 63 | 240 | 5 |
| 200 | 42 | 350 | 4 |
| 250 | 40 | 375 | 4 |
| 300 | 40 | 380 | 4 |
| 400 | 30 | 650 | 3 |
| 500 | 30 | 860 | 3 |
| 600 | 32 | 1,525 | 2 |
| 700 | 25 | 1,650 | 1.5 |
| 800 | $16 / 25^{2)}$ | 1,460 | 1.5 |
| 900 | $16 / 25^{2)}$ | 1,845 | 1.5 |
| 1,000 | $10 / 25^{2)}$ | 1,560 | 1.5 |

${ }^{1}$ ) PFA: allowable operating pressure - also applies to clamping rings; $\mathrm{PMA}=1.2 \times$ PFA; PEA $=1.2 \times$ PFA $+5-$ higher PFA's on enquiry. ${ }^{2}$ Wall-thickness class K10 under EN 545:2006.
${ }^{3)}$ DN 80 to DN 250 with high-pressure lock - higher tractive forces on enquiry

| VRS $^{\ominus}-$ T joint | VRS ${ }^{\ominus}-$ T joint with clamping ring |
| :--- | :--- |
| DN 80 to DN 500 | DN 80 to DN 500 |
|  |  |



Notes on the use of VRS ${ }^{-}$-T joints

- trenchless installation of DN 80 to DN 250 size pipes only with high-pressure lock
- for installation instructions see p. 71
- higher pressures are possible, e. g. for snow-making systems or turbine pipelines

Retaining chamber
Clamping ring TYTON ${ }^{\text {® }}$ - or VRS $^{\circledR}$ - - gasket


Notes on the use of clamping rings

- as a replacement for the welded bead, e.g. on pipes cut on site
- up to PFA of 16 bars in double socket bends, socket spigot-bends, $90^{\circ}$ flange socket duckfoot bends and $90^{\circ}$ duckfoot bends with side outlets; higher PFA's on enquiry
- not in above-ground pipelines or buried pipelines subject to pulsating pressures
- not in trenchless installation techniques
- tightening torque of bolts $\geq 60 \mathrm{Nm}$
- for installation instructions see p. 72

|  | Dimensions ${ }^{\text {n }}$ [mm] |  |  |  |  |  |  | Weight[kg] |  |  |  | PFA ${ }^{2}$ [bar] |  |  | Number of locks ${ }^{3)}$ | $\begin{aligned} & \text { Allowable } \\ & \text { tractive } \\ & \text { force }{ }^{4)}[\mathrm{kN}] \end{aligned}$ | Max. angular deflection [•] | $\begin{aligned} & \text { Min. } \\ & \text { radius }{ }^{\text {s) }} \\ & {[\mathrm{m}]} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DN |  | 1 | D | t | L | ${ }_{\text {a }}$ | b | Set of locks | $\begin{gathered} \text { High } \\ \text { pressure } \\ \text { lock } \end{gathered}$ | Clamping ring | Gasket | Without high pressure lock | With high pressure lock | Clamping ring |  |  |  |  |
| 80 | 98 | $\begin{array}{\|c\|} \hline+1 \\ \hline-2.7 \end{array}$ | 156 | 127 | 86 | 8 | 5 | 0.4 | 0.3 | 0.9 | 0.13 | 100 | 110 | 45 | 2 | 115 | 5 | 57/69 |
| 100 | 118 | $\begin{array}{\|c\|} \hline+1 \\ \hline-2.8 \\ \hline \end{array}$ | 182 | 135 | 91 | 8 | 5 | 0.4 | 0.4 | 1.0 | 0.16 | 75 | 100 | 45 | 2 | 150 | 5 | 57/69 |
| 125 | 144 | $\begin{array}{\|c\|} \hline+1 \\ \hline-2.8 \\ \hline \end{array}$ | 206 | 143 | 96 | 8 | 5 | 0.6 | 0.5 | 1.4 | 0.19 | 63 | 100 | 45 | 2 | 225 | 5 | 57/69 |
| 150 | 170 | $\begin{array}{\|c\|} \hline+1 \\ \hline-2.9 \\ \hline \end{array}$ | 239 | 150 | 101 | 8 | 5 | 0.8 | 0.6 | 1.7 | 0.22 | 63 | 75 | 45 | 2 | 240 | 5 | 57/69 |
| 200 | 222 | $\begin{aligned} & +1 \\ & \hline-3 \\ & \hline \end{aligned}$ | 293 | 160 | 106 | 9 | 5.5 | 1.1 | 0.8 | 2.2 | 0.37 | 42 | 63 | 45 | 2 | 350 | 4 | 72/86 |
| 250 | 274 | $\begin{gathered} \hline+1 \\ \hline-3.1 \end{gathered}$ | 357 | 165 | 106 | 9 | 5.5 | 1.5 | 1.2 | 2.7 | 0.48 | 40 | 44 | 45 | 2 | 375 | 4 | 72/86 |
| 300 | 326 | $\begin{array}{\|c\|} \hline+1 \\ \hline-3.3 \\ \hline \end{array}$ | 410 | 170 | 106 | 9 | 5.5 | 2.7 | - | 3.6 | 0.67 | 40 | - | 30 | 4 | 380 | 4 | 72/86 |
| 400 | 429 | $\begin{array}{\|c\|} \hline+1 \\ \hline-3.5 \\ \hline \end{array}$ | 521 | 190 | 115 | 10 | 6 | 4.4 | - | 6.0 | 1.1 | 30 | - | 30 | 4 | 650 | 3 | 95/115 |
| 500 | 532 | $\begin{array}{\|c\|} \hline+1 \\ \hline-3.8 \\ \hline \end{array}$ | 636 | 200 | 120 | 10 | 6 | 5.5 | - | 7.2 | 1.6 | 30 | - | 30 | 4 | 860 | 3 | 95/115 |

[^0]
## VRS ${ }^{\oplus}$-T pipe

## DN 80 to DN 500



Laying length of 5 m .

## External coatings

- Zinc coating with PUR-longlife polyurethane finishing layer
- Zinc coating with PUR-TOP Enhanced polyurethane finishing layer plus PE-tape

WKG insulation

- Other coatings up on request

Internal coatings

- Portland cement
- High-alumina cement
- Other coatings up on request

For notes on the fields of use of coatings see chapter 5


Laying length of 6 m .
External coatings

- Cement mortar coating (ZMU)
- Zinc coating with finishing layer
- Zinc-aluminium coating with finishing layer (Zinc PLUS coating)
- WKG insulation
- ZMU PLUS cement mortar coating

Internal coatings

- Blast furnace cement
- High-alumina cement

For notes on the fields of use of the coatings see chapter 5

|  | Dimensions [mm] ${ }^{\text {4) }}$ |  |  | Total weight [kg] |  | PFA ${ }^{10}$ [bar] |  |  | Number of locks ${ }^{5}$ ) | Allowable tractive force ${ }^{6}$ [kN] | Max. angular deflection [$\left.{ }^{\circ}\right]$ | $\begin{aligned} & \text { Min. } \\ & \text { radius }^{7} \text { [m] } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DN | $S_{1}$ <br> Ductile iron | $\mathrm{S}_{2}$ Cement mortar lining | Cement mortar coating | per mpipe ${ }^{2)}$ | permpipe + cement mortar coating ${ }^{3)}$ | Without high-pressure lock | With high-pressure lock | Clamping ring ${ }^{\text {a }}$ |  |  |  |  |
| 80 | 4.7 | 4 | 5 | 16.3 | 19.4 | 100 | 110 | 45 | 2 | 115 | 5 | 57/69 |
| 100 | 4.7 | 4 | 5 | 20.0 | 24.0 | 75 | 100 | 45 | 2 | 150 | 5 | 57/69 |
| 125 | 4.8 | 4 | 5 | 25.6 | 30.7 | 63 | 100 | 45 | 2 | 225 | 5 | 57/69 |
| 150 | 5.0 | 4 | 5 | 31.4 | 37.5 | 63 | 75 | 45 | 2 | 240 | 5 | 57/69 |
| 200 | 4.8 | 4 | 5 | 40.9 | 48.5 | 42 | 63 | 45 | 2 | 350 | 4 | 72/86 |
| 250 | 5.2 | 4 | 5 | 54.0 | 63.7 | 40 | 44 | 45 | 2 | 375 | 4 | 72/86 |
| 300 | 5.6 | 4 | 5 | 73.9 | 81.3 | 40 | - | 30 | 4 | 380 | 4 | 72/86 |
| 400 | 6.4 | 5 | 5 | 104.0 | 117.8 | 30 | - | 30 | 4 | 650 | 3 | 95/115 |
| 500 | 7.2 | 5 | 5 | 142.4 | 156.8 | 30 | - | 30 | 4 | 860 | 3 | 95/115 |

${ }^{10}$ PFA: allowable operating pressure; PMA $=1.2 \times$ PFA; PEA $=1.2 \times$ PFA +5 - higher PFA's on $\quad{ }^{5}$ ) Plus high-pressure lock if required with DN 80 to DN 250 sizes, ${ }^{6)}$ Higher tractive forces on enquiry, ${ }^{7}$ ) Min. radius of curves enquiry, ${ }^{2}$ ) Theoretical weight per mpipe incl. cement mortar lining, zinc (zinc-aluminium) and ( $5 \mathrm{mpipe} / 6 \mathrm{mpipe}$ ), which results from the angular deflection possible at the sockets - applies to both open trench and finishing layer, ${ }^{3)}$ Theoretical weight per mpipe incl. cement mortar coating \& lining and zinc, ${ }^{4)}$ trenchless laying, ${ }^{8}$ Approx. assembly time of the joint, not including any protection it may be given, ${ }^{9}$ See notes on the use of $\mathrm{s} 1=\mathrm{min}$. dimension, $\mathrm{s} 2 / \mathrm{s} 3=$ nominal dimensions. Note that tolerances are possible clamping rings, page 72

BLS ${ }^{\text {joint }}$
DN 600 to DN 1000


| DN | Dimensions [mm] ${ }^{\text {² }}$ |  |  |  |  |  |  | Weight [kg] |  | Number oflocks locks | PFA ${ }^{2}$ [ [bar] | Allowabletractive force3) $[\mathrm{kN}]$ | Max. angular deflection [] | $\operatorname{Min.}_{\text {radius }^{4}}{ }^{[\mathrm{m}]}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | d |  | D | t | L | a | b | Set of locks | Gasket |  |  |  |  |  |
| 600 | 635 | +1 -4 | 732 | 175 | 116 | 9 | 6 | 9 | 2.3 | 9 | 32 | 1,525 | 2.0 | 172 |
| 700 | 738 | $\begin{array}{r}+1 \\ \hline-4.3\end{array}$ | 849 | 197 | 134 | 9 | 6 | 11 | 4.3 | 10 | 25 | 1,650 | 1.5 | 230 |
| 800 | 842 | +1 +4.5 | 960 | 209 | 143 | 9 | 6 | 14 | 5.2 | 10 | 16/25 ${ }^{\text {6 }}$ | 1,460 | 1.5 | 230 |
| 900 | 945 | $\begin{array}{r}+1 \\ \hline-4.8\end{array}$ | 1,073 | 221 | 149 | 9 | 6 | 13 | 6.3 | 13 | 16/25 ${ }^{\text {6 }}$ | 1,845 | 1.5 | 230 |
| 1,000 | 1,048 | $\begin{array}{r}+1 \\ \hline-5\end{array}$ | 1,188 | 233 | 159 | 9 | 6 | 16 | 8.3 | 14 | 10/25 ${ }^{\text {6 }}$ | 1,560 | 1.5 | 230 |

[^1]
## BLS ${ }^{\ominus}$-pipe <br> DN 600 to DN 1000



Laying length of 6 m .
External coatings

- Cement mortar coating (TRM ZMU)

Internal coatings

- Zinc coating with finishing layer
- Zinc-aluminium coating with finishing layer (Zinc PLUS)
- WKG insulation
- 
- High-alumina cement

| DN | Dimensions [mm] ${ }^{\text {4 }}$ |  |  | Weight [kg] |  | Number of locks | PFA ${ }^{\text {® }}$ [bar] | Allowable tractive force ${ }^{5}$ [kN] | Max. angular deflection [`] | Minimum radius ${ }^{6)}$ [m] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{S}_{1}$ | Cement mortar lining $\mathrm{s}_{2}$ | Cement mortar coating $\mathrm{S}_{3}$ | permpipe ${ }^{\text {2) }}$ | $\begin{gathered} \text { permpipe + } \\ \text { cement mortar } \\ \text { coating }{ }^{3} \end{gathered}$ |  |  |  |  |  |
| 600 | 8.0 | 5 | 5 | 186.4 | 206.6 | 9 | 32 | 1,525 | 2.0 | 172 |
| 700 | 8.8 | 6 | 5 | 235.0 | 258.3 | 10 | 25 | 1,650 | 1.5 | 230 |
| 800 | 9.6 | 6 | 5 | 294.6 | 321.3 | 10 | 16/25 ${ }^{\text {8 }}$ | 1,460 | 1.5 | 230 |
| 900 | 10.4 | 6 | 5 | 355.2 | 385.0 | 13 | 16/25 ${ }^{\text {8 }}$ | 1,845 | 1.5 | 230 |
| 1,000 | 11.2 | 6 | 5 | 420.7 | 453.9 | 14 | 10/25 ${ }^{\text {8 }}$ | 1,560 | 1.5 | 230 |

[^2]
### 2.2 Fittings with positive locking joints

Compatibility
There is no compatibility with positive locking systems used by other manufacturers. For possible solutions in this regard, please get in touch with our Applications Engineering Division.

E-mail address: office@trm.at

Laying lengths
Except where otherwise noted, the laying lengths Lu of fittings conform to the A series in EN 545.

Flanged fittings (see chapter 4)
When ordering flanged fittings, it is essential to give the PN pressure rating required. Accessories such as hex-head bolts, nuts, washers and gaskets must be obtained from specialist suppliers.

## Coating

Except where otherwise specified, all the fittings shown below are provided internally and externally with an epoxy coating at least $250 \mu \mathrm{~m}$ thick. The coating complies with EN 14901 and meets the requirements of the Quality Association for the Heavy Duty Corrosion Protection of Powder Coated Valves and Fittings (GSK). All fittings to EN 545, Annex D.2.3., can thus be installed in soils of any desired corrosiveness. For notes on the fields of use of the coating see chapter 5 .

Allowable operating pressure (PFA)
(except where otherwise stated)

| DN | PFA [bar] |  |  |
| :---: | :---: | :---: | :---: |
|  | VRS ${ }^{\text {- }}$ T | BLS ${ }^{\text {® }}$ | Flanged |
| 80-300 | 100 | - | PFA $=$ PN |
| 400 | 30 | - |  |
| 500 | 30 | - |  |
| 600 | - | 40 |  |
| 700 | - | 25 |  |
| 800 | - | 25 |  |
| 900 | - | 25 |  |
| 1,000 | - | 25 |  |

PFA: maximum allowable operating pressure in bars

- PMA $=1.2 \times$ PFA (allowable maximum operating pressure for a short period, e.g. the period of a pressure surge)
- $P E A=1.2 \times P F A+5$ (allowable site test pressure)


## Scope of supply

The fittings supplied by TRM include all the gaskets, locks and other securing components required for all the sockets. For flanged joints, the gaskets, bolts, nuts and washers are not included in the scope of supply.


## MMK 11 fittings

$1114^{\circ}$ double socket bends
to EN 545


| DN | Dimensions [mm] | PFA [bar] | Weight [kg] ~ |
| :---: | :---: | :---: | :---: |
|  | $L^{\prime}$ |  |  |
| VRS ${ }^{\text {-T }}$ |  |  |  |
| 80 | 30 | 100 | 10.1 |
| 100 | 30 |  | 14.0 |
| 125 | 35 |  | 18.6 |
| 150 | 35 |  | 23.3 |
| 200 | 40 |  | 38.2 |
| 250 | 50 |  | 52.3 |
| 300 | 55 |  | 70.4 |
| 400 | 65 | 30 | 116.0 |
| 500 | 75 |  | 171.5 |
| BLS ${ }^{\circ}$ |  |  |  |
| 600 | 85 | 40 | 186.0 |
| 700 | 95 | 25 | 277.0 |
| 800 | 110 |  | 378.0 |
| 900 | 120 |  | 532.0 |
| 1,000 | 130 |  | 614.0 |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |




MMK 22 fittings
$2212^{\circ}$ double socket bends
$\sim$
to EN 545






| DN | dn | Dimensions [mm] |  | PFA [bar] | Weight [kg] ~ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Lu | ${ }_{4}$ |  |  |
| VRS®-T |  |  |  |  |  |
| 80 | 80 | 170 | 85 | 100 | 16.1 |
| 100 | 80 | 170 | 95 |  | 20.0 |
|  | 100 | 190 | 95 |  | 22.4 |
| 125 | 80 | 170 | 105 |  | 25.1 |
|  | 100 | 195 | 110 |  | 28.1 |
|  | 125 | 225 | 110 |  | 31.0 |
| 150 | 80 | 170 | 120 |  | 33.6 |
|  | 100 | 195 | 120 |  | 34.5 |
|  | 125 | 255 | 125 |  | 39.0 |
|  | 150 | 255 | 125 |  | 41.1 |
| 200 | 80 | 175 | 145 |  | 46.2 |
|  | 100 | 200 | 145 |  | 47.3 |
|  | 125 | 255 | 145 |  | 50.0 |
|  | 150 | 255 | 150 |  | 54.3 |
|  | 200 | 315 | 155 |  | 63.1 |
| 250 | 80 | 180 | 170 |  | 72.0 |
|  | 100 | 200 | 170 |  | 63.9 |
|  | 125 | 230 | 175 |  | 78.0 |
|  | 150 | 260 | 175 |  | 70.6 |
|  | 200 | 315 | 180 |  | 77.8 |
|  | 250 | 375 | 190 |  | 89.1 |
| 300 | 80 | 180 | 195 | 100 | 93.0 |
|  | 100 | 205 | 195 |  | 80.2 |
|  | 150 | 260 | 200 |  | 88.6 |
|  | 200 | 320 | 205 |  | 96.6 |
|  | 250 | 375 | 210 |  | 109.0 |
|  | 300 | 435 | 220 |  | 127.4 |
| 400* | 400 | 560 | 280 | 30 | 236.0 |
| 500* | 500 | 800 | 400 |  | 396.8 |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |

[^3]
to manufacturer's standard


| DN |  |  | PFA [bar] | Weight [kg] ~ |
| :---: | :---: | :---: | :---: | :---: |
|  | $I_{u}$ | $\mathrm{L}_{\text {u }}$ |  |  |
| VRS ${ }^{\text {® }}$-T; $=1114^{\circ}$ |  |  |  |  |
| 80 | 30 | 175 | 100 | 8.4 |
| 100 | 30 | 185 |  | 11.1 |
| 125 | 35 | 200 |  | 15.1 |
| 150 | 35 | 210 |  | 20.1 |
| 200 | 40 | 230 |  | 32.7 |
| 250 | 50 | 250 |  | 51.0 |
| 300 | 55 | 270 |  | 71.0 |
| 400 | 65 | 375 | 63 | 125.0 |
| 500 | 75 | 405 | 50 | 220.0 |
| DN | Dimensions [mm] |  | PFA [bar] | Weight [kg] ~ |
|  | ${ }_{\text {I }}$ | $L_{u}$ |  |  |
| VRS ${ }^{\text {® }}$-T; $=221{ }^{\circ}{ }^{\circ}$ |  |  |  |  |
| 80 | 40 | 185 | 100 | 8.7 |
| 100 | 40 | 195 |  | 11.6 |
| 125 | 50 | 215 |  | 15.9 |
| 150 | 55 | 230 |  | 21.5 |
| 200 | 65 | 255 |  | 35.3 |
| 250 | 75 | 275 |  | 53.0 |
| 300 | 85 | 300 |  | 73.0 |
| 400 | 110 | 420 | 63 | 138.8 |
| 500 | 130 | 460 | 50 | 220.0 |



| DN | Dimensions [mm] |  | PFA [bar] | Weight [kg] ~ |
| :---: | :---: | :---: | :---: | :---: |
|  | ${ }_{u}$ | $\mathrm{L}_{\mathbf{u}}$ |  |  |
| VRS ${ }^{\text {- }}$ - ${ }^{\text {a }}=30^{\circ}$ |  |  |  |  |
| 80 | 45 | 190 | 100 | 8.9 |
| 100 | 50 | 205 |  | 11.9 |
| 125 | 55 | 220 |  | 16.2 |
| 150 | 65 | 240 |  | 22.4 |
| 200 | 80 | 270 |  | 36.5 |
| 250 | 95 | 295 |  | 57.0 |
| 300 | 110 | 320 |  | 82.0 |
| 400 | 140 | 450 | 63 | 157.2 |
| 500 | 170 | 495 | 50 | 224.0 |
| DN | Dimensions [mm] |  | PFA [bar] | Weight [kg] ~ |
|  | ${ }_{u}$ | $L_{u}$ |  |  |
| VRS ${ }^{\text {- }}$ T; $=45^{\circ}$ |  |  |  |  |
| 80 | 55 | 200 | 100 | 9.1 |
| 100 | 65 | 220 |  | 12.3 |
| 125 | 75 | 240 |  | 17.0 |
| 150 | 85 | 260 |  | 24.2 |
| 200 | 110 | 300 |  | 39.7 |
| 250 | 130 | 335 |  | 60.5 |
| 300 | 150 | 365 |  | 87.3 |



* To manufacturer's standard


| DN | L [mm] | Weight [kg] |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | PN 10 | PN 16 | PN 25 | PN 40 | PN 63 | PN 100 |
| VRS ${ }^{\text {® }}$-T |  |  |  |  |  |  |  |
| 80 | 350 | 7.5 |  |  |  | 11.9 | 11.2 |
| 100 | 360 | 8.5 |  | 10.4 |  | 14.1 | 15.7 |
| 125 | 370 | 12.4 |  | 13.1 | 14.3 | 20.0 | 22.8 |
| 150 | 380 | 19.3 |  | 21.0 | 21.0 | 31.9 | 28.0 |
| 200 | 400 | 25.2 | 25.2 | 26.0 | 30.8 | 46.6 | 55.4 |
| 250 | 420 | 35.1 | 35.2 | 37.7 | 45.4 | - | - |
| 300 | 440 | 46.0 | 44.8 | 49.1 | 62.0 | - | - |
| 400 | 480 | 104.0 | 109.0 | 114.0 | 154.0* | - | - |
| 500 | 500 | 146.0 | 156.0 | 161.0 | - | - | - |
| BLS ${ }^{\text {® }}$ |  |  |  |  |  |  |  |
| 600 | 560 | 134.3 | 160.3 | 174.3 | 235.3 | - | - |
| 700 | 600 | 180.6 | 195.6 | 229.6 | - | - | - |
| 800 | 600 | 228.0 | 247.0 | 296.0 | - | - | - |
| 900 | 600 | 348.0 | 359.0 | - | - | - | - |
| 1,000 | 600 | 503.0 | 538.0 | - | - | - | - |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |

* Take note of the PFA of the $\mathrm{VRS}{ }^{*}-$ T joint
U fittings
Collars
to EN 545



There are cases where collars with VRS ${ }^{刃}$-T joints cannot be fully slid on.
They must be used only with TYTON ${ }^{\star}$ gaskets.


| DN | $\mathrm{L}_{\mathrm{u}}$ [mm] | z [mm] | Weight [kg] |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | PN 10 | PN 16 | PN 25 | PN 40 | PN 63 | PN 100 |
| VRS ${ }^{\text {- }}$ T |  |  |  |  |  |  |  |  |
| 80 | 130 | 90 |  |  |  | 0.2 | 12.3 | - |
| 100 | 130 | 90 |  | 12.2 |  | 12.7 | 16.3 | 20.7 |
| 125 | 135 | 95 |  | 15.5 | 17.0 | 17.0 | 26.8 | - |
| 150 | 135 | 95 |  | 19.9 | 22.1 | 22.1 | 31.5 | 33.4 |
| 200 | 140 | 100 | 28.7 | 28.9 | 29.6 | 34.6 | 49.0 | 56.4 |
| 250 | 145 | 105 | 40.6 | 39.7 | 44.3 | 51.9 | 67.5 | 86.4 |
| 300 | 150 | 110 | 52.3 | 52.1 | 56.1 | 69.9 | 84.9 | 120.0 |
| 400 | 160 | 120 | 85.5 | 89.0 | 102.0 | 127.5 | - | - |
| 500 | 170 | 130 | 125.0 | 140.5 | 151 | 162.0* | - | - |
| BLS ${ }^{\text {® }}$ |  |  |  |  |  |  |  |  |
| 600 | 180 | 140 | 137.5 | 167.5 | 173.5 | 209.0* | - | - |
| 700 | 190 | 150 | 202.0 | 248.0 | 278.0 | - | - | - |
| 800 | 200 | 160 | 269.5 | 270.0 | 316.0 | - | - | - |
| 900 | 210 | 170 | 347.0 | 370.0 | 427.0 | - | - | - |
| 1,000 | 220 | 180 | 439.0 | 464.0 | 549.0 | - | - | - |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |

[^4]

| DN | dn | $\mathrm{L}_{\mathrm{u}}[\mathrm{mm}]$ | ${ }_{\text {u }}$ [mm] | Weight[kg] |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | PN 10 | PN 16 | PN 25 | PN 40 |
| VRS®-T |  |  |  |  |  |  |  |
| 80 | 80 | 170 | 165 | 15.8 |  |  |  |
| 100 | 80 | 170 | 175 |  |  |  |  |
|  | 100 | 190 | 180 | 21.9 |  | - |  |
| 125 | 80 | 170 | 190 | 24.8 |  |  |  |
|  | 100 | 195 | 195 | 27.6 |  | 24.8 |  |
|  | 125 | 255 | 200 | - |  | - | - |
| 150 | 80 | 170 | 205 |  |  |  |  |
|  | 100 | 195 | 210 |   <br> 33.0 30.6 |  |  |  |
|  | 150 | 225 | 220 |  | 39.0 | - | - |
| 200 | 80 | 175 | 235 | 39.0 45.4 |  |  |  |
|  | 100 | 200 | 240 | 46.8 |  | - |  |
|  | 150 | 250 | 250 | 51.6 |  | - | - |
|  | 200 | 315 | 260 | - | 57.0 |  | - |
| 250 | 80 | 180 | 265 | 56.0 |  |  |  |
|  | 100 | 200 | 270 | 57.5 |  | - |  |
|  | 150 | 260 | 280 | 63.5 |  | - | - |
|  | 200 | 315 | 290 | - | 71.5 | - | - |
|  | 250 | 375 | 300 | - <br> 76.6 |  | - | - |
| 300 | 80 | 180 | 295 |  |  |  |  |
|  | 100 | 205 | 300 | 81.2 |  |  | - |  |
|  | 150 | 260 | 310 | 80.0 |  | - | - |
|  | 200 | 320 | 320 | - | - | - | - |
|  | 300 | 435 | 340 | 110.0 |  |  | - |
| 400 | 150 | 270 | 370 |  |  | 152.0 | 152.0 |
|  | 200 | 440 | 380 | 170.0 | 171.0 | 173.0 | - |
|  | 300 | 440 | 400 | 191.0 | 192.0 | 197.0 | - |
|  | 400 | 560 | 420 | 200.0 | 205.0 | 217.0 | - |
| 500 | 200 | 450 | 440 | 192.5 | 192.5 | 194.5 | - |
|  | 300 | 450 | 460 | 205.0 | 205.0 | 211.0 | - |
|  | 400 | 565 | 480 | 297.0 | 303.0 | 315.0 | - |
|  | 500 | 680 | 500 | 338.0 | 362.0 | 363.0 | 372* |
| 600 | 150 | 570 | 490 | 237.0 |  | 238.0 | - |
|  | 200 |  | 500 | 254.0 | 254.0 | 247.0 | - |
|  | 300 |  | 520 | 266.0 | 266.0 | 272.0 | - |
|  | 400 |  | 540 | 279.0 | 284.0 | 296.0 | - |
|  | 600 | 800 | 580 | 376.5 | 401.0 | 415.0 | - |
| 800 | 150 | 1045 | 580 | 657.0 |  | 645.0 | - |
|  | 200 |  | 585 | 667.0 | 667.0 | 655.0 | - |
|  | 400 |  | 615 | 695.0 | 682.0 | 693.0 | - |
|  | 600 |  | 645 | 745.0 | 770.0 | 784.0 | - |
|  | 800 |  | 675 | 791.0 | 809.0 | 855.0 | - |
| 900 | 100 | 475 | 630 | 540.0 | 592.0 | 598.0 | - |
|  | 125 |  | 635 | 541.0 | 593.0 | 594.0 | - |
|  | 150 |  | 640 | 543.0 | 594.0 | 600.0 | - |
|  | 200 |  | 645 | 546.0 | 596.0 | 603.0 | - |
|  | 250 |  | 655 | 550.0 | 599.0 | 608.0 | - |
|  | 300 |  | 660 | 555.0 | 603.0 | 613.0 | - |
| 1,000 | 100 | 480 | 690 | 672.0 | 738.0 | 745.0 | - |
|  | 125 |  | 695 | 673.0 | 738.0 | 746.0 | - |
|  | 150 |  | 700 | 675.0 | 739.0 | 747.0 | - |
|  | 200 |  | 705 | 678.0 | 741.0 | 750.0 | - |
|  | 250 |  | 715 | 682.0 | 741.0 | 750.0 | - |
|  | 300 |  | 720 | 687.0 | 748.0 | 760.0 | - |
|  |  |  |  |  |  |  |  |
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|  |  |  |  |  |  |  |  |

[^5]0 fittings
Spigot end caps
to manufacturer's standard


| DN | $\mathrm{t}[\mathrm{mm}]$ | $\mathrm{D}[\mathrm{mm}]$ | PFA [bar] | Weight [kg] |
| :---: | :---: | :---: | :---: | :---: |
| VRS $^{\circ}-\mathrm{T}$ 0-Stücke |  |  |  |  |
| 400 | 225 | 540 | 30 | 117 |
| 500 | 240 | 650 | 30 | 170 |

## Pplugs

Socket plugs
to manufacturer's standard
F


| DN | L. [mm] | I. [mm] | d [mm] | PFA [bar] | Masse [kg] |
| :---: | :---: | :---: | :---: | :---: | :---: |
| VRS ${ }^{\circ}$-T Pplug |  |  |  |  |  |
| 80 | 170 | 86 | M 12 | 100 | 4.1 |
| 100 | 175 | 91 | M12 |  | 4.4 |
| 125 | 195 | 96 | M16 |  | 6.7 |
| 150 | 200 | 101 | M16 |  | 9.2 |
| 200 | 210 | 106 | M 16 |  | 14.5 |
| 250 | 250 | 106 | M20 |  | 27.2 |
| 300 | 300 | 106 | M20 |  | 49.4 |



| DN | Weioght[kg] |  |  |  |  |  |  |  | Coating internal/ external |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | PFA [bar] |  |  |  |  |  |  |  |  |
|  | 10 | 16 | 25 | 30 | 40 |  |  | 100 |  |
| VRS ${ }^{\circ}-\mathrm{T}$ L $=400 \mathrm{~mm}$ oder 800 mm |  |  |  |  |  |  |  |  |  |
| 80 | 7.6 bzw .15 .4 |  |  |  |  |  |  |  | Epoxy/ Epoxy |
| 100 | 12.0 bzw. 25.0 |  |  |  |  |  |  |  |  |
| 125 |  |  |  |  |  |  |  |  |  |
| 150 | 15.6 bzw. 31.0 |  |  |  |  |  |  |  |  |
| 200 | 22.0 bzw. $44.0{ }^{\text {² }}$ |  |  |  |  |  |  |  |  |
| $\mathrm{VRS}^{\circ}-\mathrm{T} \mathrm{L}^{\text {a }}=800 \mathrm{~mm}$ |  |  |  |  |  |  |  |  |  |
| 250 | 44.6 |  |  |  |  | 66.7 |  |  | Epoxy/ Epoxy |
| 300 | 55.8 |  |  | 56.8 |  |  |  |  |  |
| 400 | 81.3 |  |  |  | - |  |  |  |  |
| 500 | 104.0 |  |  |  |  |  |  |  |  |
|  | BLS ${ }^{\circ} \mathrm{L}=800 \mathrm{~mm}$ |  |  |  |  |  |  |  | Cement mortar/ zinc + epoxy |
| 600 | $127.6{ }^{2 /}$ |  |  |  | - |  |  | - |  |
| 700 |  | 164.1 |  | - | - |  |  | - |  |
| 800 | $\begin{aligned} & 201.8 \\ & 240.4 \end{aligned}$ |  | 219.6 | - | - |  |  | - |  |
| 900 |  |  | 263.2 | - | - |  |  | - |  |
| 1,000 |  | 310.4 |  | - | - |  |  | - |  |

1) PFA of 100 with high-pressure lock 2) Max. PFA of 32

HAS fittings (A fittings)
House service connection fittings
with outlet with 2 " female thread
to manufacturer's standard


| DN | L. [mm] | I. [mm] | PFA [bar] | Weight [kg] |
| :---: | :---: | :---: | :---: | :---: |
| VRS ${ }^{\text {®-T }}$ HAS-fittings |  |  |  |  |
| 80 | 305 | 215 | 100 | 10.5 |
| 100 | 315 | 225 |  | 13.8 |
| 125 | 325 | 235 |  | 17.8 |
| 150 | 340 | 250 |  | 23.1 |
| 200 | 355 | 265 |  | 34.8 |
| 250 | 370 | 275 |  | 54.0 |
| 300 | 380 | 285 |  | 72.0 |



| DN | Dimensions [mm] |  |  |  | Weight [kg] |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | $\mathrm{L}_{2}$ | c | d | PN 10 | PN 16 | PN 25 | PN 40 |
| VRS ${ }^{\text {- }}$ T EN-fittings |  |  |  |  |  |  |  |  |
| 80 | 165 | 145 | 110 | 180 |  |  |  |  |
| 100 | 180 | 158 | 125 | 200 |  |  |  |  |

## Marking of fittings

All fittings produced by member companies of the "Fachgemeinschaft Gussrohrsysteme/European Association for Ductile Iron Pipe Systems (FGR/ EADIPS)" carry the "FGR" mark indicating that all the guidelines required for the award of the "FGR Quality Mark" have been complied with. As well as this, all fittings are marked with their nominal sizes and bends are marked with their respective angles.

Flanged fittings have the pressure ratings PN 16, 25 or 40 cast or stamped onto them. No pressure rating appears on flanged fittings for PN 10 or on any socket fittings.

To identify their material as "ductile iron", fittings are marked with three raised dots arranged in a triangle $\left(\bullet^{\bullet}\right)$ ) on their outer surface. In special cases, there may be further markings which are specified as needing to be applied.


## 3 - THE NON-POSITIVE LOCKING SYSTEM

### 3.1 Overview

This Chapter deals only with non-positive locking push-in joints.

Dealt with below are the following non-restrained joints:

## - The TYTON joint (TYT) to DIN 28603 - DN 80 to DN 1,000

The TYTON joint has been the leading joint for pipes and fittings on the international market since 1965 . It can be deflected angularly to a maximum of $5^{\circ}$, is resistant to the penetration of roots and is leaktight at any desired internal water pressure.

- The bolted gland joint (STB) to DIN 28602 - DN 400 to DN 1,000 Available for certain fittings such as flanged sockets and collars Suitable above all for later connections into existing pipelines.

Pipes and fittings with non-positive locking joints are designed primarily for conventional open trench laying.

The sizing of thrust blocks and of the lengths of pipelines needing to be restrained is dealt with in outline in Chapter 8.

PFA - allowable operating pressure
Under EN 545:2010, ductile iron pipe with non-restrained push-in joints (e.g.
TYTON ${ }^{\circledR}$ joints) are divided into pressure classes. These pressure classes are also known as $C$ classes. The maximum PFA of a pipe corresponds to its pressure class (e.g. $C 50=$ PFA of 50 bars). This applies only to non-restrained pipes.

TYTON ${ }^{\circledR}$ push-in joint
to DIN 28603


DN 80 to DN 600


Socket for fittings

| DN | Dimensions [mm] |  |  | Weight [kg] ~ |  |  |  | Max. angular deflection |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Socket |  |  | Gasket |  |
|  | Ød ${ }_{1}$ | ø ${ }^{1}$ | t | Pipe | Fitting | Flanged socket |  |  |
| 80 | 98 | 142 | 84 | 3.4 | 2.8 | 2.4 | 0.13 | $5{ }^{\circ}$ |
| 100 | 118 | 163 | 88 | 4.3 | 3.3 | 3.1 | 0.16 |  |
| 125 | 144 | 190 | 91 | 5.7 | 4.5 | 4.0 | 0.19 |  |
| 150 | 170 | 217 | 94 | 7.1 | 5.6 | 4.9 | 0.22 |  |
| 200 | 222 | 278 | 100 | 10.3 | 8.0 | 7.1 | 0.37 |  |
| 250 | 274 | 336 | 105 | 14.2 | 11.1 | 9.7 | 0.48 |  |
| 300 | 326 | 385 | 110 | 18.6 | 14.3 | 12.5 | 0.67 |  |
| 350 | 378 | 448 | 110 | 23.7 | 17.1 | 15.2 | 0.77 | $4^{\circ}$ |
| 400 | 429 | 500 | 110 | 29.3 | 20.8 | 18.6 | 1.1 |  |
| 500 | 532 | 607 | 120 | 42.3 | 31.7 | 27.6 | 1.6 | $3^{\circ}$ |
| 600 | 653 | 732* | 120 | 59.3 | 42.3 | 36.2 | 2.3 |  |
| 700 | 738 | 849* | 197 | 79.1 | 71.2 | 59.1 | 4.3 |  |
| 800 | 842 | 960* | 209 | 102.6 | 95.4 | 79.8 | 5.2 |  |
| 900 | 945 | 1,073* | 221 | 129.9 | 150.3 | 122.7 | 6.3 |  |
| 1,000 | 1,048 | 1,188* | 233 | 161.3 | 186.9 | 152.1 | 8.3 |  |

[^6]Bolted gland joint (STB) to DIN 28602


| DN | Dimensions [mm] |  |  |  |  | Weight [kg] ~ |  |  |  | Max. angular deflection | PFA |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Ø d ${ }_{1}$ | Ø D | $\emptyset \mathrm{d}$ | 1 | n | t | Bolted gland ring | Gasket | Teehead bolt |  |  |
| 400 | 429 | 570 | M20 | 90 | 12 | 132 | 10.6 | 0.8 | 5.5 | $3{ }^{\circ}$ | 25 |
| 500 | 532 | 680 | M20 | 100 | 16 | 138 | 15.0 | 1.1 | 7.7 | 3 | 25 |
| 600 | 635 | 790 | M20 | 100 | 16 | 143 | 20.9 | 1.5 | 7.7 |  | 25 |
| 700 | 738 | 900 | M20 | 110 | 20 | 149 | 27.2 | 1.9 | 10.0 | $2^{\circ}$ | 16 |
| 800 | 842 | 1,010 | M20 | 110 | 24 | 154 | 34.1 | 2.3 | 12.0 |  | 16 |
| 900 | 945 | 1,125 | M20 | 120 | 24 | 160 | 44.0 | 2.9 | 12.5 | $1.5{ }^{\circ}$ | 16 |
| 1,000 | 1,048 | 1,250 | M 24 | 120 | 24 | 165 | 56.9 | 3.5 | 18.5 |  | 16 |

PFA: allowable operating pressure in bars; may be lower depending on the pressure class
PMA $=1.2 \times$ PFA; PEA $=1.2 \times$ PFA +5


PFA: allowable operating pressure in bars; may be lower depending on the pressure class
PMA $=1.2 \times$ PFA; PEA $=1.2 \times$ PFA +5

### 3.2 Tyton $^{\oplus}$ pipes -6 m laying length

Tyton ${ }^{\circ}$ pipes -6 m laying length
DN 80 to DN 1000
to EN 545:2010


External coatings

- cement mortar coating (TRM ZMU)
- zinc coating with finishing layer
- zinc-aluminium coating with finishing layer (TRM Zinc PLUS)
- WKG coating


Internal coatings

- blast furnace cement
- high-alumina cement

For notes on the fields of use of the coatings see Chapter 5

| DN | $\begin{gathered} \mathrm{d}_{1} \\ \text { [mm] } \end{gathered}$ | C25 |  | C30 |  | C 40 |  |  | C50 |  |  | C64 |  |  | C 100 |  |  | $\begin{aligned} & \text { Weight } \\ & \text { ZMU } \\ & \text { [kg] } \\ & \hline \end{aligned}$ | $\mathrm{S}_{2}$ | $\mathrm{S}_{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $S_{1}$ | Weight [kg] | $\mathrm{S}_{1}$ | Weight [kg] | $\mathrm{S}_{1}$ | Weight [kg] | $\begin{gathered} \text { PFA } \\ \text { (BRS) } \end{gathered}$ | $\mathrm{S}_{1}$ | Weight [kg] | $\begin{gathered} \hline \text { PFA } \\ \text { (BRS) } \end{gathered}$ | $\mathrm{S}_{1}$ | Weight [kg] | $\begin{gathered} \text { PFA } \\ \text { (BRS) } \end{gathered}$ | $\mathrm{S}_{1}$ | Weight [kg] | $\begin{gathered} \hline \text { PFA } \\ \text { (BRS) } \end{gathered}$ |  |  |  |
| 80 | $98-{ }_{-27}^{+1}$ |  |  |  |  |  |  |  | 3.5 | 79.1 | 16 |  |  |  | $4.7{ }^{3)}$ | 94.0 | 32 | 19.5 | 4 | 5 |
| 100 | 118 |  |  |  |  |  |  |  | 3.5 | 98.7 | 16 |  |  |  | $4.7{ }^{3)}$ | 118.4 | 32 | 24.0 | 4 |  |
| 125 | 144 |  |  |  |  |  |  |  | 3.5 | 125.2 | 16 | $4.8{ }^{3)}$ | 150.4 | 25 | 5.0 | 155.5 | 25 | 28.0 | 4 |  |
| 150 | 170-19 |  |  |  |  |  |  |  | $3.7{ }^{17}$ | 154.3 | 16 | $\begin{aligned} & 4.7^{2)} \\ & 5.0^{3)} \end{aligned}$ | $\begin{array}{r} 175.4 \\ 183.8 \\ \hline \end{array}$ | 25 | 5.9 | 205.8 | 25 | 33.0 | 4 |  |
| 200 | $222{ }^{+1+0}$ |  |  |  |  |  |  |  | 3.9 | 209.1 | 16 | $\begin{aligned} & 5.0^{2} \\ & 5.5^{3)} \end{aligned}$ | $\begin{aligned} & 245.4 \\ & 259.2 \end{aligned}$ | 25 | 7.7 | 323.1 | 25 | 43.0 | 4 |  |
| 250 | $274{ }^{\frac{7}{-31}}$ |  |  |  |  | $4.2{ }^{11}$ | 272.9 | 16 | $5.2^{2)}$ | 316.3 | 25 | 6.1 | 347.4 | 25 | 9.5 | 468.1 | 25 | 52.0 | 4 |  |
| 300 | 326 ${ }^{-3,3}$ |  |  |  |  | 4.6 | 351.8 | 16 | $5.7{ }^{\text {2) }}$ | 410.0 | 25 | 7.3 | 475.8 | 25 |  |  |  | 63.0 | 4 |  |
| 350 | $378{ }^{-34}$ |  |  | 4.7 | 416.1 | $6.0{ }^{2}$ | 496.0 | 25 | 6.6 | 524.8 | 25 | 8.5 | 615.6 | 25 |  |  |  | 72.0 | 5 |  |
| 400 | $429{ }^{-1.5}$ |  |  | 4.8 | 513.3 | $6.4{ }^{2)}$ | 601.3 | 16 | 7.5 | 661.5 | 16 | 9.6 | 775.4 | 16 |  |  |  | 82.0 | 5 |  |
| 500 | $532{ }^{-38}$ |  |  | 5.6 | 707.4 | 7.5 | 837.4 | 16 | 9.3 | 959.7 | 16 |  |  |  |  |  |  | 101.0 | 5 |  |
| 600 | $635^{-4.0}$ |  |  | 6.7 | 982.1 | 8.9 | 1.162 .0 | 10 |  |  |  |  |  |  |  |  |  | 121.0 | 5 |  |
| 700 | $738{ }_{41}^{-43}$ | 6.8 | 1,173.3 | 7.8 | 1,268.8 | 10.4 | 1.516 .0 | - |  |  |  |  |  |  |  |  |  | 140.0 | 6 |  |
| 800 | $842_{41}^{-45}$ | 7.5 | 1,479.1 | 8.9 | 1,631.8 |  |  |  |  |  |  |  |  |  |  |  |  | 160.0 | 6 |  |
| 900 | $945{ }_{\text {+1 }}^{-4.8}$ | 8.4 | 1,798.4 | 10.0 | 1,994.4 |  |  |  |  |  |  |  |  |  |  |  |  | 179.0 | 6 |  |
| 1,000 | 1,048 | 9.3 | 2,151.3 | 11.1 | 2,395.9 |  |  |  |  |  |  |  |  |  |  |  |  | 199.0 | 6 |  |

${ }^{17}$ C40 under EN545:2006; ${ }^{2)}$ K9 under EN 545:2006; ${ }^{3}$ K10 under EN 545:2006
$\mathrm{s}_{1}$ ) Minimum wall thickness in mm ; $\mathrm{s}_{2}$ ) Nominal thickness of cement mortar lining in mm; $\mathrm{s}_{3}$ ) Nominal thickness of ZMU in mm; Weight of the
pipes $=$ theoretical figures in kg incl. cement mortar lining, zinc-aluminium coating and epoxy finishing layer; Weight of $\mathrm{ZMU}=$ additional weight of ZMU in kg;

The maximum PFA of a pipe corresponds to its pressure class (e.g. C $50=$ PFA of 50 bars); PFA (BRS) $=$ PMA $=1.2 \times$ PFA; PEA $=1.2 \times$ PFA +5 ; Inside green frames: all coatings are possible; outside: only Zinc Plus; Other laying lenghts and outside coatings upon request.

### 3.3 Tyton ${ }^{\oplus}$ pipes -5 m laying length

## Tyton ${ }^{\circ}$ pipes -5 m laying length

DN 80 to DN 500
to EN 545:2010


External coatings

- Zinc coating with PUR-longlife finishing layer
- Zinc coating with PUR-TOP finishing layer
- WKG coating
- Other coatings up on request

Internal coatings

- Portland cement
- High-alumina cement
- Other coatings up on request

For notes on the fields of use of the coatings see Chapter 5

| DN | $\begin{gathered} \mathrm{d}_{1} \\ {[\mathrm{~mm}]} \end{gathered}$ | C30 |  | C 40 |  |  | C50 |  |  | C64 |  |  | C 100 |  |  | $\mathrm{S}_{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $S_{1}$ | Weight [kg] | $\mathrm{S}_{1}$ | Weight [kg] | $\begin{gathered} \text { PFA } \\ \text { (BRS) } \end{gathered}$ | $\mathrm{S}_{1}$ | Weight [kg] | $\begin{gathered} \text { PFA } \\ \text { (BRS) } \end{gathered}$ | $\mathrm{S}_{1}$ | Weight [kg] | $\begin{gathered} \hline \text { PFA } \\ \text { (BRS) } \end{gathered}$ | $\mathrm{S}_{1}$ | Weight [kg] | $\begin{gathered} \hline \text { PFA } \\ \text { (BRS) } \end{gathered}$ |  |
| 80 | $98{ }_{-27}^{+1}$ |  |  |  |  |  |  |  |  |  |  |  | $4.7{ }^{\text {3) }}$ | 79.5 | 32 | 4 |
| 100 | $118{ }_{-28}^{*+1}$ |  |  |  |  |  |  |  |  |  |  |  | $4.7{ }^{\text {3) }}$ | 97.3 | 32 | 4 |
| 125 | $144{ }_{-28}^{18}$ |  |  |  |  |  |  |  |  | $4.8{ }^{3)}$ | 123.8 | 25 | 5.0 | 126.7 | 25 | 4 |
| 150 | $170{ }_{-29}^{1+29}$ |  |  |  |  |  |  |  |  | $4.7{ }^{\text {2) }}$ | 146.3 | 25 | 5.9 | 167.1 | 25 | 4 |
| 200 | $222{ }_{-3,0}^{+1}$ |  |  |  |  |  |  |  |  | $5.0^{2)}$ | 202.5 | 25 | 7.7 | 264.1 | 25 | 4 |
| 250 | $274{ }_{-3,1}^{+1}$ |  |  | 3.9 | 215.1 | 16 | $5.2^{2)}$ | 260.1 | 25 | 6.1 | 285.9 | 25 | 9.5 | 382.0 | 25 | 4 |
| 300 | $326{ }_{-3,3}^{+1}$ |  |  | 4.6 | 293.5 | 16 | $5.7{ }^{\text {2) }}$ | 331.6 | 25 | 7.3 | 386.4 | 25 |  |  |  | 4 |
| 400 | $429{ }_{-3,5}^{1}$ | 4.8 | 423.8 | $6.4{ }^{2)}$ | 497.2 | 16 | 7.5 | 547.3 | 16 | 9.6 | 642.3 | 16 |  |  |  | 5 |
| 500 | $532{ }_{-3.8}^{+1}$ | 5.6 | 585.3 | $7.5^{2)}$ | 693.7 | 16 | 9.3 | 795.6 | 16 |  |  |  |  |  |  | 5 |

${ }^{1)}$ C40 under EN545:2006; 2) K9 under EN 545:2006; ${ }^{3)}$ K10 under EN 545:2006
$\mathrm{s}_{1}$ ) Minimum wall thickness in mm ; $\mathrm{s}_{2}$ ) Nominal thickness of cement mortar lining in mm
Weight = theoretical figures in kg incl. cement mortar lining, zinc coating and polyurethane (PUR) finishing layer; The
maximum PFA of a pipe corresponds to its pressure class (e.g. C $50=$ PFA of 50 bars); PFA (BRS $)=$ allowable operating pressure in bars with BRS gasket;
PMA $=1.2 \times$ PFA; PEA $=1.2 \times$ PFA +5 ; Other laying lenghts and outside coatings upon request.

### 3.4 Fittings with non-positive locking joints

## Compatibility

Except where otherwise noted, all fittings comply with DIN 28603 (TYTON*). This means that TYTON ${ }^{\circledR}$-SIT-PLUS ${ }^{\circledR}$ gaskets can also be inserted in their sockets, thus producing the friction locking BRS ${ }^{\oplus}$ push-in joint.

Laying lengths
Except where otherwise noted, the laying lengths Lu of fittings conform to the A series in EN 545.

Flanged fittings (see Chapter 4)
When ordering flanged fittings, it is essential to give the PN pressure rating required. Accessories such as hex-head bolts, nuts, washers and gaskets must be obtained from specialist suppliers.

Coating (see Chapter 5)
Except where otherwise specified, all the fittings shown below are provided internally and externally with an epoxy coating at least $250 \mu$ m thick.
The coating complies with EN 14901 and meets the requirements of the Quality Association for the Heavy Duty Corrosion Protection of Powder Coated Valves and Fittings (GSK).

All fittings to EN 545, Annex D.2.3., can thus be installed in soils of any desired corrosiveness.

Allowable operating pressure (PFA)
(except where otherwise specified)

| DN | PFA ${ }^{\text {1 }}$ [bar] |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | TYTON ${ }^{\text {® }}$ | BRS ${ }^{2)}$ | STB | Flange |
| 80 | 100 | 32 |  | $P F A=P N$ |
| 100 | 100 | 32 |  |  |
| 125 |  |  |  |  |
| 150 | 64 |  |  |  |
| 200 |  | 25 | - |  |
| 250 |  | 25 |  |  |
| 300 | 50 |  |  |  |
| 350 |  |  |  |  |
| 400 |  |  |  |  |
| 500 | 40 | 16 | 25 |  |
| 600 |  | 10 |  |  |
| 700 |  |  |  |  |
| 800 | 30 |  | 16 |  |
| 900 | 30 |  | 16 |  |
| 1,000 |  |  |  |  |

${ }^{1}$ ) PFA: allowable operating pressure in bars. PMA $=1.2 \times$ PFA; PEA $=1.2 \times$ PFA +5 2) PFA depends on the $C$ class of the pipe used, see p. 27

## Scope of supply

The socket fittings supplied include the gaskets required and with screwed socket joints and bolted gland joints they include the additional components required (slide rings, screw rings, bolted gland rings, tee-head bolts). For flanged joints, the gaskets, bolts, nuts and washers are not included in the scope of supply.
$1114^{\circ}$ double socket bends
to EN 545


| DN | Dimensions [mm] | PFA [bar] | Weight [kg] ~ |
| :---: | :---: | :---: | :---: |
|  | $L_{u}$ |  |  |
| 80 | 30 | 100 | 7.5 |
| 100 | 30 |  | 8.5 |
| 125 | 35 | 64 | 12.8 |
| 150 | 35 |  | 16.5 |
| 200 | 40 |  | 24.9 |
| 250 | 50 | 50 | 34.2 |
| 300 | 55 |  | 43.0 |
| 350 | 60 |  | 60.5 |
| 400 | 65 | 40 | 70.9 |
| 500 | 75 |  | 100.0 |
| 600 | 85 |  | 140.0 |
| 700 | 95 | 30 | 190.7 |
| 800 | 110 |  | 271.2 |
| 900 | 120 |  | 393.5 |
| 1,000 | 130 |  | 495.7 |

## MMK 30 fittings

$30^{\circ}$ double socket bends
to EN 545


| DN | Dimensions [mm] | PFA [bar] | Weight [kg] ~ |
| :---: | :---: | :---: | :---: |
|  | $\mathrm{L}_{u}$ |  |  |
| 80 | 45 | 100 | 7.7 |
| 100 | 50 |  | 9.7 |
| 125 | 55 | 64 | 14.0 |
| 150 | 65 |  | 18.0 |
| 200 | 80 |  | 22.0 |
| 250 | 95 | 50 | 32.0 |
| 300 | 110 |  | 43.2 |
| 350 | 125 |  | 71.5 |
| 400 | 140 | 40 | 85.3 |
| 500 | 180 |  | 109.2 |
| 600 | 200 |  | 155.9 |
| 700 | 230 | 30 | 275.3 |
| 800 | 260 |  | 345.9 |
| 900 | 290 |  | 496.3 |
| 1,000 | 320 |  | 630.3 |

MMK 22 fittings
$2212^{\circ}$ double socket bends
to EN 545


| DN | Dimensions [mm] | PFA [bar] | Weight [kg] ~ |
| :---: | :---: | :---: | :---: |
|  | $\mathrm{L}_{u}$ |  |  |
| 80 | 40 | 100 | 7.7 |
| 100 | 40 |  | 9.4 |
| 125 | 50 | 64 | 13.3 |
| 150 | 55 |  | 17.5 |
| 200 | 65 |  | 21.0 |
| 250 | 75 | 50 | 30.7 |
| 300 | 85 |  | 40.4 |
| 350 | 95 |  | 64.6 |
| 400 | 110 | 40 | 80.2 |
| 500 | 130 |  | 100.4 |
| 600 | 150 |  | 140.5 |
| 700 | 175 | 30 | 185.7 |
| 800 | 195 |  | 315.8 |
| 900 | 220 |  | 456.0 |
| 1,000 | 240 |  | 575.9 |

## MMK 45 fittings

$45^{\circ}$ double socket bends
to EN 545
3


| DN | Dimensions [mm] | PFA [bar] | Weight [kg] ~ |
| :---: | :---: | :---: | :---: |
| 80 | 55 | 100 | 8.1 |
| 100 | 65 | 100 | 10.0 |
| 125 | 75 |  | 14.1 |
| 150 | 85 | 64 | 18.4 |
| 200 | 110 |  | 24.6 |
| 250 | 130 |  | 35.7 |
| 300 | 150 | 50 | 48.7 |
| 350 | 175 |  | 76.9 |
| 400 | 195 |  | 86.0 |
| 500 | 240 | 40 | 127.0 |
| 600 | 285 |  | 183.6 |
| 700 | 330 |  | 296.7 |
| 800 | 370 | 30 | 406.1 |
| 900 | 415 | 30 | 577.9 |
| 1,000 | 460 |  | 737.2 |

MMQ fittings
$90^{\circ}$ double socket bends
to EN 545


| DN | Dimensions [mm] | PFA [bar] | Weight [kg] ~ |
| :---: | :---: | :---: | :---: |
|  | $\mathrm{L}_{\mathrm{u}}$ |  |  |
| 80 | 100 | 100 | 8.2 |
| 100 | 120 |  | 10.6 |
| 125 | 145 | 64 | 15.6 |
| 150 | 170 |  | 19.6 |
| 200 | 220 |  | 30.9 |
| 250 | 270 | 50 | 50.6 |
| 300 | 320 |  | 69.1 |
| $350{ }^{11}$ | 410 |  | 96.8 |
| $400{ }^{1)}$ | 430 | 40 | 119.0 |
| $500{ }^{\text {1 }}$ | 550 |  | 199.4 |
| $600{ }^{1)}$ | 645 |  | 365.0 |
| $700{ }^{1)}$ | 720 | 30 | 449.0 |
| $800{ }^{1)}$ | 800 |  | 613.0 |

${ }^{1}$ ) To manufacturer's standard


| DN | Dimensions [mm] |  | PFA [bar] | Weight [kg] ~ |
| :---: | :---: | :---: | :---: | :---: |
|  | $L_{u}$ | $\mathrm{I}_{u}$ |  |  |
| 80 | 248 | 38 | 100 | 8.1 |
| 100 | 253 | 43 |  | 9.7 |
| 125 | 274 | 49 | 64 | 15.1 |
| 150 | 299 | 55 |  | 18.4 |
| 200 | 331 | 66 |  | 29.2 |
| 250 | 260 | 75 | 50 | 37.8 |
| 300 | 265 | 90 |  | 50.2 |
| 350 | 270 | 100 |  | 52.0 |
| 400 | 278 | 110 | 40 | 76.7 |
| 500 | 300 | 135 |  | 97.0 |
| 600 | 357 | 155 |  | 163.0 |
| 700 | 420 | 190 | 30 | 336.0 |
| 800 | 455 | 205 |  | 460.0 |
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MK 11 fittings
$1114^{\circ}$ single socket bends
to manufacturer's standard


| DN | Dimensions [mm] |  | PFA [bar] | Weight [kg] ~ |
| :---: | :---: | :---: | :---: | :---: |
|  | $L_{u}$ | $\mathrm{I}_{4}$ |  |  |
| 80 | 240 | 30 | 100 | 7.6 |
| 100 | 243 | 33 |  | 9.8 |
| 125 | 261 | 36 | 64 | 14.0 |
| 150 | 284 | 40 |  | 18.0 |
| 200 | 311 | 46 |  | 27.0 |
| 250 | 255 | 50 | 50 | 37.8 |
| 300 | 260 | 60 |  | 47.0 |
| 350 | 235 | 65 |  | 46.0 |
| 400 | 238 | 70 | 40 | 66.9 |
| 500 | 250 | 85 |  | 83.2 |
| 600 | 287 | 95 |  | 163.0 |
| 700 | 340 | 110 | 30 | 249.0 |
| 800 | 375 | 125 |  | 286.0 |

## MK 30 fittings

$30^{\circ}$ single socket bends
to manufacturer's standard


| DN | Dimensions [mm] |  | PFA [bar] | Weight [kg] ~ |
| :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{L}_{u}$ | ${ }_{u}$ |  |  |
| 80 | 253 | 44 | 100 | 7.4 |
| 100 | 260 | 50 |  | 10.8 |
| 125 | 283 | 57 | 64 | 15.1 |
| 150 | 309 | 65 |  | 20.0 |
| 200 | 345 | 80 |  | 30.8 |
| 250 | 270 | 95 | 50 | 38.9 |
| 300 | 280 | 110 |  | 52.9 |
| 350 | 295 | 125 |  | 56.0 |
| 400 | 308 | 140 | 40 | 76.5 |
| 500 | 335 | 170 |  | 107.0 |
| 600 | 412 | 200 |  | 178.0 |
| 700 | 480 | 250 | 30 | 286.0 |
| 800 | 510 | 260 |  | 350.0 |
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U fittings
Collars
Collars
$=$


| DN | Joint | L. [mm] | PFA [bar] | Weight ${ }^{\text {[ }}$ [g] |
| :---: | :---: | :---: | :---: | :---: |
| 500 | Bolted gland | 200 | 25 | 119.3 |
| 600 |  | 210 |  | 162.7 |
| 700 |  | 220 | 16 | 210.3 |
| 800 |  | 230 |  | 249.9 |
| 900 |  | 240 |  | 305.0 |
| 1,000 |  | 250 |  | 386.0 |
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|  |  |  |  |  |

[^7]MQ fittings
$90^{\circ}$ single socket bends
to manufacturer's standard


| DN | Dimensions [mm] |  | PFA [bar] | Weight [kg] ~ |
| :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{L}_{u}$ | $\mathrm{I}_{u}$ |  |  |
| 80 | 312 | 102 | 100 | 9.0 |
| 100 | 333 | 123 |  | 11.2 |
| 125 | 374 | 49 | 64 | 18.4 |
| 150 | 419 | 174 |  | 25.4 |
| 200 | 491 | 226 |  | 43.8 |
| 250 | 583 | 280 | 50 | 76.1 |
| 300 | 660 | 330 |  | 83.2 |
| 350 | 580 | 410 |  | 139.0 |
| 400 | 625 | 430 | 40 | 186.3 |
| 500 | 715 | 550 |  | 235.4 |
| 600 | 805 | 645 |  | 314.0 |
| 700 | 900 | 720 | 30 | 473.0 |
| 800 | 1,080 | 800 |  | 644.5 |

## MMB fittings <br> All-socket tees with $90^{\circ}$ branch

to EN 545


| DN | dn | L. [mm] | [ [mm] | PFA [bar] | Weight [kg] |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 80 | $40^{12}$ | 170 | 80 | 40 | 10.5 |
|  | 80 |  | 85 | 64 | 13.7 |
| 100 | $40^{12}$ | 190 | 90 | 40 | 13.6 |
|  | 80 |  | 95 | 64 | 14.7 |
|  | 100 |  |  |  | 16.6 |
| 125 | $40^{12}$ | 170 | 100 | 40 | 15.1 |
|  | 80 |  | 105 | 64 | 16.5 |
|  | 100 | 195 | 110 |  | 17.8 |
|  | 125 | 225 | 110 |  | 19.9 |
| 150 | $40^{12}$ | 170 | 115 | 40 | 18.2 |
|  | 80 |  | 120 | 62 | 19.9 |
|  | 100 | 195 |  |  | 20.9 |
|  | 150 | 255 | 125 |  | 25.5 |
| 200 | $40^{122}$ | 200 | 140 | 40 | 29.5 |
|  | 80) |  | 145 | 50 | 30.0 |
|  | 100 |  |  |  | 31.0 |
|  | 150 | 255 | 150 |  | 41.0 |
|  | 200 | 315 | 155 |  | 44.6 |
| 250 | 801) | 200 | 170 | 43 | 44.4 |
|  | 100 |  | 175 |  | 45.3 |
|  | $125{ }^{1}$ |  | 175 |  | 45.5 |
|  | 150 | 260 | 180 |  | 50.4 |
|  | 200 | 315 | 185 |  | 54.4 |
|  | 250 | 375 | 190 |  | 63.9 |
| 300 | 80) | 205 | 195 | 40 | 55.5 |
|  | 100 | 205 | 200 |  | 57.0 |
|  | $150{ }^{11}$ | 320 | 200 |  | 60.7 |
|  | 200 | 320 | 205 |  | 64.4 |
|  | $250{ }^{11}$ | 430 | 210 |  | 79.6 |
|  | 300 | 430 | 215 |  | 89.4 |

[^8]


| DN | Joint | L | Dimensions $[\mathrm{mm}]$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 40 | Screwed <br> socket | 97 | 56 | Max. PFA <br> [bar] | Weight [kg] ~ | 16 |





Screw rings for $P$ socket plugs are used in conjunction with $P$ socket plugs for closing off screwed socket joints.



[^9]


34|The non-positive locking system - Chapter 3

Miscellaneous
Weld-on connections
for ductile iron pipes
Straight connections with female thread


R has to be adapted for pipes of other nominal sizes (DN's)

## Marking of fittings

All fittings produced by member companies of the "Fachgemeinschaft Gussrohrsysteme/European Association for Ductile Iron Pipe Systems (FGR/
EADIPS)" carry the "FGR" mark indicating
 that all the guidelines required for the award of the "FGR Quality Mark" have been complied with.

As well as this, all fittings are marked with their nominal sizes and bends are marked with their respective angles. Flanged fittings have the pressure ratings PN 16, 25 or 40 cast or stamped onto them. No
 pressure rating appears on flanged fittings for PN 10 or on any socket fittings.

To identify their material as "ductile iron", fittings are marked with three raised dots arranged in a triangle $(\bullet \bullet)$ on their outer surface. In special cases, there may be further markings which are specified as needing to be applied.

## 4 - FLANGED JOINTS, PIPES AND FITTINGS



## Introduction

The flanged joints described in this Chapter comply with EN 1092-2. The flanges may be integrally cast, bolted on or welded on.

Regardless of the material of which they are made, all flanges of the same DN and the same PN can be combined with one another. Shown on the following pages are flanged joints of the PN 10, PN 16, PN 25 and PN 40 pressure ratings.

PN 63 and PN 100 flanges are also possible. For further information on them see our leaflet entitled "Ductile iron pipe systems for Snow-making systems".

Fields of use/advantages
Flanged joints are restrained joints. Their primary field of use is above-ground pipeline laying, equipment in manholes, and building services. The standardised hole patterns also allow them to be used for transitions between different materials.

When buried pipelines are laid, flanges are used above all for the installation of shut-off devices.

PFA - allowable operating pressure

- the stated PN defines the allowable operating pressure (PFA)
- $\mathrm{PMA}=1.2 \times$ PFA (allowable maximum operating pressure for a short period, e.g. the period of a pressure surge)
- PEA $=1.2 \times$ PFA +5 (allowable site test pressure).


### 4.1 Flanged joints

Flanged joints
Measurements


Flanged joints for PN10 - PN63 to EN 1092-2 and for PN100 to EN 1092-1. Flanged joints produced to this norm can be connected with all other flanges with measurements to DIN 2501-1.

|  | Flange |  |  |  | Gasket |  | Screws |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DN | PN | $\emptyset \mathrm{D}$ | OK | a | $\emptyset G$ | c | Number | Thread | øL | SW |
| 50 | 10 | 165 | 125 | 19 | 99 | 3 | 4 | M 16 | 19 | 24 |
|  | 16 | 165 | 125 | 19 | 99 | 3 | 4 | M 16 | 19 | 24 |
|  | 25 | 165 | 125 | 19 | 99 | 3 | 4 | M 16 | 19 | 24 |
|  | 40 | 165 | 125 | 19 | 99 | 3 | 4 | M 16 | 19 | 24 |
|  | 63 | 180 | 135 | 28 | 99 | 3 | 4 | M20 | 23 | 30 |
|  | 100) | 195 | 145 | 30 | 99 | 3 | 4 | M 24 | 28 | 36 |
| 80 | 10 | 200 | 160 | 19 | 132 | 3 | 8 | M 16 | 19 | 24 |
|  | 16 | 200 | 160 | 19 | 132 | 3 | 8 | M16 | 19 | 24 |
|  | 25 | 200 | 160 | 19 | 132 | 3 | 8 | M 16 | 19 | 24 |
|  | 40 | 200 | 160 | 19 | 132 | 3 | 8 | M 16 | 19 | 24 |
|  | 63 | 215 | 170 | 31 | 132 | 3 | 8 | M20 | 23 | 30 |
|  | 100) | 230 | 180 | 32 | 132 | 3 | 8 | M24 | 28 | 36 |


|  | Flange |  |  |  | Gasket |  | Screws |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DN | PN | øD | 0k | a | ¢6 | c | Number | Thread | ø L | sw |
| 100 | 10 | 220 | 180 | 19 | 156 | 3 | 8 | M 16 | 19 | 24 |
|  | 16 | 220 | 180 | 19 | 156 | 3 | 8 | M16 | 19 | 24 |
|  | 25 | 235 | 190 | 19 | 156 | 3 | 8 | M20 | 23 | 30 |
|  | 40 | 235 | 190 | 19 | 156 | 3 | 8 | M 20 | 23 | 30 |
|  | 63 | 250 | 200 | 33 | 156 | 3 | 8 | M 24 | 28 | 36 |
|  | 100" | 265 | 210 | 36 | 156 | 3 | 8 | M 27 | 31 | 41 |
| 125 | 10 | 250 | 210 | 19 | 184 | 3 | 8 | M 16 | 19 | 24 |
|  | 16 | 250 | 210 | 19 | 184 | 3 | 8 | M 16 | 19 | 24 |
|  | 25 | 270 | 220 | 23,5 | 184 | 3 | 8 | M 24 | 28 | 36 |
|  | 40 | 270 | 220 | 23,5 | 184 | 3 | 8 | M 24 | 28 | 36 |
|  | 63 | 295 | 240 | 37 | 184 | 3 | 8 | M 27 | 31 | 41 |
|  | $100{ }^{10}$ | 315 | 250 | 40 | 184 | 3 | 8 | M30 | 34 | 46 |
| 150 | 10 | 285 | 240 | 19 | 211 | 3 | 8 | M20 | 23 | 30 |
|  | 16 | 285 | 240 | 19 | 211 | 3 | 8 | M20 | 23 | 30 |
|  | 25 | 300 | 250 | 26 | 211 | 3 | 8 | M 24 | 28 | 36 |
|  | 40 | 300 | 250 | 26 | 211 | 3 | 8 | M24 | 28 | 36 |
|  | 63 | 345 | 280 | 39 | 211 | 3 | 8 | M 30 | 34 | 46 |
|  | 100" | 355 | 290 | 44 | 211 | 3 | 12 | M 30 | 34 | 46 |
| 200 | 10 | 340 | 295 | 20 | 266 | 3 | 8 | M20 | 23 | 30 |
|  | 16 | 340 | 295 | 20 | 266 | 3 | 12 | M20 | 23 | 30 |
|  | 25 | 360 | 310 | 22 | 274 | 3 | 12 | M 24 | 28 | 36 |
|  | 40 | 375 | 320 | 30 | 284 | 3 | 12 | M27 | 31 | 41 |
|  | 63 | 415 | 345 | 46 | 284 | 3 | 12 | M 33 | 37 | 50 |
|  | 100) | 430 | 360 | 52 | 284 | 3 | 12 | M 33 | 37 | 50 |
| 250 | 10 | 400 | 350 | 22 | 319 | 3 | 12 | M20 | 23 | 30 |
|  | 16 | 400 | 355 | 22 | 319 | 3 | 12 | M24 | 28 | 36 |
|  | 25 | 425 | 370 | 24,5 | 330 | 3 | 12 | M 27 | 31 | 41 |
|  | 40 | 450 | 385 | 34,5 | 345 | 3 | 12 | M 30 | 34 | 46 |
|  | 63 | 470 | 400 | 50 | 345 | 3 | 12 | M33 | 37 | 50 |
|  | 100) | 505 | 430 | 60 | 345 | 3 | 12 | M36 | 40 | 55 |
| 300 | 10 | 455 | 400 | 24,5 | 370 | 4 | 12 | M 20 | 23 | 30 |
|  | 16 | 455 | 410 | 24,5 | 370 | 4 | 12 | M 24 | 28 | 36 |
|  | 25 | 485 | 430 | 27,5 | 389 | 4 | 16 | M 27 | 31 | 41 |
|  | 40 | 515 | 450 | 39,5 | 409 | 4 | 16 | M 30 | 34 | 46 |
|  | 63 | 530 | 460 | 57 | 409 | 4 | 16 | M33 | 37 | 50 |
|  | 100) | 585 | 500 | 68 | 409 | 4 | 16 | M 39 | 43 | 60 |
| 400 | 10 | 565 | 515 | 24,5 | 480 | 4 | 16 | M 24 | 28 | 36 |
|  | 16 | 580 | 525 | 28 | 480 | 4 | 16 | M 27 | 31 | 41 |
|  | 25 | 620 | 550 | 32 | 503 | 4 | 16 | M 33 | 37 | 50 |
|  | 40 | 660 | 585 | 48 | 535 | 4 | 16 | M36 | 40 | 55 |
|  | 63 | 670 | 585 | 65 | 535 | 4 | 16 | M39 | 44 | 60 |
|  | 100) | 715 | 620 | 78 | 535 | 4 | 16 | M 45 | 50 | 70 |
| 500 | 10 | 670 | 620 | 26,5 | 582 | 4 | 20 | M24 | 28 | 36 |
|  | 16 | 715 | 650 | 31,5 | 609 | 4 | 20 | M 30 | 34 | 46 |
|  | 25 | 730 | 660 | 36,5 | 609 | 4 | 20 | M 33 | 37 | 50 |
|  | 40 | 755 | 670 | 52 | 615 | 4 | 20 | M 39 | 44 | 60 |
|  | 63) | 800 | 705 | 68 | 602 | 4 | 20 | M 45 | 48 | 70 |
|  | 100" | 870 | 760 | 94 | 630 | 4 | 20 | M 52 | 56 | 80 |
| 600 | 10 | 780 | 725 | 30 | 685 | 4 | 20 | M 27 | 31 | 41 |
|  | 16 | 840 | 770 | 36 | 725 | 4 | 20 | M33 | 37 | 50 |
|  | 25 | 845 | 770 | 42 | 720 | 4 | 20 | M36 | 40 | 55 |
|  | 40 | 890 | 795 | 58 | 735 | 4 | 20 | M 45 | 50 | 70 |
| 700 | 10 | 895 | 840 | 32,5 | 800 | 4 | 24 | M 27 | 31 | 41 |
|  | 16 | 910 | 840 | 39,5 | 795 | 4 | 24 | M 33 | 37 | 50 |
|  | 25 | 960 | 875 | 46,5 | 820 | 4 | 24 | M 39 | 43 | 60 |
|  | 40 | 995 | 900 | 77 | 840 | 4 | 24 | M 45 | 48 | 70 |
| 800 | 10 | 1015 | 950 | 35 | 905 | 5 | 24 | M 30 | 34 | 46 |
|  | 16 | 1025 | 950 | 43 | 900 | 5 | 24 | M36 | 41 | 55 |
|  | 25 | 1085 | 990 | 51 | 930 | 5 | 24 | M 45 | 49 | 70 |
|  | 40 | 1140 | 1030 | 80 | 960 | 5 | 24 | M52 | 57 | 80 |
| 900 | 10 | 1115 | 1050 | 37,5 | 1005 | 5 | 28 | M 30 | 34 | 46 |
|  | 16 | 1125 | 1050 | 46,5 | 1000 | 5 | 28 | M 36 | 41 | 55 |
|  | 25 | 1185 | 1090 | 55,2 | 1030 | 5 | 28 | M 45 | 49 | 70 |
|  | 40 | 1250 | 1140 | 90 | 1070 | 5 | 28 | M 52 | 57 | 80 |
| 1000 | 10 | 1230 | 1160 | 40 | 1110 | 5 | 28 | M33 | 37 | 50 |
|  | 16 | 1255 | 1170 | 50 | 1115 | 5 | 28 | M 39 | 44 | 60 |
|  | 25 | 1320 | 1210 | 60 | 1140 | 5 | 28 | M 52 | 56 | 80 |
|  | 40 | 1360 | 1250 | 99 | 1180 | 5 | 28 | M52 | 57 | 80 |

[^10]
### 4.2 Flanged pipes

Ductile iron flanged pipes
PN 10, PN 16 and PN 25 double-flanged pipes
to EN 545
with puddle flange to manufacturer's standard


External protection:

> zinc coating plus finishing layer, puddle flange bare metal Internal protection: cement mortar lining (CML)


Larger DN's and higher PN's available on enquiry; When ordering, please state: L, L1, whether to be in the form of a flanged spigot, $\varnothing$ D if different from Table; puddle flanges can also be supplied in sections which can be welded-on on site. Minimum concrete class $\mathrm{C} 20 / 25$. Curing time of 3 days

### 4.3 Flanged fittings



| DN | Dimensions [mm] | Weight [kg] ~ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | PN10 | PN16 | PN25 | PN40 |
| 80 | 130 | 9.5 |  |  |  |
| 100 | 140 | 11.9 |  | 12.9 |  |
| 125 | 150 | 15.3 |  | 17.8 | 20.5 |
| 150 | 160 | 19.7 |  | 21.5 | 25.5 |
| 200 | 180 | 29 | 27.5 | 32.5 | 42 |
| 250 | 210 | 41.5 | 41 | 48 | 65.5 |
| 300 | 255 | 60 | 59 | 69.5 | 96.5 |
| 350 | 140 | 58 | 64 | 81 | 128 |
| 400 | 153 | 67 | 75.5 | 98 | 156.5 |
| 500 | 185 | 99 | 127 | 148 | 232 |
| 600 | 254 | 182 | 227 | 248 | 350 |
| 700 | 284 | 313 | 339 | 334 |  |
| 800 | 314 | 428 | 646 | 445 |  |


| DN | Dimensions [mm] | Weight [kg1 ~ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | PN10 | PN16 | PN25 | PN40 |
| 80 | 130 | 9.5 |  |  |  |
| 100 | 140 | 11.9 |  | 12.9 |  |
| 125 | 150 | 15.3 |  | 17.3 | 20.5 |
| 150 | 160 | 19 |  | 21.5 | 25.5 |
| 200 | 180 | 26 | 25 | 29.5 | 39 |
| 250 | 210 | 41.5 | 41 | 48 | 65.5 |
| 300 | 255 | 60 | 59.5 | 69.5 | 96.5 |
| 350 | 105 | 56 | 61.5 | 77 | 135.9 |
| 400 | 113 | 58 | 67.5 | 90 | 165.3 |
| 500 | 135 | 85 | 113 | 134 | 232.8 |
| 600 | 174 | 157 | 202 | 223 | 253.2 |
| 700 | 194 | 243 | 269 | 299 | - |
| 800 | 213 | 330 | 366 | 333 |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |

## FFK 30 fittings

$30^{\circ}$ double flanged bends
to EN 545


| DN | Dimensions [mm] | Weight [kg] ~ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | PN10 | PN16 | PN25 | PN40 |
| 80 | 130 | 9.5 |  |  |  |
| 100 | 140 | 11.9 |  | 12.9 |  |
| 125 | 150 | 15.3 |  | 17.8 | 20.5 |
| 150 | 160 | 19.5 |  | 19.5 | 25 |
| 200 | 180 | 29 | 27.5 | 32.5 | 42 |
| 250 | 210 | 41.5 | 40.5 | 48 | 65 |
| 300 | 255 | 59.5 | 59 | 69 | 96 |
| 350 | 165 | 65 | 71 | 88 | 138 |
| 400 | 183 | 73 | 82.5 | 106 | 163.5 |
| 500 | 220 | 109 | 137 | 158 | 256 |
| 600 | 309 | 212 | 257 | 278 | 284 |
| 700 | 346 | 360 | 386 | 430 | - |
| 800 | 383 | 493 | 529 | 674 |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |



| DN | Dimensions [mm] | Weight [kg] ~ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | PN10 | PN16 | PN25 | PN40 |
| 80 | 130 | 9.4 |  |  |  |
| 100 | 140/200* | 11.3 |  | 12.3* |  |
| 125 | 150 | 14.5 |  | 15.7 | 18.3 |
| 150 | 160 | 18.4 |  | 20.5 | 24.5 |
| 200 | 180 | 27.5 | 27 | 31 | 41.5 |
| 250 | 350 | 54.5 | 54 | 61.5 | 82 |
| 300 | 400 | 77.2 | 76.2 | 87.7 | 118.2 |
| 350 | 298 | 75.5 | 82 | 99 | 141 |
| 400 | 324 | 94.4 | 106.4 | 128.4 | 196.4 |
| 500 | 375 | 143.5 | 173.5 | 196.5 | 264.5 |
| 600 | 426 | 210 | 263 | 292 | 397 |
| 700 | 478 | 292.5 | 322.5 | 392.5 | - |
| 800 | 529 | 399.5 | 437.5 | 535.5 |  |
| 900 | 581 | 513 | 561 | 682 |  |
| 1,000 | 632 | 661 | 744 | 899 |  |

F fittings
Flanged spigots
nach EN 545


| DN | Dimensions [mm] |  | Weight[kg] ~ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | $\mathrm{d}_{1}$ | PN10 | PN16 | PN25 | PN40 |
| 80 | 350 | 98 | 7.5 |  |  |  |
| 100 | 360 | 118 | 8.5 |  | 10.4 |  |
| 125 | 370 | 144 | 12.4 |  | 13.1 | 14.3 |
| 150 | 380 | 170 | 15.6 |  | 16.6 | 17.5 |
| 200 | 400 | 222 | 24.6 | 24 | 24.5 | 29 |
| 250 | 420 | 274 | 32 | 31.5 | 36 | 45 |
| 300 | 440 | 326 | 43.2 | 42.7 | 47.7 | 63.2 |
| 350 | 460 | 378 | 52.3 | 55.3 | 64.3 | 85.3 |
| 400 | 480 | 429 | 64.3 | 70.3 | 81.3 | 115 |
| 500 | 520 | 532 | 93.9 | 109 | 121 | 154 |
| 600 | 560 | 635 | 133 | 159 | 173 | 226 |
| 700 | 600 | 738 | 179 | 194 | 228 | - |
| 800 | 600 | 842 | 226 | 245 | 294 | - |
| 900 | 600 | 945 | 272 | 295 | 356 | - |
| 1,000 | 600 | 1,048 | 328 | 369 | 447 | - |
|  |  |  |  |  |  |  |

Q fittings
90 ${ }^{\circ}$ double flanged bends
to EN 545



| DN ${ }_{1}$ | DN ${ }_{2}$ | Dimensions [mm] |  | Weight [kg] |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | L | I | PN10 | PN16 | PN25 | PN40 |
| 80 | $40^{0}$ | 330 | 155 | 14 |  |  |  |
|  | $50^{\prime \prime}$ |  | 160 | 1515.7 |  |  |  |
|  | 80 |  | 165 |  |  |  |  |
| 100 | $40^{\circ}$ | 360 |  | 18 |  | 18.1 |  |
|  | $50^{\circ}$ |  | 170 |  |  |  |  |
|  | 80 |  | 175 | $\begin{gathered} 17.1 \\ 18.4 \end{gathered}$ |  | 18.1 |  |
|  | 100 |  | 180 | 19 |  | 20.5 |  |
| 125 | 80 | 400 | 190 | $\begin{aligned} & 22.8 \\ & 23.8 \end{aligned}$ |  | 24.3 | $\begin{aligned} & 26.8 \\ & 28.3 \\ & 30.7 \\ & \hline \end{aligned}$ |
|  | 100 |  | 195 |  |  | 25.8 |  |
|  | 125 |  | 200 |  |  | 26.7 |  |
| 150 | 80 | 440 | 205 | 28.5 |  | 30.531.9 | 30.7 35 |
|  | 100 |  | 210 | 29.4 |  |  | 35 35.9 |
|  | 125 |  | 215 | 30.9 |  | 33.4 | 35.9 38.9 |
|  | 150 |  | 220 | 32.2 |  | 35.3 | 41.9 |
| 200 | 80 | 520 | 240 | 42.2 | 41.7 | 45.7 | 56.757.6 |
|  | 100 |  |  | 43.1451 | 42.6 | 47.1 |  |
|  | $125^{\circ}$ |  | 40 |  | 51 <br> 45.5 <br> 18 | 50.5 | 57.6 <br> 58 |
|  | 150 |  | 250 | 46 |  |  | 63 |
|  |  |  | 260 | 49.5 | 48.5 | 55 | 70.599 |
| 250 | 801 | 700 | 275 | 7267.6 | 71 | 79 |  |
|  | 120 <br>  <br> $1255^{\prime \prime}$ <br> 150 <br> 200 |  |  |  |  | 75.1 | 99 95.2 |
|  |  |  |  | 92 | 91 | 100 | 121 |
|  |  |  | 300 | $\frac{81}{75.2}$ | 80 | 89 | 111 |
|  |  |  | 325 |  | 74.2 | 84.2 | 109.7 |
|  | 250 |  | 350 | 81 | 80 | 91.5 | 121.5 |
| 300 | $80^{\prime \prime}$ | 800 | 290 |  | 97 |  | 142 |
|  | 100 <br> $150^{10}$ <br> 200 |  | 300 |  | 92.8 | 104.8 | 135.8 |
|  |  |  | $\begin{aligned} & 325 \\ & 350 \end{aligned}$ | $\frac{101}{102.4}$ | 100 | 112 |  |
|  |  |  |  |  | 101.4 | 114.4 | 151.4 |
|  | $\begin{aligned} & 250^{10} \\ & 300^{10} \end{aligned}$ |  | 400 | 113.9 | 112.9 | 128.9 | 175.9 |
|  |  |  | 375 | 117.4 | 113 | 128 | 168 |
| 350 | 100 | 850 | 325 | 115 | 121.5 | 138.5 | 181.5 |
|  | 200350 |  |  | 120.5 | 126.5 | 145.5 | 193.5 |
|  |  |  | 425 | 138.8 | 147.8 | 172.8 | 236.8 |
| 400 | $80^{10}$ | 900 | 350 | 154.4 | 167.4 | 173 | 240 |
|  | 100 |  |  | 158 | 173.2 | 174.4 | 241.4 |
|  | $150{ }^{\prime \prime}$ |  |  | 144 | 156 | 179 | 249 |
|  | 200 |  |  | 179.5 | 179.5 | 201.1 | 264.3 |
|  | 300" |  | 450 | $\begin{aligned} & 183 \\ & 182.5 \end{aligned}$ | 187.3 | 215 | 295 |
|  | 400 |  |  |  | 209.5 | 238.5 | 340.5 |
| 500 | $80^{\prime \prime}$ | 1,000 | 400 | 215.5 | 216 | 263 | 330 |
|  | 100 |  |  | 218.5 | 247 | 287 | 331 |
|  | 150" |  |  | 225.5 | 255.5 | 270 | 344 |
|  | 200 |  |  | 259 | 273.6 | 274 | 344 |
|  | 300 ${ }^{\prime \prime}$ |  |  |  | 267 | 287 | 373 |
|  | 400 |  | 500 | 266.9 | 327.4 | 337.1 | 427.7 |
|  | 500 |  |  | 29.7 | 298.2 | 337.3 | 449.7 |
| 600 | $80^{\prime \prime}$ | 1,100 | 450 | 335 | 366 | 351 | 445 |
|  | $100^{\circ}$ |  |  | 350.7 | 385.5 | 352 | 446 |
|  | 150 |  |  | 363.6 | 365 | 357 | 453 |
|  | 200 |  |  | 296.4 | 394.9 | 387 | 479 |
|  | $300{ }^{1}$ |  | 550 | 368 | 416.6 | 416 | 506 |
|  | 400 |  |  | 355 | 409 | 482.1 | 569 |
|  | $500^{\circ}$ |  |  | 370 | 435 | 468 | 598 |
|  | 600 |  |  | 388 | 488 | 455 | 634 |
| 700 | $10{ }^{1}$ | 650 | 525 | 310 | 336 | 458 | - |
|  | $150{ }^{\circ}$ |  |  | 310 | 336 | 458 |  |
|  | 200 |  |  | 339.3 | 377.1 | 470 |  |
|  | 3000 | 870 | 555 | 383 | 416 | 503 |  |
|  | 400 |  |  | 468.4 | 444.5 | 543.5 |  |
|  | 500" |  |  | 539.8 | 532 | 644 |  |
|  | 600" | 1,200 | 600 | 541.4 | 627.8 | 673 |  |
|  | 700 |  |  | 604 | 591 | 695 |  |
|  | $80^{11}$ |  | 570 | 407.5 | 445.5 | 537.5 |  |
|  | $100^{\prime \prime}$ | 690 | 570 | 398.5 | 452 | 539 |  |
|  | $150{ }^{\circ}$ | 690 | 580 | 438.2 | 409 | 543 |  |
|  | 200 |  | 585 | 448.7 | 455 | 550 |  |
| 800 | $300{ }^{\circ}$ | 910 | 600 | 547.6 | 518 | 613 |  |
|  | 400 | 910 | 615 | 556.2 | 553 | 655 | - |
|  | $500^{\circ}$ |  | 645 | 697.6 | 698 | 801 |  |
|  | 600 | 1,350 |  | 654.4 | 729 | 832 |  |
|  | $700^{\circ}$ |  | 675 | 679 | 731 | 856 |  |
|  | 800 |  |  | 716 | 720 | 927 |  |
|  | $100{ }^{\prime \prime}$ | 730 | 640 | 445 | 488 | 730 |  |
|  | 200 | 730 | 645 | 432 | 480 | 603 |  |
|  | 3000 | 950 | 660 | 544 | 588 | 690 |  |
| 900 | 400 |  | 675 | 532.5 | 585.5 | 717.5 | - |
|  | $500^{\prime \prime}$ |  | 690 | 784 | 842 | 960 |  |
|  | 600 | 1,500 | 705 | 771 | 846 | 981 |  |
|  | 900 |  | 750 | 818 | 890 | 1.071 |  |
|  | 150" | 770 | 705 | 561 | 640 | 790 |  |
|  | 200 |  |  | 564 | 643 | 793 |  |
|  | $300{ }^{1}$ | 990 | 735 | 645 | 724 | 879 |  |
|  | 400 |  |  | 657 | 738 | 899 |  |
| 1,000 | $500^{\prime \prime}$ |  |  | 951 | 1,055 | 1,225 | - |
|  | $700^{\prime \prime}$ |  |  | 989 | 1,082 1,102 | 1,243 1292 |  |
|  | 800" | 1,650 | 825 | 1,016 | 1,123 | 1,339 |  |
|  | 900) |  |  | 1,036 | 1,148 | 1,356 |  |
|  | 1,000 |  |  | 1,066 | 1,186 | 1,413 |  |



FFR fittings
Double flanged tapers
to EN 545


FFRe fittings
Eccentric double flanged tapers
to manufacturer's standard


| DN ${ }_{1}$ | dn | Dimensions [mm] | Weight [kg] |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | L | PN10 | PN16 | PN25 | PN40 |
| 50 | 40 | 200 | 7 |  |  |  |
| 65 | 40 | 200 | 8.5 |  |  |  |
|  | 50 |  |  |  |  |  |
| 80 | 40 | 200 | 9.2 |  |  |  |
|  | 50 |  | 9.7 |  |  |  |
|  | 65 |  | 10.7 |  |  |  |
| 100 | 40 | 200 | 11.1 |  | 11.6 |  |
|  | 50 |  | 12.1 |  | 12.1 |  |
|  | 65 |  | 12.6 |  | 12.6 |  |
|  | 80 |  | 13.1 |  | 13.1 |  |
| 125 | 50 | 200 | 13.6 |  | 14.2 | 16.1 |
|  | 65 |  | 14.6 |  | 15.1 | 16.4 |
|  | 80 |  | 15.6 |  | 16.2 | 17.5 |
|  | 100 | 300 | 16.5 |  | 17.1 | 18.4 |
| 150 | 50 | 300 | 17.9 |  | 21.5 | 23.5 |
|  | 80 |  | 19 |  | 23 | 25 |
|  | 100 |  | 20 |  | 24.5 | 26.5 |
|  | 125 |  | 25.5 |  | 25.5 | 29 |
| 200 | 80 | 300 | 24.4 | 25 | 27 | 33.5 |
|  | 100 |  | 24.5 | 24.5 | 28 | 34 |
|  | 125 |  | 25.5 | 25.5 | 29 | 35 |
|  | 150 |  | 29.5 | 29.5 | 31.5 | 38.5 |
| 250 | 100 | 300 | 35.5 | 35.5 | 39 | 49 |
|  | 125 |  | 36 | 36 | 39.5 | 50.5 |
|  | 150 |  | 40 | 40 | 42.5 | 51.5 |
|  | 200 |  | 42 | 42 | 48 | 64 |
| 300 | 100 | 300 | 40.5 | 40.5 | 45 | 60 |
|  | 150 |  | 42.5 | 46.1 | 59 | 82 |
|  | 200 |  | 53.1 | 53.1 | 63 | 87.5 |
|  | 250 |  | 55 | 55 | 66.5 | 94 |
| 350 | 200 | 500 | 82 | 85 | 99 | 122 |
|  | 250 |  | 83 | 85.5 | 101 | 128 |
|  | 300 |  | 108 | 114 | 125 | 162 |
| 400 | 150 | 500 | 81 | 90 | 102 | 138 |
|  | 200 | 600 | 85 | 85 | 110.5 | 150.5 |
|  | 250 | 500 | 91 | 102 | 123 | 163 |
|  | 300 |  | 105 | 104 | 124 | 183 |
|  | 350 |  | 117 | 126 | 145 | 200 |
| 500 | 250 | 500 | 114.5 | 127 | 140.5 | 186 |
|  | 300 |  | 115 | 135 | 153 | 204 |
|  | 350 |  | 120.5 | 141 | 158 | 207 |
|  | 400 |  | 162 | 162 | 194 | 194 |
| 600 | 300 | 500 | 182 | 193 | 212 | 288 |
|  | 400 |  | 196 | 241 | 252 | 345 |
|  | 500 |  | 236 | 252 | 262 | 357 |

## N fittings

Double flanged $90^{\circ}$ duckfoot bends
to EN 545


| DN | Dimensions [mm] |  |  | Weight [kg] ~ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | c | d | PN10 | PN16 | PN 25 | PN 40 |
| 80 | 165 | 110 | 180 | 13.2 |  |  |  |
| 100 | 180 | 125 | 200 | 16.9 |  | 17.9 |  |
| 125 | 200 | 140 | 225 | 22.1 |  | 23.1 | 26.1 |
| 150 | 220 | 160 | 250 | 28.8 |  | 30.8 | 35.8 |
| 200 | 260 | 190 | 300 | 46.2 | 45.2 | 49.7 | 60.2 |
| 250 | 350 | 225 | 350 | 73.5 | 72.5 | 80.5 | 101 |
| 300 | 400 | 255 | 400 | 103.9 | 102.9 | 113.9 | 144.9 |
| 350 | 450 | 290 | 450 | 136 | 142 | 158 | 201 |
| 400 | 500 | 320 | 500 | 176.4 | 186.4 | 209.4 | 277.4 |
| 500 | 600 | 385 | 600 | 281 | 311 | 335 | 402 |
| 600 | 700 | 450 | 700 | 425 | 478 | 506 | 612 |


| DN | b [mm] |  |  |  | Weight [kg] ~ |  |  |  | Optional bored hole(s) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | PN 10 | PN 16 | PN 25 | PN 40 | PN 10 | PN 16 | PN 25 | PN 40 | ["] |
| 40 | 16 |  |  |  | 2.5 |  |  |  | $1 x^{1 / 2 "}$ central |
| 50 | 16 |  |  |  | 3 |  |  |  |  |
| 65 | 16 |  |  |  | 4 |  |  |  |  |
| 80 | 16 |  |  |  | 3.6 |  |  |  | $1 \times 2$ " central |
| 100 | 16 |  |  |  | 4.3 |  | 4.8 |  |  |
| 125 | 16 |  |  | 20.5 | 5.6 |  | 6.2 | 7.9 |  |
| 150 | 16 |  | 17 | 23 | 7.2 |  | 8.3 | 11.1 |  |
| 200 | 17 |  | 19 | 27 | 11 | 10.8 | 13.3 | 20 |  |
| 250 | 19 |  | 21.5 | 31 | 16.9 | 16.6 | 21 | 33.5 |  |
| 300 | 20.5 |  | 23.5 | 35.5 | 26 | 25.5 | 32 | 51.5 | $2 \times 2$ eccentric |
| 350 | 20.5 | 22.5 | 26 | 40) | 33 | 37 | 46 | 73.5 |  |
| 400 | 20.5 | 24 | 28 | 44) | 41 | 49 | 62.5 | 106 |  |
| 500 | 22.5 | 27.5 | 32.5 | $48^{17}$ | 65 | 85.5 | 102 | 151 |  |
| 600 | 25 | 31 | 37 | $53^{1}$ | 99.5 | 136 | 159 | 230 |  |
| 700 | 27.5 | 34.5 | 41.5 ${ }^{\text { }}$ | - | 147 | 179 | 225 | - |  |
| 800 | 30 | 38 | 461) | - | 207 | 252 | 325 | - |  |
| 900 | 32.5 | 41.5 | 50.5 ${ }^{1}$ | - | 273 | 335 | 429 | - |  |
| 1,000 | 35 | 45 | 55 ${ }^{1}$ | - | 360 | 453 | 578 | - |  |

As well as this, all fittings are marked with their nominal sizes and bends are marked with their respective angles. Flanged fittings have the nominal pressures PN 16, 25 or 40 cast or stamped onto them. No nominal pressure appears on flanged fittings for PN 10 or on any socket fittings.

To identify their material as "ductile iron", fittings are marked with three raised dots arranged in a triangle $\left(\bullet^{\bullet}\right)$ on their outer surface. In special cases, there may be further markings which are specified as needing to be applied.
${ }^{1}$ ) To manufacturer's standard, flange connection dimensions to EN 1092-2; flanges for higher pressures available on enquiry

## Marking of fittings

All fittings produced by member companies of the "Fachgemeinschaft Gussrohrsysteme/European Association for Ductile Iron Pipe Systems (FGR/EADIPS) carry the "FGR" mark indicating that all the guidelines required for the award of the "FGR Quality Mark" have been complied with.

## DN 80 transition flanges

Flanges for PN 10 to PN 40 transitions
to manufacturer's standard


| DN | Dimensions [mm] |  | PN [bar] | Weight [kg] ~ |
| :---: | :---: | :---: | :---: | :---: |
|  | D | e |  |  |
| 80 | 200 | 27 | 10/40 | 3.9 |
|  |  |  |  |  |
|  |  |  |  |  |
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|  |  |  |  |  |



## 5 - COATINGS

## Preliminary remarks

In their as-supplied form, ductile iron pipes and fittings have factory-applied internal and external coatings. The various coatings available for pipes can be selected to suit a wide variety of factors and can be combined almost as desired.

Some of the crucial influencing factors are as follows:

- the medium to be carried
- the corrosiveness of the soil and groundwater
- the grain size of the bedding
- the temperature of the medium
- the ambient temperature
- the installation technique

The structure, operation and fields of use of the various internal and external coatings available for pipes are described in the following Chapter.

For fittings, what has shown itself to be the state of the art internal and external coating is the epoxy coating to EN 14901 . Fittings with this coating can be used both for the supply of drinking water and for the disposal of sewage and other wastewater. Other coatings such as a cement mortar lining, enamelling or bitumen are possible on enquiry.


### 5.1 External coatings

## Zinc coating with polyurethane finishing layer (PUR Longlife coating)

## Structure

A zinc coating with a polyurethane (PUR) finishing layer is available for 5 m laying length pipes of nominal sizes from DN 80 to DN 500 and for all push-in joints. The finishing layer consists of polyurethane.

It complies with Austrian Ö-NORM B 2560 and is available in the following colours:

- blue for drinking water
- black for snow-making systems and turbine pipelines Other colours are available on enquiry.

The mean thickness of the finishing layer is $120 \mu \mathrm{~m}$. Below the finishing layer there is a zinc coating with a mass of at least $200 \mathrm{~g} / \mathrm{m}^{2}$.

If there is damage to the corrosion protection which extends down to the surface of the ductile iron, an electrochemical cell, a so-called macrocell, forms at the damaged point. When metals are arranged in the electrochemical series, zinc is a less noble metal than iron; it has a more negative electrode potential and if it is in conductive contact with iron and an electrolyte is present it goes into solution. In electrochemical terms, the exposed surface of the ductile iron thus forms a cathode and the zinc-coated surface of the pipe an anode. Zinc ions migrate to the damaged point and form a layer of "scarring" which stops the corrosion.


Cathodic protective action of the zinc at injuries to the protective layer

When pipes are laid in the ground, over the course of time the layer of zinc changes into a dense, firmly adhering, impermeable and uniformly crystalline layer of insoluble compounds consisting of zinc oxides, hydrates and zinc salts of different compositions. Although the exchange processes between the zinc and the ground are hampered by the porous finishing layer, they are not completely suppressed and in a spatially confined region conditions are created for a slow conversion which encourages salts to crystallise out.
Even though the metallic zinc which was originally present has been converted, this layer of products of the corrosion of the zinc maintains the protective action.

In anaerobic soils in which bacterial corrosion by sulphate-reducing bacteria may occur, zinc provides additional protection as a result of its antibacterial action and its ability to increase the pH at the interface between the ductile iron and the soil.

## Fields of use

- Under Austrian ÖNORM B 2538, the allowable grain size of the pipe bedding material is limited to 100 mm
- With regard to the corrosiveness of the bedding material, the present external coating can be assumed to be comparable to the zinc coating and reinforced finishing layer under EN 545. Many soils are permitted as pipe bedding materials in this case but the following are exceptions
- soils with a low resistivity of less than 1,000 ohms $x$ cm when installation is above the water table or one of less than 1,500 ohms $\times \mathrm{cm}$ when installation is below the water table
- mixed soils, i.e. soils made up of two or more different types of soil
- soils with a pH of less than 6 and a high base-neutralising capacity
- soils which contain refuse, cinders or slag or which are polluted by wastes or industrial effluents.
Further information on the present subject can be found in Chapter 8.


## Operation

There are three factors on which the protective action of the zinc coating with a finishing layer is based:

- the electrochemical action of the zinc
- a reduction in any subsequent diffusion of the attacking medium. caused by the products of reaction of the zinc which form and which are insoluble in water
- the anti-bacterial action of zinc salts


### 5.2 External coatings PUR-TOP premium coating

The PUR-TOP finishing layer is an enhanced version of the PUR Longlife finishing layer. The PUR finishing layer is increased to a thickness of $400 \mu \mathrm{~m}$ and it also has a polyethylene bandage for protection against impacts wound round it. The thickness of the impact protection bandage is $\geq 0.65 \mathrm{~mm}$.

With regard to the corrosiveness of the bedding material, the PUR TOP coating constitutes a reinforced coating under EN 545. Soils of any desired corrosiveness are thus possible as bedding materials.

PE tape protection
Enhanced polyurethane finishing layer (min. 400 4 m )

## Installation instructions

The directions given in Chapter 8 relating to bedding materials and the cutting of pipes should be followed. Special requirement for PUR TOP coatings.

Before pipes with PUR TOP coatings are cut, the polyethylene bandage must be removed by pulling it off for a length of 2 L or 2LS, as the case may be, as shown in the Table below (for collars, allowance must also be made for the dimension for sliding on the collar).


| DN | TYTON $^{\oplus} /$ | VRS $^{\oplus}-\mathrm{T}$ |
| :---: | :---: | :---: |
|  | $\mathrm{L}(\mathrm{mm})$ | $\mathrm{L}_{\mathrm{s}}(\mathrm{mm})$ |
| 80 | 95 | 165 |
| 100 | 100 | 175 |
| 125 | 100 | 185 |
| 150 | 105 | 190 |
| 200 | 110 | 200 |
| 250 | 115 | 205 |
| 300 | 120 | 210 |
| 350 | 120 | - |
| 400 | 120 | 230 |
| 500 | 130 | 245 |

Once the pipe joint has been assembled, the region in which the joint is situated should be covered with a shrink-on sleeve.

### 5.3 External coatings <br> Zinc coating with epoxy layer

## Structure

A zinc coating with a finishing layer is available for 6 m laying length pipes of nominal sizes from DN 80 to DN 1000 and for all push-injoints. The finishing layer may consist of epoxy paint or bitumen.

It complies with EN 545 and is available in the following colours:

- blue for drinking water
- green for non-drinking water
- black (bitumen) for snow-making systems and turbine pipelines

Other colours are available on enquiry.

The mean thickness of the finishing layer is $70 \mu \mathrm{~m}$. Below the finishing layer there is a zinc coating with a mass of at least $200 \mathrm{~g} / \mathrm{m} 2$.

## Operation

There are three factors on which the protective action of the zinc coating with a finishing layer is based:

- the electrochemical action of the zinc
- a reduction in any subsequent diffusion of the attacking medium, caused by the products of reaction of the zinc which form and which are insoluble in water
- the anti-bacterial action of zinc salts

If there is damage to the corrosion protection which extends down to the surface of the ductile iron, an electrochemical cell, a so-called macrocell, forms at the damaged point. When metals are arranged in the electrochemical series, zinc is a less noble metal than iron; it has a more negative electrode potential and if it is in conductive contact with iron and an electrolyte is present it goes into solution. In electrochemical terms, the exposed surface of the ductile iron thus forms a cathode and the zinc-coated surface of the pipe an anode. Zinc ions migrate to the damaged point and form a layer of "scarring" which stops the corrosion.


Cathodic protective action of the zinc at injuries to the protective layer

When pipes are laid in the ground, over the course of time the layer of zinc changes into a dense, firmly adhering, impermeable and uniformly crystalline layer of insoluble compounds consisting of zinc oxides, hydrates and zinc salts of different compositions. Although the exchange processes between the zinc and the ground are hampered by the porous finishing layer, they are not completely suppressed and in a spatially confined region conditions are created for a slow conversion which encourages salts to crystallise out. Even though the metallic zinc which was originally present has been converted, this layer of products of the corrosion of the zinc maintains the protective action.

In anaerobic soils in which bacterial corrosion by sulphate-reducing bacteria may occur, zinc provides protection as a result of its antibacterial action and its ability to increase the pH at the interface between the ductile iron and the soil.

## Fields of use

Pipes with a zinc coating are used above all in applications where an exchange of soil is intended. There are two main factors which may dictate such an exchange:

- Under DVGW W 400-2, Anhang G, the allowable grain size of the pipe bedding material is limited to 0 to 32 mm (rounded grains) or 0 to 16 mm (fragmented grains)
- Many soils are permitted as pipe bedding materials under EN 545 but the following are exceptions
- soils with a low resistivity of less than 1,500 ohms $\times \mathrm{cm}$ when installation is above the water table or one of less than 2,500 ohms x cm when installation is below the water table
- mixed soils, i.e. soils made up of two or more different types of soil
- soils with a pH of less than 6 and a high base-neutralising capacity
- soils which contain refuse, cinders or slag or which are polluted by wastes or industrial effluents.

A thicker finishing layer with a local minimum thickness of $100 \mu \mathrm{~m}$ is able to widen the field of use to cover a soil resistivity of 1,000 ohms $x \mathrm{~cm}$ when installation is above the water table and one of 1,500 ohms $\times \mathrm{cm}$ when it is below the water table.

Further information on the present subject can be found in Chapter 8.

## Installation instructions

The directions given in Chapter 8 relating to bedding materials and the cutting of pipes should be followed.

### 5.4 External coatings <br> Zinc-aluminium coating with finishing layer (Zinc Plus)

Structure
A zinc-aluminium coating with a finishing layer is available for 6 m laying length pipes of nominal sizes from DN 80 to DN 1,000 and for all push-in joints. The finishing layer consists of blue epoxy paint and complies with EN 545. Other colours are available on enquiry.
The mean thickness of the finishing layer is $70 \mu \mathrm{~m}$. Below the finishing layer there is a zinc-aluminium coating ( $85 \%$ zinc and $15 \%$ aluminium) with a mass of at least $400 \mathrm{~g} / \mathrm{m}^{2}$.

Operation
There are three factors on which the protective action of the zinc-aluminium coating with a finishing layer is based:

- the electrochemical action of the zinc
- a reduction in any subsequent diffusion of the attacking medium. caused by the products of reaction of the zinc which form and which are insoluble in water
- the anti-bacterial action of zinc salts

If there is damage to the corrosion protection which extends down to the surface of the ductile iron, an electrochemical cell, a so-called macrocell, forms at the damaged point. When metals are arranged in the electrochemical series, zinc is a less noble metal than iron; it has a more negative electrode potential and if it is in conductive contact with iron and an electrolyte is present it goes into solution. In electrochemical terms, the exposed surface of the ductile iron thus forms a cathode and the zinc-coated surface of the pipe an anode. Zinc ions migrate to the damaged point and form a layer of "scarring" which stops the corrosion.


Cathodic protective action of the zinc at injuries to the protective layer

When pipes are laid in the ground, over the course of time the layer of zinc changes into a dense, firmly adhering, impermeable and uniformly crystalline layer of insoluble compounds consisting of zinc oxides, hydrates and zinc salts of different compositions. Although the exchange processes between the zinc and the ground are hampered by the porous finishing layer, they are not completely suppressed and in a spatially confined region conditions are created for a slow conversion which encourages salts to crystallise out.

Even though the metallic zinc which was originally present has been converted, the layer of products of the corrosion of the zinc maintains the protective action.

To delay the effect of this conversion for as long as possible, and thus to maintain the protective electrochemical action, the zinc has a $15 \%$ proportion of aluminium added to it. This and the increase in the total mass of zinc produces a further rise in the technical operating life which can be expected and an extension of the fields of use.

In anaerobic soils in which bacterial corrosion by sulphate-reducing bacteria may occur, zinc provides additional protection as a result of its antibacterial action and its ability to increase the pH at the interface between the ductile iron and the soil.

## Fields of use

Pipes with a zinc-aluminium coating (Zinc Plus) are used above all in applications where an exchange of soil is intended. Such an exchange is dictated mainly by the allowable grain sizes.

Under DVGW W 400-2, the allowable grain size of the pipe bedding material is limited to 0 to 32 mm (rounded grains) or 0 to 16 mm (fragmented grains).

Few limits are set in respect of the corrosiveness of the pipe bedding material and the only soils which are ruled out under EN 545 are the following:

- acidic peaty soils
- soils which contain refuse, cinders or slag or which are polluted by wastes or industrial effluents
- soils below sea level whose resistivity is less than 500 ohms $\times \mathrm{cm}$.

In soils of these kinds, and also where stray currents occur, it is advisable for pipes with a cement mortar coating to be used.

Further information on the present subject can be found in Chapter 8.

Installation instructions
The directions given in Chapter 8 relating to bedding materials and the cutting of pipes should be followed.

### 5.5 External coatings <br> Cement mortar coating

## Structure

The cement mortar coating (ZMU) is available for 6 m laying length pipes of nominal sizes from DN 80 to DN 1,000 and for all push-in joints. It complies with EN 15 542. The nominal layer thickness is therefore 5 mm . Below the ZMU there is always a zinc coating of a mass of at least $200 \mathrm{~g} / \mathrm{m} 2$.
An additional primer may be applied between the zinc and the ZMU but this can be dispensed with if the ZMU is of the polymer-modified type. The cement mortar is applied by an extrusion process (winding-on) or a spraying process. The sockets are protected by rubber protective sleeves or shrink-on material (see Chapter 6, p. 51).

For special conditions of use, such for example as for trenchless installation in non-cohesive soils, we can also supply our ZMU Plus coating. In this case the pipe is sheathed with cement mortar to a depth sufficient to give it an entirely cylindrical external outline.

## Operation

The ZMU is highly effective in providing corrosion protection and protects against both chemical and mechanical attack.
The protective action against chemicals is based above all on the porosity and alkalinity of the mortar used, which is based on blast furnace cement. When the mortar is acted on by groundwater or the soil moisture, what is produced, in time, at the surface of the ductile iron pipe is a $\mathrm{pH}>10$, which is a reliable means of stopping corrosion from occurring.
In the unlikely event of the ZMU being damaged mechanically, the corrosion protection is maintained by the zinc coating situated below the ZMU.

In addition to this, the allowable mechanical loads are laid down by stipulations relating to them in EN 15 542. Standardised figures are given for, amongst other things, strength of adhesion and impact resistance. The consequence is that the ZMU has an outstanding ability to carry mechanical loads.

Fields of use
Because of the excellent mechanical and chemical protective properties of the ZMU, pipes with an external coating of this kind can be used almost anywhere. Some of the significant fields of use are:

- corrosive/contaminated soils

Under Annex D of EN 545, ductile iron pipes with a fibre-reinforced cement mortar coating to EN 15542 can be installed in soils of any desired corrosiveness.

- coarse grained pipe bedding material

DVGW directive W 400-2 regulates the allowable grain sizes of the pipe bedding material. Under Anhang $G$ to this directive, a maximum grain size of 100 mm , where the grains are of a rounded or fragmented form, is allowable for pipes with a cement mortar coating.

- trenchless installation techniques

The trenchless installation techniques for which ductile iron pipes are relevant are regulated in DVGW directives GW 320-1 to GW 324. Under these documents, pipes with a cement mortar coating are approved for all such techniques.

- stray currents

The latest investigations indicate that ductile iron pipes with a cement mortar coating should be used in areas subject to stray currents. In this way, by installing joints which are not electrically conductive, stray currents can be stopped from having an adverse effect on the pipeline.


### 5.6 Internal coatings

## Operation

The cement mortar lining has both an active and a passive protective action. The active action is based on an electrochemical process. Water penetrates into the pores of the cement mortar. When this happens the pH of the water rises to a level of more than 12 as a result of the absorption of free lime from the mortar. It is impossible for ductile iron to corrode in this pH range. The passive action results from the physical separation which exists between the pipe's ductile iron wall and the water.

## Fields of use

Ductile iron pipes with a cement mortar lining based on blast furnace cement or Portland cement can be used to transport all types of water for human consumption which comply with EU Council Directive 98/83/EC. For other types of water such as raw water for example, the limits governing use are given in the Table below as a function of the type of cement used for the lining.

| Water characteristics | Portland cement | Blast furnace cement | High-alumina <br> cement |
| :--- | :---: | :---: | :---: |
| Minimum pH | $6-12$ | $6-12$ | $4-10$ |
| Maximum content <br> (mg/l) of: <br> - corrosice $\mathrm{CO}_{2}$ |  |  |  |
| - sulphate $\left(\mathrm{SO}_{4}^{-}\right)$ |  |  |  |
| - magnesium $\left(\mathrm{Mg}^{+}\right)$ | 7 | 15 | Unlimited |
| - ammonium $\left(\mathrm{NH}_{4}^{+}\right)$ | 100 | 30000 | Unlimited |

Repairing the cement mortar lining
On-site repairs to the cement mortar lining (ZMA)
All repairs to any damaged parts of the ZMA must be carried out using the repair kit supplied by the pipe manufacturer.

Contents of the repair kit:
approx. 5 kg of sand/cement mixture
approx. 1 litre of diluted additive.

These components are specially adjusted for use with Duktus drinking water pipes.
They must not be replaced by any other material or used to produce classes of cement mortar different from those specified on the repair kit.

## Repair instructions

A proper repair can only be made at temperatures of above $5^{\circ} \mathrm{C}$.
Apart from the repair kit, what you will also need are:

Rubber gloves
Dust-tight protective goggles
Wire brush
Spatula
Additional mixing vessel
Possibly drinking water for mixing

If there is severe damage:
Hammer
Cold chisel

Preparing the damaged area
If there is only slight surface damage, simply remove any loose pieces of cement mortar and any pieces which are not firmly attached with the wire brush.

Finally, moisten the damaged area. If the damage is severe, it is advisable for the cement mortar to be completely removed (down to the bare metal) in the damaged area with a hammer and cold chisel. The protective goggles must be worn when doing the above!

Remove the cement mortar in such a way that square edges are obtained:

## RIGHT

Damaged area


WRONG

## Damaged area



Do not use excessive force when removing the cement mortar as this may cause the sound cement mortar to become detached in the region next to the damaged area. Remove any loose material which is still present with the wire brush and moisten the damaged area.

## Mixing

First of all stir the diluted additive well. Then mix the mortar, adding as little additive and water as possible, until a mixture which can be applied easily with the spatula is obtained - the amount of water contained in the additive is normally all that is needed. To begin with, use only the additive solution and meter it in carefully. Then add extra water if necessary (e.g. at high temperatures in summer).

## Application

Once the mortar is easily workable, fill the damaged area with it and level off the surface. Finally, smooth the repaired area, and especially the parts at the edges, with a moistened, wide paintbrush or a moistened dusting brush.

Drying, installation and entry into service
Pipes can be installed immediately; however, the repaired areas are not capable of withstanding any mechanical loads (e.g. impacts, vibration, etc.) until after about an hour, and significantly later in cold, damp weather.

A pipeline must not be put into service until at least 12 hours after a repair.


## 6 - ACCESSORIES

Laying tools and other accessories for pipes and fittings with TYTON ${ }^{\oplus}$,
BRS ${ }^{\oplus}$ or VRS $^{\oplus}-\mathrm{T}$ push-in joints
The following laying tools and other accessories are needed for laying and assembling pipes and fittings:
Note: a chain-hoist traction assembly must be used for assembling
BRS ${ }^{\circledR}$ push-in joints of DN 350 size and above!
Laying tools

${ }^{11}$ Use chain-hoist traction assemblies for BRS® push-in joints of DN 350 size and above.


Laying tools for nominal sizes up to and including DN 400


| DN | Consisting of |  | Weight $[\mathrm{kg}] \sim$ |
| :---: | :---: | :---: | :---: |
|  | Type 1 | Type 2 |  |
| 80 |  |  | 14.0 |
| 100 |  |  | 15.0 |
| 125 |  |  | 15.5 |
| 150 | 1mounting clamp |  | 17.1 |
| 200 | 1 yoke | 2 mounting clamps | 18.1 |
| 250 | 2 levers | 2 levers | 20.5 |
| 300 |  |  | 23.5 |
| $350^{01}$ |  |  | 25.0 |
| $400^{0}$ |  |  |  |

${ }^{1}$ ) Use chain-hoist traction assemblies for $\mathrm{BRS}^{\circledR}$ push-in joints of DN 350 size and above.
Laying tool type 1 for DN 80 to DN 400 size pipes and fittings with a zinc or zincaluminium coating and a finishing layer (silver identifying marking).
Laying tool type 2 for DN 80 to DN 400 size pipes with a cement mortar coating (blue identifying marking).
Laying tool type 3 for DN 80 to DN 400 size pipes and fittings with thermal insulation (WKG) (red identifying marking).


Chain-hoist traction assemblies for nominal sizes from DN 350 to DN 1000


| DN | Consisting of | Weight [kg] ~ |
| :---: | :---: | :---: |
| 350" | $2 \times 30 \mathrm{kN}$ lever chain-hoists* 1 cable yoke 1 traction cable 1 mounting clamp | 92 |
| 4001 |  | 97 |
| 500 |  | 101 |
| 600 |  | 105 |
| 700 |  | 108 |
| 800 |  | 112 |
| 900 | $\begin{aligned} & 2 \times 50 \text { kN lever chain-hoists* } \\ & 1 \text { cable yoke } \\ & 1 \text { traction cable } \\ & 1 \text { mounting clamp } \end{aligned}$ | 115 |
| 1,000 |  | 119 |

* Obtainable from specialist suppliers
${ }^{10}$ Use chain-hoist traction assemblies for BRS ${ }^{*}$ push-in joints of DN 350 size and above.


## Other accessories

Dusting brush, cotton waste, wire brush, spatula, scraper (e.g. bent screwdriver), paint brush, lubricant, depth gauge.

For cutting of pipes
Use a disc cutter or grinder fitted with a cutting disc for stone, e.g. the C24RT Spezial type. For bevelling the spigot end use a coarse-grain grinding disc.

Laying tools and other accessories for pipes and fittings with BLS ${ }^{\oplus}$ VRS ${ }^{\oplus}$-T push-injoints
As well as the usual laying tools and other accessories, the followingmay also be needed when pipes and fittings with VRS ${ }^{\oplus}$-T push-in joints are being laid.

| DN | Accessory | Used for |
| :---: | :---: | :---: |
| 80 bis 500 | Torque wrench able to apply <br> a torque of at least 50 kN | Tightening the bolts of a clamping ring |
| 80 bis 1000 | Copper guide of the appropriate <br> nominal size to guide the welded bead | Re-application of welded bead <br> (e.g. to cut pipes) |

Laying tools and other accessories for fittings with screwed socket and bolted gland joints
The following laying tools and other accessories are needed forassembling fittings with screwed socket and bolted gland joints.

Laying tools


Other accessories:
Dusting brush, wire brush, spatula, chalk, hammer, paint brush, lubricant.

Laying tools and other accessories for fittings with screwed socket joints

| Hook spanner |
| :--- |
| DN |
| DN |
| Weight [kg] ~ |
| DN |

One-piece shrink-on sleeves for pipes with a cement mortar coating (ZMU) and TYTON ${ }^{\oplus}$, BRS ${ }^{\oplus}$ or VRS $^{\oplus}-$ T push-in joints DN 80 to DN 500


| DN | Product designation |  |  |  | Dimensions [mm] |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Product | Loading class | Width L | Nominal size (DN) | L | ØD/Ød) |
| 80 | MPSM | C30 | or $\begin{aligned} & 300 \\ & \\ & 300\end{aligned}$ | DN XXX | 300 | 200/80 |
| 100 |  |  |  |  | 300 | 235/100 |
| 125 |  |  |  |  | 300 | 280/135 |
| 150 |  |  |  |  | 300 | 280/135 |
| 200 |  |  |  |  | 300 | 340/205 |
| 250 | PMO | C30 |  | DN XXX | 300 | 405/243 |
| 300 |  |  |  |  | 300 | 460/275 |
| 350 |  |  |  |  | 300 | 515/314 |
| 400 |  |  |  |  | 300 | 565/345 |
| 500 |  |  |  |  | 300 | 680/414 |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |

${ }^{1}$ ) $\emptyset \mathrm{D} / \varnothing \mathrm{d}=\sim$ in unshrunk state/smallest shrunken size; dimensions and degrees of shrinkage may vary slightly depending on the product; tape material should be used onjoints of DN 600 size and above

Pre-cut shrink-on sleeves of tape material with a sealing strip for pipes with a cement mortar coating (ZMU)
DN 600 to DN 1000


Width $\mathrm{L}=300 \mathrm{~mm}$ ( 12 inch) for TYTON*/BRS
Width $L=450 \mathrm{~mm}$ (17 inch) for BLS ${ }^{\circ}$

| DN | Product | Product designation |  | Nominal size | Dimensions [mm] |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Loading class |  |  | ZL" |
| 600 | MEPS C30 incl. WPCP IV $8 \times 12$ or $8 \times 17$ |  | 300 or 450 | DNXXX | 2.500 |
| 700 |  |  | 2.950 |  |
| 800 |  |  | 300 or 450 | DN XXX | 3.260 |
| 900 | $\begin{aligned} & \text { WLOX C30 } \\ & \text { incl. CLH-150-300 or 450 } \\ & \hline \end{aligned}$ |  |  |  | 3.600 |
| 1,000 |  |  | 3.960 |  |

[^11]Rubber sleeves for protecting cement mortar, for pipes with a cement mortar coating (ZMU) and TYTON ${ }^{\ominus}$, BRS $^{\circledR}$ or
VRS ${ }^{\oplus}$-T push-injoints


These are combination sleeves which will fit TYTON ${ }^{\oplus}$, BRS $^{\circledR}$ and $V R S^{\ominus}-T$ push-in joints.

| DN | Dimensions [mm] |
| :---: | :---: |
|  |  |
| 80 | 155 |
| 100 | 155 |
| 125 | 160 |
| 150 | 165 |
| 200 | 170 |
| 250 | 180 |
| 300 | 200 |
| 350 | 135 |
| 400 | 210 |
| 500 | 210 |
| 600 | 265 |
| 700 | 265 |
| 800 | 265 |
| 900 | 265 |
| 1,000 | 265 |

## 7 - SPECIAL PRODUCTS



### 7.1 External coatings <br> Thermally insulated ductile iron pipes and fittings (WKG)

## Structure of the WKG pipe system

The WKG pipe system consists of ductile iron pipes and socket bends (MMK, MMQ) to EN 545 (water) or EN 598 (sewerage) with TYTON ${ }^{\oplus}$ push-in joints to DIN 28603 which may be restrained if desired.

The pipes are enclosed in thermal insulation formed by a CFC-free rigid polyurethane (PUR) foam with an average density of $80 \mathrm{~kg} / \mathrm{m}^{3}$. This rigid foam is protected from the effects of the weather in one of two ways: for above-ground pipelines (FL), by folded spiral-seam outer tubing of galvanized steel to EN 1506 or, as an option, of stainless steel, or for buried pipelines (EL) with a small height of cover which are thus at risk of freezing, by an outer sleeve of high-density polyethylene (HDPE) to EN 253.


The gap in the area of the push-injoint is filled with a ring of soft polyethylene and is covered with a sheet-metal sleeve (in the case of the FL system) or with a shrinkon polyethylene bandage (in the case of the EL system).


## Operation

The insulation slows down the heat loss from the pipeline and hence from the drinking water it contains. In this way, even when the water stands still for quite long periods in the pipeline, it is possible for such periods to be waited out without the pipeline freezing. The exact periods depend on a variety of factors such as the ambient temperature, the temperature of the water, the thickness of the insulating layer and special local factors. The tables on $p .55$ provide an overview of possible heat loss times.
If these times are not long enough, it is possible for a trace heating system to be incorporated. This system consists of a self-limiting heating cable which is bonded to the pipe carrying the medium and which is switched on at the desired temperature by means of a thermostat. The number and heating capacity of the cables have to be matched to the particular circumstances.

## Fields of use

WKG pipes and fittings can be used anywhere where the pipeline can be expected to freeze. Some typical applications are the following:

- Bridge pipelines and pipelines laid above ground

Positive locking joint systems (VRS ${ }^{\oplus}-\mathrm{T}$ joints) should always be used in this case. The outer covering should be galvanized steel or stainless steel.

- Buried pipelines with small heights of cover

A polyethylene outer sleeve should be used in this case. The grain size of the bedding material should not exceed 0 to 40 mm (rounded grains) or 0 to 11 mm (fragmented material). There is no limit to the corrosiveness of the bedding material. All the types of joint can be used, as dictated by the particular conditions.


### 7.2 Product range

WKG pipes with TYTON ${ }^{\text {p }}$ push-in joints
to DIN 28 603, or, up to DN 600, BRS ${ }^{\oplus}$ restrained push-in joints
Folded spiral-seam outer tubing (FL) HDPE outer sleeve (EL)


| DN | Dimensions [mm] |  |  |  | Weight [kg] ~ ${ }^{\text {d }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ø品 | $\emptyset \mathrm{d}_{1}$ | L | $s_{0}$ | FL-pipe* | EL-pipe |
| 80 | 180 | 98 | 94 | 41.0 | 112 | 108 |
| 100 | 200 | 118 | 98 | 41.0 | 135 | 129 |
| 125 | 225 | 144 | 101 | 40.5 | 168 | 159 |
| 150 | 250 | 170 | 104 | 40.0 | 207 | 195 |
| 200 | 315 | 222 | 110 | 46.5 | 276 | 261 |
| 250 | 400 | 274 | 115 | 63.0 | 369 | 366 |
| 300 | 450 | 326 | 120 | 62.0 | 453 | 456 |
| 400 | 560 | 429 | 120 | 65.5 | 683 | 696 |
| 500 | 710 | 532 | 130 | 89.0 | 966 | 983 |
| 600 | 800 | 635 | 130 | 82.5 | 1,218 | 1,266 |
| 700 | 900 | 738 | 172 | 81.0 | 1,548 | 1,614 |
| 800 | 1,000 | 842 | 184 | 79.0 | 1,896 | 1,974 |

${ }^{1}$ "Total weight; other nominal sizes, insulating layers of other thicknesses and trace heating are available on enquiry. * Where pipes are intended for use in above-ground pipelines it is essential to consult our Applications Engineering Division.

WKG pipes with VRS ${ }^{\oplus}$-T push-in joints
Folded spiral-seam outer tubing (FL)
HDPE outer sleeve (EL)


| DN | Dimensions [mm] |  |  |  | Weight [kg] ~ ${ }^{\text {) }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ØDa | $\emptyset \mathrm{d}_{1}$ | L | $\mathrm{S}_{\mathrm{D}}$ | FL-pipe | EL-pipe |
| 80 | 180 | 98 | 207 | 41.0 | 121 | 110 |
| 100 | 225 | 118 | 215 | 53.5 | 149 | 140 |
| 125 | 250 | 144 | 223 | 53.0 | 180 | 171 |
| 150 | 280 | 170 | 230 | 55.0 | 212 | 204 |
| 200 | 355 | 222 | 240 | 66.5 | 300 | 288 |
| 250 | 400 | 274 | 265 | 63.0 | 383 | 378 |
| 300 | 450 | 326 | 270 | 62.0 | 476 | 471 |
| 400 | 560 | 429 | 290 | 65.5 | 705 | 715 |
| 500 | 710 | 532 | 300 | 89.0 | 986 | 1,003 |
| 600 | 800 | 635 | 280 | 82.5 | 1,266 | 1,314 |
| 700 | 900 | 738 | 302 | 81.0 | 1,632 | 1,698 |
| 800 | 1,000 | 842 | 314 | 79.0 | 2,004 | 2,082 |

[^12]Dimension and weights of pipes of 5 m laying length are available on enquiry

WKG socket bends (MMK) with TYTON ${ }^{\oplus}$ push-in joints or, up to DN 600, BRS ${ }^{\oplus}$ restrained push-in joints
Folded spiral-seam outer tubing (FL)/HDPE outer sleeve (EL)


| DN | Ø Da | Dimensions L [mm] |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} \text { MMK } \\ 11^{\circ} \end{gathered}$ | $\begin{aligned} & \text { MMK } \\ & 22^{\circ} \end{aligned}$ | $\begin{gathered} \text { MMK } \\ 30^{\circ} \end{gathered}$ | $\begin{aligned} & \text { MMK } \\ & 45^{\circ} \end{aligned}$ | $\begin{aligned} & \text { MMQ } \\ & \left(90^{\circ}\right) \end{aligned}$ |
| 80 | 180 | 30 | 40 | 45 | 55 | 100 |
| 100 | 200 | 30 | 40 | 50 | 65 | 120 |
| 125 | 225 | 35 | 50 | 55 | 75 | 145 |
| 150 | 250 | 35 | 55 | 65 | 85 | 170 |
| 200 | 315 | 40 | 65 | 80 | 110 | 220 |
| 250 | 400 | 50 | 75 | 95 | 130 | 270 |
| 300 | 450 | 55 | 85 | 110 | 150 | 320 |
| 400 | 560 | 65 | 110 | 140 | 195 | 430 |
| 500 | 710 | 75 | 130 | 170 | 240 | 550 |
| 600 | 800 | 85 | 150 | 200 | 285 | 645 |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |

Other nominal sizes, insulating layers of other thicknesses and trace heating are available on
enquiry. Other types of fitting have to be insulated by the installer. * Where BRS* push-in joints are
intended for use in above-ground pipelines it is essential to consult our Applications Engineering Division.

WKG socket bends (MMK) with VRS®-T push-in joints
Folded spiral-seam outer tubing (FL)/HDPE outer sleeve (EL)


| DN | $\emptyset \mathrm{Da}$ | Dimensions L ${ }_{\text {L }}$ [mm] |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} \hline \text { MMK } \\ 11^{\circ} \end{gathered}$ | $\begin{aligned} & \text { MMK } \\ & 22^{\circ} \end{aligned}$ | $\begin{gathered} \text { MMK } \\ 30^{\circ} \end{gathered}$ | $\begin{aligned} & \hline \text { MMK } \\ & 45^{\circ} \end{aligned}$ | $\begin{aligned} & \hline \text { MMQ } \\ & \left(90^{\circ}\right) \end{aligned}$ |
| 80 | 180 | 30 | 40 | 45 | 55 | 100 |
| 100 | 225 | 30 | 40 | 50 | 65 | 120 |
| 125 | 250 | 35 | 50 | 55 | 75 | 145 |
| 150 | 280 | 35 | 55 | 65 | 85 | 170 |
| 200 | 355 | 40 | 65 | 80 | 110 | 220 |
| 250 | 400 | 50 | 75 | 95 | 130 | 270 |
| 300 | 450 | 55 | 85 | 110 | 150 | 320 |
| 400 | 560 | 65 | 110 | 140 | 195 | 430 |
| 500 | 710 | 75 | 130 | 170 | 240 | - |
| 600 | 800 | 85 | 150 | 200 | 285 | - |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |

[^13]Example: Installation of a bridge pipeline using WKG FL system and push-in joints

If there is a high point, an insulated air-release valve


Annular gap at passage
through wall sealed with gasket.
One sliding hanger per pipe for support distance
from joint approx. 0.5 m
Heat-shrink end cap at the
Sliding hanger, e.g. made by Huckenbeck
(supplied by client).
transition to the non-thermally insulated pipeline

Hangers for above-ground pipelines


Width B of clamp when hangers are spaced 6 mapart

| DN | $80-125$ | $150-200$ | $250-300$ | $400-500$ | $600-700$ | 800 |
| :---: | :---: | :---: | :---: | :---: | :---: | :--- |
| B | 100 | 150 | 200 | 300 | 400 | 450 |

Sliding hangers with anti-lift-off guards. For fastening with anchor bolts or to brackets or bridges. Suitable for WKG pipes in line with structural requirements (e.g. made by Huckenbeck, supplied by the client)

Heat loss times for standing water in fully filled pipes
(initial water temperature $8^{\circ} \mathrm{C}$ )
Buried pipelines (EL) with HDPE
outer sleeves and TYTON ${ }^{\oplus}$ push-in joints

| DN of medium pipe | Thickness of insulation $\mathrm{s}_{\mathrm{D}}$ [mm] | Max. depth of frost penetration 1.4 m |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Height of cover 0.3 m |  | Height of cover 0.5 m |  |
|  |  | Cooling to $0^{\circ} \mathrm{C}$ [h] | Cooling to 25\% ice $[\mathrm{h}]$ | Cooling to $0^{\circ} \mathrm{C}$ [h] | Cooling to 25\% ice $[\mathrm{h}]$ |
| 80 | 41.0 | 24 | 68 | 32 | 102 |
| 100 | 41.0 | 31 | 94 | 41 | 142 |
| 125 | 40.5 | 40 | 130 | 53 | 196 |
| 150 | 40.0 | 49 | 169 | 64 | 254 |
| 200 | 46.5 | 76 | 292 | 100 | 440 |
| 250 | 63.0 | 125 | > 500 | 164 | > 500 |
| 300 | 62.0 | 151 |  | 199 |  |
| 400 | 65.5 | 214 |  | 282 |  |
| 500 | 89.0 | 447 |  | > 500 |  |
| 600 | 82.5 | > 500 |  |  |  |
| 700 | 81.0 |  |  |  |  |
| 800 | 79.0 |  |  |  |  |

For other depths of frost penetration and heights of cover, please consult our Applications Engineering Division.

### 7.3 Installation instructions for ductile iron pipes with WKG thermal insulation

## Applicability

These installation instructions apply to thermally insulated (WKG) ductile iron pipes and fittings. For the assembly of the joints of pipes or fittings, see the particular installation instructions applicable to ductile iron pressure pipes with

- TYTON ${ }^{\star}$ push-injoints,
- restrained VRS®-T push-injoints,
- restrained BRS ${ }^{\oplus}$ push-in joints.

Special notes on transport and storage
When pipes are to be loaded or unloaded or moved about on site, and when they are being installed, slings should be used.
Pipes must only be placed down on at least 10 cm wide lengths of squared timber or other suitable materials spaced about 1.5 m away from the ends of the pipes.

They are not to be:

- put down with ajolt,
- thrown off the vehicle,
- dragged or rolled,
- stacked.


## Laying tools and other accessories

- TYTON ${ }^{\star}$ assembly kit (bent screwdriver and depth gauge),
- V 303 laying tool for DN 80 to DN 400 pipes1),
- chain-hoist or cable-hoist laying tool for all other nominal sizes.

Plus. in the case of pipes with restrained VRS ${ }^{\oplus}-$ T push-injoints

- copper guide for welded bead
- clamping strap (DN 600 and above); see p. 18.

1) For $\mathrm{BRS}{ }^{\oplus}$ push-in joints on pipes of DN 350 size and above, use a chain-hoist laying tool.

FL system for above-ground pipelines (folded spiral-seam outer tubing) First the joint is assembled or assembled and locked, as the case may be, and then, depending on the type of joint (TYTON ${ }^{\oplus}$, BRS ${ }^{\oplus}$ * or VRS ${ }^{\oplus}-\mathrm{T}$ ), one or more rings of soft polyethylene are inserted in the gap that is left between the spigot end and the end-face of the socket.
Finally, the joint is sealed off with a sheet-metal sleeve.


For this purpose, the installer inserts elastic sealing rings (supplied) in the beads formed on the sheet-metal sleeve and fixes the sleeve in position over the joint, in a centralised position, with self-tapping screws.

EL system for buried pipelines (outer sleeve of HDPE)
The gap is first insulated as in the case of the FL system. The joint is then sealed off with heat-shrinkable material (a heat-shrinkable bandage). One-piece sleeves have to be slid onto the barrels of the pipes before the joint is assembled.

Clean the surface area which is going to be covered of any grease. dirt and loose particles. Heat this area to about $60^{\circ} \mathrm{C}$ with a propane gas flame set to a soft setting. Peel the backing film protecting the adhesive away from the bandage for a distance of about 150 mm .

* Our applications Engineering Division must be consulted when BRS® or TYTON ${ }^{\star}$ push-in joints are going to be used in above-ground pipelines.

Fix the free end of the bandage over the joint in a centralised position and at right angles to the plane of the joint and wrap the bandage loosely around the outer sleeve while at the same time peeling off the rest of the protective backing film. Overlap the bandage by at least 80 mm in an easily accessible area at the top of the pipeline.

At low ambient temperatures, it is advisable for the inner side of the overlapping part of the bandage and the inner side of the sealing strip to be heated briefly and pressed firmly against the pipes.


From the outside, heat the sealing strip evenly with a soft. constantly moving flame until the texture of the glass-fibre fabric can be seen. While wearing gloves, press the sealing strip firmly against the pipes by hand.
Shrink on the bandage in the circumferential direction using a soft, evenly moved, flame.

The shrinking-on has been properly carried out if

- the whole of the bandage has been shrunk on,
- it rests down flat, without any cold spots or air bubbles, and the sealing adhesive has been pressed out at both ends,
- the overlap on the outer tube is at least 50 mm .

The transition from a WKG thermally insulated pipe to ductile iron pipes with no thermal insulation is made by means of a heat-shrinkable end cap. With the appropriate changes, this is fitted in the same way as the shrink-on bandages.

## Cutting of pipes

Ensure that the pipes are suitable for cutting (see p. 82). Cuttable pipes are identified by a continuous longitudinal line (adhesive tape) on the outer tubing or outer sleeve and by the white stamped letters "SR" (Schnittrohr = cuttable pipe) on the end-face of the socket. Before the medium pipe is cut to the desired length, the outer tubing or outer sleeve and the polyurethane foam have to be removed in the region of the future spigot end. The length required for the spigot end must be copied from the original pipe or taken from the Tables on p. 55.

When collars (EU and U fittings) having screwed socket joints or bolted gland joints are being used, allowance must be made at the polyurethane foam and the outer tubing or outer sleeve for the larger amount of clear space required. As dictated by the type of joint, the spigot ends should be finished as directed in the corresponding installation instructions.

## Support for the FL system

Ensure that above-ground pipelines have supports, i.e. pipe hangers, of the minimum widths (see p. 55).

Underground installation of EL system
Bedding as per DVGW directive W 400-2 or EN 805 should be provided for the pipes. In the region of surfaces carrying traffic, the filling of pipeline trenches should follow the directive for backfilling pipeline trenches (issued by the Forschungsgesellschaft für das Straßen- und Verkehrswesen of Cologne). When there are small heights of cover (<0.5 m), load distributing slabs should be used above the pipeline zone. Our Applications Engineering Division is at your service to answer any other questions you may have!

## Trace heating

When WKG pipes with trace heating are being used, make sure that the heating cable is situated at the bottom of the pipes.

### 7.4 Coating of fittings (internal and external)

## Structure

In a similar way to what is happening with valves, the powder coating of fittings with epoxy powder is becoming an increasingly important practice. Under EN 545, fittings coated in this way are suitable for use in soils of all classes of corrosiveness. For this purpose, the fittings are first subjected to surface treatment by abrasive blasting (to give a standard of cleanliness of Sa 2.5 ). They are then heated to a temperature of approx. $200^{\circ} \mathrm{C}$ and are dipped into a fluidised bed of epoxy powder or are electrostatically coated by the use of a spray gun. Pore-free layers of a thickness of more than $250 \mu \mathrm{~m}$ are obtained when this is done. If the type of system being used is suitable, the coating process can be automated. When they have cooled, the fittings have their coatings made good at the points of suspension and are tested and packed.
The coating of our fittings meets the requirements of EN 14910 and those of the GSK, the Quality Association for the Heavy Duty Corrosion Protection of Powder Coated Valves and Fittings.


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## Operation

The action of the epoxy coating in protecting against corrosion is based on its absolutely pore-free nature, which keeps all corrosive factors away from the ductile iron. Provided the coating is intact, there is a guarantee of protection. Any injuries to the coating should be avoided or should be repaired as quickly as possible.

## Fields of use

Ductile iron fittings with an epoxy finishing layer to EN 14901 can be used for transporting drinking water, non-drinking water, surface runoff, raw water, sewage and other wastewater.
Under EN 545 they can be used in soils of any desired corrosiveness. The grain size of the bedding material should not exceed 0 to 32 mm (rounded grains) of 0 to 16 mm (fragmented grains).

Installation instructions
It is essential to avoid any damage to the internal and external coatings. Should any damage nevertheless occur, it must be repaired as quickly as possible. For this purpose, any loose parts of the coating must be removed and the damaged point repainted with a suitable epoxy paint. The point which has been repaired must be allowed to cure before the repaired fitting is re-installed.


## 8 - PLANNING, TRANSPORT AND INSTALLATION



### 8.1 Transport and storage

By carrying out comprehensive checks on all pipes and fittings during and after manufacture, including tests of their strength and leak tightness, we ensure that they are all in perfect condition when they leave us.

Provided our products are carefully handled during transport, storage and installation, the drinking water pipelines for which they are used will provide many years of trouble-free service. We therefore recommend that you only allow pipes and fittings to be unloaded and installed under the supervision of properly trained personnel.

Unloading and storage of pipes and pipe bundles
Pipes of up to DN 350 nominal size are supplied bundled. Above this size they are supplied as individual pipes. The exact number of pipes per bundle is shown in the table below. The weights of the pipes can, if required, be found from the pages dealing with the individual pipes.

|  | pipes per bundle |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DN | 80 | 100 | 125 | 150 | 200 | 250 | 300 | 350 |  |  |  |  |  |  |  |  |
| 6 m-pipes | 15 | 15 | 10 | 6 | 6 | 4 | 4 | 4 |  |  |  |  |  |  |  |  |
| 5 m-pipes | 15 | 15 | 12 | 8 | 6 | 4 | 4 |  |  |  |  |  |  |  |  |  |

When pipes or bundles of pipes are to be loaded or unloaded by crane, slings should be used. If individual pipes are unloaded with crane hooks, this must be done with wide, padded hooks fitted at the top of the ends of the pipe as otherwise there is a risk of the pipe and its coating or lining being damaged. Particularly with large pipes, an insert shoe matched to the shape of the pipe must be placed between the hook and the pipe. As an alternative to loading and unloading by crane, suitable fork-lift trucks may also be used. In this case, particular attention must be paid to the following points:

- The pipes must not be able to tilt off the forks sideways (the forks should be at a width of at least 3 m ).
- The pipes must not be able to roll off the forks.
- The forks must be adequately padded to prevent them from damaging the pipe.

During the loading or unloading operation, no-one must stand below the pipe or pipe bundle or on it or in the danger area around the crane.
If pipes are to be moved around by hand, the caps fitted into the ends must first be removed temporarily.


Pipes must only be placed down or stacked on lengths of squared timber or other suitable materials.

They are not to be:

- put down with a jolt,
- thrown off the vehicle,
- dragged, or to be rolled for any great distance.

They are to be:

- secured against rolling and slipping,
- stored on level ground able to take their weight.


If ductile iron drinking water pipes are stored in stacks, they must rest on lengths of squared timber at least 10 cm wide. spaced approx. 1.5 m in from the ends of the pipes.

Maximum allowable heights of stack

| DN | Layers |
| :---: | :---: |
| $80-150$ | 15 |
| $200-300$ | 10 |
| $350-600$ | 4 |
| $700-1,000$ | 2 |

To prevent accidents, you should avoid building any stacks higher than 3 m . Thermally insulated ductile iron pipes (WKG pipes) must not be stacked!


## Unstrapping bundles of pipes

Steel or plastic straps are used to bundle our pipes. The straps should only be cut with suitable tools such as tin snips or side cutters. Using cold chisels, crowbars, pickaxes or the like may cause damage to the external coating of the pipes and also means a greater risk of accidents. Before the straps are cut, make sure that

- the bundle of pipes is standing on non-sloping ground which is as level as possible and which is able to carry the weight of the bundle,
- the pipes are secured against rolling and slipping,
- no-one is standing beside the bundle of pipes or on top of it.

Laying out the pipes on the installation site
If the pipes are laid out beside the pipe trench before they are installed, they should be stored on lengths of squared timber as described above and should be secured against slipping and rolling. The caps fitted to seal off the ends of drinking water pipes should not be removed at this stage. They should only be removed just before the pipes are installed.


## Storage of gaskets

To ensure that the pipeline will operate reliably, it is essential that the gaskets fitted are only ones which comply with the relevant quality specifications and are supplied with the pipes by the manufacturer. If other gaskets are used this may invalidate any claims under guarantee.

Gaskets should be stored in a cool, dry place without being in any way deformed. They should be protected from direct sunlight. Care must be taken to ensure that they are not damaged and do not get dirty.

At temperatures of below $0^{\circ} \mathrm{C}$, the hardness of the gaskets increases to some degree. To make fitting easier, gaskets should therefore be stored at a temperature of more than $10^{\circ} \mathrm{C}$ when the outside temperature is below $0^{\circ} \mathrm{C}$.
Gaskets should not be removed from the store until just before they are going to be fitted and should be checked for any fouling or damage at this time.

### 8.2 Pipeline trenches and bedding

Pipeline trenches should be set out and dug in accordance with current technical codes. Codes to be observed include:

EN 805, EN 1610, DIN 18 300, DIN 4124, DIN 50929 Part 3, ONORM B 2538, DIN 30375 Part 2, DVGW directive W 400-2 or GW 9, ATV DVGW directive A 139 and the directive on the filling of pipeline trenches.

Installation
Pipes and fittings should be installed in accordance with our installation instructions. The external coatings of pipes and the bedding material used for them should be selected in accordance with DIN 30675 Part 2.

| Pipe coating | Coating recommended for joints | Anode backfill | Fields of use in the form of soil classes |
| :---: | :---: | :---: | :---: |
| Zinc coating with finishing layer, to EN 545 | None | No | I, II |
|  |  | Yes | I, II, \|II ${ }^{\text {2 }}$ |
| Zinc-aluminium coating with finishing layer, to EN 545 | None | No | I, II, \|II ${ }^{\text {2 }}$ |
| Cement mortar coating to EN 15542 | Rubber sleeves or heat-shrink material, or B-50M ${ }^{11}$ or $\mathrm{C}-50 \mathrm{M}^{11}$ coating to DIN $30672{ }^{11}$ | No | I, II, III |

AB-50M or C-30M coating to DIN 30672 may be used for joints at sustained operating temperatures of $\mathrm{T} 30^{\circ} \mathrm{C}$. Not suitable when there is constant exposure to eluates of pH < 6 and in peaty, boggy, muddy and marshy soils. The directions given in section 4.1 of DIN 30675 Part 2 must be followed.

| Classification of soils into main groups under DIN 50 929 Part 3 |  |  |
| :---: | :---: | :---: |
| Evaluation number | Soil class | Aggressiveness of soil |
| $>0$ | Ia | Not aggressive |
| -1 bis -4 | Ib | Of low aggressiveness |
| -5 bis -10 | II | Aggressive |
| $<-10$ | III | Highly aggressive |

Not only the aggressiveness of the soil but also its grain size has a part to play in the selection of the external coating for pipes. DVGW directive W 400-2 provides an overview of the allowable grain sizes.

| Pipe material | Coating | Grain size of rounded <br> material | Grain size of fragmented <br> material |
| :--- | :--- | :--- | :--- |
| Ductile iron pipes | Zinc/bitumen <br> Zinc/epoxy <br> Zinc-aluminium/epoxy <br> Zinc/polyurethane | $0-32 \mathrm{~mm}$ <br> Individual grains <br> up to a max. of $63 \mathrm{~mm}^{*}$ | $0-16 \mathrm{~mm}$ <br> Individual grains <br> up to a max. of 32 mm |
| Ductile iron pipes | Cement mortar | $0-63 \mathrm{~mm}$ <br> Individual grains <br> up to a max. of 100 mm | $0-63 \mathrm{~mm}$ <br> Individual grains <br> up to a max. of 100 mm |

*According to ÖNORM B2538 the designer has the possibility to increase the maximum grain size up to 100 mm for ductile iron pipes coated with PUR (polyurethane finishing) or PUR-TOP (polyurethane finishing plus PE-tape). Essential condition therefore is no compression of the backfill area and settlements which maybe occur on top are acceptable (f.e. forest soil, agricultural areas....).


Heights of cover for TYTON pipes

| DN |  | 40-150 | 200-300 | 350-400 | 450-600 | 700-2000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class 40 | Class 40 | Class 30 | Class 30 | Class 25 |
| K (2) |  | 0,110 (20) | 0,110 (20) | 0,105 (45 ${ }^{\circ}$ | 0,105 (45*) | 0,103 (60) |
| $=0,5$ <br> Rural areas | $\mathrm{E}^{\prime}=0$ | 0,3-12,0 | 0,3-7,0 | 0,3-3,8 | 0,3-3,1 | 0,5-1,6 |
|  | $\mathrm{E}^{\prime}=1000$ | 0,3-12,6 | 0,3-7,8 | 0,3-4,8 | 0,3-4,2 | 0,3-3,0 |
|  | $\mathrm{E}^{\prime}=2000$ | 0,3-13,2 | 0,3-8,6 | 0,3-5,7 | 0,3-5,2 | 0,3-4,2 |
|  | $\mathrm{E}^{\prime}=5000$ | 0,3-15,0 | 0,3-11,1 | 0,3-8,5 | 0,3-8,1 | 0,3-7,8 |
| $=0,75$ <br> Access roads | $\mathrm{E}^{\prime}=0$ | 0,3-12,0 | 0,3-6,9 | 0,4-3,7 | 0,5-3,0 | 0,9-1,2 |
|  | $\mathrm{E}^{\prime}=1000$ | 0,3-12,6 | 0,3-7,7 | 0,3-4,7 | 0,4-4,1 | 0,4-2,9 |
|  | $\mathrm{E}^{\prime}=2000$ | 0,3-13,2 | 0,3-8,6 | 0,3-5,6 | 0,3-5,1 | 0,3-4,1 |
|  | $\mathrm{E}^{\prime}=5000$ | 0,3-14,9 | 0,3-11,0 | 0,3-8,5 | 0,3-8,1 | 0,3-7,8 |
| $=1,50$ <br> Main roads | $\mathrm{E}^{\prime}=0$ | 0,3-11,9 | 0,4-6,7 | 0,9-3,2 | 1,2-2,2 | a |
|  | $\mathrm{E}^{\prime}=1000$ | 0,3-12,5 | 0,4-7,6 | 0,7-4,3 | 0,8-3,7 | 1,0-2,3 |
|  | $\mathrm{E}^{\prime}=2000$ | 0,3-13,1 | 0,3-8,4 | 0,6-5,4 | 0,6-4,8 | 0,7-3,9 |
|  | $\mathrm{E}^{\prime}=5000$ | 0,3-14,8 | 0,3-10,9 | 0,4-8,3 | 0,4-7,9 | 0,4-7,7 |

a) Not recommended; a specific calculation for each case provides an adequate answer only

Heights of cover for K9 VRS ${ }^{\oplus}$-T/BLS pipes

| DN |  | 40-200 | 250-300 | 350-450 | 500-2000 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| K (2) |  | 0,110 (20) | 0,110 (20) | 0,105 (45 ${ }^{\circ}$ | 0,103 (60) |
| $=0,5$ <br> Rural areas | $E^{\prime}=0$ | 0,3-15,4 | 0,3-9,9 | 0,3-6,9 | 0,3-2,2 |
|  | $\mathrm{E}^{\prime}=1000$ | 0,3-15,9 | 0,3-10,6 | 0,3-7,8 | 0,3-3,5 |
|  | $\mathrm{E}^{\prime}=2000$ | 0,3-16,4 | 0,3-11,3 | 0,3-8,7 | 0,3-4,7 |
|  | $\mathrm{E}^{\prime}=5000$ | 0,3-17,9 | 0,3-13,4 | 0,3-11,4 | 0,3-8,3 |
| $=0,75$ <br> Access roads | $\mathrm{E}^{\prime}=0$ | 0,3-15,3 | 0,3-9,8 | 0,4-6,8 | 0,5-2,0 |
|  | $\mathrm{E}^{\prime}=1000$ | 0,3-15,8 | 0,3-10,5 | 0,3-7,7 | 0,4-3,4 |
|  | $\mathrm{E}^{\prime}=2000$ | 0,3-16,4 | 0,3-11,2 | 0,3-8,7 | 0,3-4,6 |
|  | $\mathrm{E}^{\prime}=5000$ | 0,3-17,9 | 0,3-13,3 | 0,3-11,3 | 0,3-8,2 |
| $=1,50$ <br> Main roads | $\mathrm{E}^{\prime}=0$ | 0,3-15,2 | 0,3-9,7 | 0,4-6,6 | a |
|  | $\mathrm{E}^{\prime}=1000$ | 0,3-15,8 | 0,3-10,4 | 0,4-7,6 | 0,6-3,0 |
|  | $\mathrm{E}^{\prime}=2000$ | 0,3-16,3 | 0,3-11,1 | 0,3-8,5 | 0,5-4,4 |
|  | $\mathrm{E}^{\prime}=5000$ | 0,3-17,8 | 0,3-13,2 | 0,3-11,2 | 0,3-8,1 |

a) Not recommended; a specific calculation for each case provides an adequate answer only.

## Pressure testing

The execution of pressure tests on pressure pipelines is governed by EN 805 or DVGW directive W 400-2. During pressure testing, all work on the pipelines being tested must be stopped. Particularly in the case of pressure pipelines, all personnel must remain at an adequate safe distance from the pipeline.

### 8.3 Calculating vertical offsets when using flanged fittings

Formulas
$L_{H}=H / \tan$
$L_{s}=H / s i n$
$L_{\text {FF }}=L_{S}-2 \cdot L$
$L_{\text {Ges }}=L_{H}+2 \cdot L$
$H=$ Vertical offset from pipe axis to pipe axis
$L=$ Centre-to-end length of the double flanged bend

$=$ Angle of the double flanged bend

How long does the double flanged pipe have to be when existing double flanged bends are being used and the vertical offset is known?

1. Find the value " $L_{s}$ " from Table 2 for the known vertical offset and the angle of the bend.
2. Find the centre-to-end length "L" of the bend from Table 1 or our Drinking Water Catalogue.
3. To find the length " $L_{\text {FF }}$ " of the double flanged pipe, deduct twice " $L$ " from " $L_{s}$ ".

How large is the vertical offset " H " when an existing double flanged pipe and existing double flanged bends are being used?

1. Measure the length "LFF" of the double flanged pipe.
2. Find the centre-to-end length "L" of the bend from Table 1 or our Drinking Water Catalogue. 3. Calculate "LS": LS = LFF + 2•L.
3. Find the $\sin$ of the bends which are being used from Table 2.
4. Calculate the vertical offset "H" given by the above as follows: $H=L S \cdot \sin$.

How long is the distance "LGES" when the vertical offset " H " and the angle of the double flanged bends are known?

1. From the known vertical offset and the angle of the double flanged bend. find the value " LH " from Table 3.
2. Find the centre-to-end length " L " of the bend from Table 1 or our Drinking Water Catalogue.
3. Calculate "LGES" as follows: $\operatorname{LGES}=\mathrm{LH}+2 \cdot \mathrm{~L}$.

## Worked example:

FFK $30^{\circ}$, DN $200, \mathrm{H}=70 \mathrm{~cm}$

140 cm
18.0 cm
$L_{\text {FF }}=140 \mathrm{~cm}-2 \cdot 18 \mathrm{~cm}=104 \mathrm{~cm}$

## Worked example:

FFK $30^{\circ}$, DN 200, LFF $=104 \mathrm{~cm}$

104 cm
18.0 cm
$L S=104 \mathrm{~cm}+2 \cdot 18 \mathrm{~cm}=140 \mathrm{~cm}$
0.5 cm
$H=140 \mathrm{~cm} \cdot 0.5=70 \mathrm{~cm}$

## Worked example:

FFK $30^{\circ}$. DN 200. $\mathrm{H}=70 \mathrm{~cm}$
121.2 cm
18.0 cm

LGES $=121.2 \mathrm{~cm}+2 \cdot 18 \mathrm{~cm}=$
157.2 cm

Table 1: Centre-to-end lengths " $L$ " of double flanged bends (FFK)
as a function of the angle and diameter DN

| Angle of FFK | Centre-to-end length L[cm] of double flanged bend |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \hline \text { DN } \\ & 80 \end{aligned}$ | $\begin{aligned} & \hline \text { DN } \\ & 100 \end{aligned}$ | $\begin{aligned} & \hline \text { DN } \\ & 125 \end{aligned}$ | $\begin{aligned} & \hline \text { DN } \\ & 150 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline \text { DN } \\ 200 \\ \hline \end{array}$ | $\begin{gathered} \hline \text { DN } \\ 250 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { DN } \\ 300 \\ \hline \end{gathered}$ | $\begin{array}{r} \hline \text { DN } \\ 350 \\ \hline \end{array}$ | $\begin{gathered} \hline \text { DN } \\ 400 \\ \hline \end{gathered}$ |
| $11^{\circ}$ | 13.0 | 14.0 | 15.0 | 16.0 | 18.0 | 21.0 | 25.0 | 10.5 | 11.3 |
| $22^{\circ}$ | 13.0 | 14.0 | 15.0 | 16.0 | 18.0 | 21.0 | 25.0 | 14.0 | 15.3 |
| $30^{\circ}$ | 13.0 | 14.0 | 15.0 | 16.0 | 18.0 | 21.0 | 25.0 | 16.5 | 18.3 |
| $45^{\circ}$ | 13.0 | 14.0 | 15.0 | 16.0 | 18.0 | 35.0 | 40.0 | 29.8 | 32.4 |
| $90^{\circ}$ | 16.5 | 18.0 | 20.0 | 22.0 | 26.0 | 35.0 | 40.0 | 45.0 | 50.0 |


| Angle <br> FFK | Centre-to-end length L[cm] of double flanged bend |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | DN | DN | DN | DN | DN | DN |
|  | 600 | 700 | 800 | 900 | 1000 |  |
| $11^{\circ}$ | 13.5 | 17.4 | 19.4 | 21.3 | - | - |
| $22^{\circ}$ | 18.5 | 25.4 | 28.4 | 31.4 | - | - |
| $30^{\circ}$ | 22.0 | 30.9 | 34.6 | 38.3 | - | - |
| $45^{\circ}$ | 37.5 | 42.6 | 47.8 | 52.9 | 58.1 | 63.2 |
| $90^{\circ}$ | 60.0 | 70.0 | 80.0 | 90.0 | 100.0 | 110.0 |

Dimensions may differ from those shown. The centre-to-end lengths " L " can also be found in Chapter 4.

Table 2 for determining the length "Ls" as a function of the angle and vertical offset "H"

| Length of the slope " $\mathrm{L}_{\text {" }}$ [ $[\mathrm{cm}]$ |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Angle of FFK | sin | Vertical offset H [cm] (pipe axis to pipe axis) |  |  |  |  |  |  |  |  |  |
|  |  | 5 | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 |
| $11^{\circ}$ | 0.19081 | 26.2 | 52.4 | 78.6 | 104.8 | 131.0 | 157.2 | 183.4 | 209.6 | 235.8 | 262.0 |
| $22^{\circ}$ | 0.37461 | 13.3 | 26.7 | 40.0 | 53.4 | 66.7 | 80.1 | 93.4 | 106.8 | 120.1 | 133.5 |
| $30^{\circ}$ | 0.5 | 10.0 | 20.0 | 30.0 | 40.0 | 50.0 | 60.0 | 70.0 | 80.0 | 90.0 | 100.0 |
| $45^{\circ}$ | 0.70711 | 7.1 | 14.1 | 21.2 | 28.3 | 35.4 | 42.4 | 49.5 | 56.6 | 63.6 | 70.7 |
| $90^{\circ}$ | 1 | 5.0 | 10.0 | 15.0 | 20.0 | 25.0 | 30.0 | 35.0 | 40.0 | 45.0 | 50.0 |
| Length of the slope "L. $\mathrm{L}_{\mathrm{s}}$ [ cm$]$ |  |  |  |  |  |  |  |  |  |  |  |
| Angle of FFK | Vertical offset H [cm] (pipe axis to pipe axis) |  |  |  |  |  |  |  |  |  |  |
|  | sin | 55 | 60 | 65 | 70 | 75 | 80 | 85 | 90 | 95 | 100 |
| $11^{\circ}$ | 0.19081 | 288.2 | 314.4 | 340.7 | 366.9 | 393.1 | 419.3 | 445.5 | 471.7 | 497.9 | 524.1 |
| $22^{\circ}$ | 0.37461 | 146.8 | 160.2 | 173.5 | 186.9 | 200.2 | 213.6 | 226.9 | 240.2 | 253.6 | 266.9 |
| $30^{\circ}$ | 0.5 | 110.0 | 120.0 | 130.0 | 140.0 | 150.0 | 160.0 | 170.0 | 180.0 | 190.0 | 200.0 |
| $45^{\circ}$ | 0.70711 | 77.8 | 84.9 | 91.9 | 99.0 | 106.1 | 113.1 | 120.2 | 127.3 | 134.3 | 141.4 |
| $90^{\circ}$ | 1 | 55.0 | 60.0 | 65.0 | 70.0 | 75.0 | 80.0 | 85.0 | 90.0 | 95.0 | 100.0 |

Table 3 for determining the length " LH " as a function of the angle and vertical offset " $H$ "

| Horizontal length " $\mathrm{L}_{H}$ " $[\mathrm{cm}]$ of the offset. from centre to centre of bends |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { Angle } \\ \text { of } \\ \text { FFK } \end{gathered}$ | tan | Vertical offset H [cm] (pipe axis to pipe axis) |  |  |  |  |  |  |  |  |  |
|  |  | 5 | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 |
| $11^{\circ}$ | 0.19438 | 25.7 | 51.4 | 77.2 | 102.9 | 128.6 | 154.3 | 180.1 | 205.8 | 231.5 | 257.2 |
| $22^{\circ}$ | 0.40403 | 12.4 | 24.8 | 37.1 | 49.5 | 61.9 | 74.3 | 86.6 | 99.0 | 111.4 | 123.8 |
| $30^{\circ}$ | 0.57735 | 8.7 | 17.3 | 26.0 | 34.6 | 43.3 | 52.0 | 60.6 | 69.3 | 77.9 | 86.6 |
| $45^{\circ}$ | 1 | 5.0 | 10.0 | 15.0 | 20.0 | 25.0 | 30.0 | 35.0 | 40.0 | 45.0 | 50.0 |
| $90^{\circ}$ | $\infty$ | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |


| Vertical offset H [cm] (pipe axis to pipe axis) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|c\|} \hline \text { Angle } \\ \text { of } \\ \text { FFK } \\ \hline \end{array}$ | tan | Vertical offset H [cm] (pipe axis to pipe axis) |  |  |  |  |  |  |  |  |  |
|  |  | 55 | 60 | 65 | 70 | 75 | 80 | 85 | 90 | 95 | 100 |
| $11^{\circ}$ | 0.19438 | 283.0 | 308.7 | 334.4 | 360.1 | 385.8 | 411.6 | 437.3 | 463.0 | 488.7 | 514.5 |
| $22^{\circ}$ | 0.40403 | 136.1 | 148.5 | 160.9 | 173.3 | 185.6 | 198.0 | 210.4 | 222.8 | 235.1 | 247.5 |
| $30^{\circ}$ | 0.57735 | 95.3 | 103.9 | 112.6 | 121.2 | 129.9 | 138.6 | 147.2 | 155.9 | 164.5 | 173.2 |
| $45^{\circ}$ | 1 | 55.0 | 60.0 | 65.0 | 70.0 | 75.0 | 80.0 | 85.0 | 90.0 | 95.0 | 100.0 |
| $90^{\circ}$ | $\infty$ | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

### 8.4 Dimensioning of concrete thrust blocks

This summary of the on-site procedure applies only to thrust blocks at dead ends, changes of direction and branches lying in a horizontal plane, under the following limiting conditions:

- nominal size $\leq$ DN 300
- concrete of strength class C30/37
- thrust block laid out symmetrically to the line along which the force to be absorbed ( $\mathrm{N}, \mathrm{RN}$ ) acts
- load spread angle in the concrete: $2_{\mathrm{K}}=90^{\circ}$
- outside temperatures of between $+10^{\circ} \mathrm{C}$ and $+30^{\circ} \mathrm{C}$
- horizontal terrain
- concrete placed against undisturbed soil and vertical wall of trench
- depth of foundation $h$ of the thrust block:
$1.0 \mathrm{~m} \leq \mathrm{h} \leq 3.0 \mathrm{~m}$
$\frac{1}{4} h \leq h_{G} \leq \frac{2}{3} h$
- height $h_{G}$ of thrust block against the trench wall:
curing time until the pressure test: at least 3 days
- approximately square bearing area of thrust block against the trench wall: $h_{G} \times b_{G}$
- water table lower than bottom face of thrust block

For practical reasons, no figures are given for the values $\left(h_{R}\right.$ and $\left.b_{R}\right)$ defining the area for transmitting force between the pipeline and the thrust block and it is recommended that the concrete covers the full width, to the sockets, of the pipeline component and that there is adequate concrete cover above the component.

For parameter values which differ from those given above, reference should be made to DVGW directive GW 310, January 2008 version.


Characteristic longitudinal force:
$N_{K}=p \cdot \frac{\pi \cdot d_{a}^{2}}{4} \quad[k N]$

Characteristic resultant force:

$$
R_{N, k}=2 N_{k} \cdot \sin \frac{\alpha_{R}}{2} \quad \rightarrow \quad R_{N, k}=N_{k} \cdot a \quad[k N] \quad \text { where } a=2 \cdot \sin \alpha_{R} / 2
$$

(for a see table below)
$d_{a}=$ outside diameter of pipe [m]
$p=$ internal pressure (test pressure) $\left[\mathrm{kN} / \mathrm{m}^{2}\right] \rightarrow 1 \mathrm{bar}=100 \mathrm{kN} / \mathrm{m}^{2}$

|  | $11^{\circ}$ | $22^{\circ}$ | $30^{\circ}$ | $45^{\circ}$ | Dead ends and <br> branches | $90^{\circ}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a | 0.2 | 0.4 | 0.5 | 0.8 | 1.0 | 1.4 |

The following table shows the values of the resultant force RN,k calculated for the most widely used nominal sizes and bends, for a test pressure of 15 bars. With these figures, it is now possible to calculate the required bearing area of a thrust block against the soil.

| DN | $\mathrm{N}_{\mathrm{k}}[\mathrm{kN}]$ | $\mathrm{R}_{N k}[k N]$ for bends of angles |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (15 bar) | 111/ ${ }^{\circ}$ | 221/2 ${ }^{\circ}$ | $30^{\circ}$ | $45^{\circ}$ | $90^{\circ}$ |
| 65 | 7.9 | 1.5 | 3.1 | 4.1 | 6.1 | 11.2 |
| 80 | 11.3 | 2.2 | 4.4 | 5.9 | 8.7 | 16.0 |
| 100 | 16.4 | 3.2 | 6.4 | 8.5 | 12.6 | 23.2 |
| 125 | 22.4 | 4.8 | 9.5 | 12.6 | 18.7 | 34.5 |
| 150 | 34.0 | 6.7 | 13.3 | 17.6 | 26.1 | 48.1 |
| 200 | 58.1 | 11.4 | 22.7 | 30.1 | 44.4 | 82.1 |
| 250 | 88.4 | 17.3 | 34.5 | 45.8 | 67.7 | 125.1 |
| 300 | 125.2 | 24.5 | 48.9 | 64.8 | 95.8 | 177.1 |
| 350 | 168.3 | 33.0 | 65.7 | 87.1 | 128.8 | 238.1 |
| 400 | 216.8 | 42.5 | 84.6 | 112.2 | 165.9 | 305.6 |
| 500 | 333.4 | 65.4 | 130.1 | 172.6 | 255.2 | 471.5 |
| 600 | 475.0 | 93.1 | 185.4 | 245.9 | 363.6 | 671.8 |
| 700 | 641.6 | 125.8 | 250.4 | 332.1 | 491.1 | 907.4 |
| 800 | 835.2 | 163.7 | 325.9 | 432.3 | 639.3 | 1,181.2 |
| 900 | 1,052.1 | 206.2 | 410.5 | 544.6 | 805.2 | 1,478.9 |
| 1,000 | 1,293.9 | 253.7 | 504.9 | 669.8 | 990.3 | 1,829.9 |

Required bearing area against the soil:

$$
A_{G}=b_{G} \cdot h_{G} \quad\left[m^{2}\right] \quad A_{G}=\frac{R_{N, k}}{\sigma_{h, w}} \quad\left[m^{2}\right]
$$

Allowable $_{\text {h.w }}=$ allowable soil pressure $\left[\mathrm{kN} / \mathrm{m}^{2}\right]$

Allowable soil pressure (allowable ${ }_{\text {h.w }}$ ) as a function of soil group and depth of foundation $h$ for thrust blocks with a square bearing area $\left(h_{G} / b_{G}=1\right)$


NB1: Sand, gravel or sharp-edged, natural broken stone, tightly compacted
NB2: Sand or sandy gravel, compacted to medium tightness
NB3: Sand or sandy gravel, loosely compacted
B1: Till, loam or clay, of at least semi-firm consistency (not kneadable)
B2: Loam, silt or clay, of at least soft consistency (difficult to knead)
B3: Loam, silt or clay, of at least soft consistency (easily kneadable)

For any desired test pressure $p$, the formula which applies to bearing area is:

$$
A_{G}=\frac{R_{N, k}}{\text { Allowable } \sigma_{h, w}} \cdot \frac{p}{15}\left[m^{2}\right]
$$

Example:

| Pipeline | DN 200 |
| :--- | :--- |
| Test pressure | $p=30$ bar |
| Soil pressure | Allowable $\sigma_{\text {h.w }}=50 \mathrm{kN} / \mathrm{m}^{2}$ |
| Angle of bend | $a_{k}=30^{\circ}$ |

Question: How large does the bearing area AG against the soil need to be?
$R_{N}=30.1 \mathrm{kN}$ (see table below)
$A_{G}=\frac{30,1}{50} \cdot \frac{30}{15} \quad\left[m^{2}\right]$

## $A_{\mathrm{G}}=1,204 \mathrm{~m}^{2}$

For calculating concrete thrust blocks under DVGW directive 310, there is also a tool for calculation available at www.eadips.org
Table for the dimensioning of concrete thrust blocks at bends and branches.
Figures were calculated for a test pressure of 15 bars and a soil pressure of
$100 \mathrm{kN} / \mathrm{m}^{2}$. Area $=$ breadth $\mathrm{B} \times$ height H .

| DN | $\begin{gathered} \mathrm{cm}^{2} \\ \mathrm{~cm} \times \mathrm{cm} \end{gathered}$ | $=11{ }^{\circ}$ | $=22^{\circ}$ | $=30^{\circ}$ | $=45^{\circ}$ | = $90^{\circ}$ | Dead ends and branches ${ }^{1}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 80 | $\begin{gathered} F \\ B \times H \end{gathered}$ | $\begin{gathered} 500 \\ 20 \times 25 \end{gathered}$ | $\begin{gathered} 500 \\ 20 \times 25 \end{gathered}$ | $\begin{gathered} 590 \\ 24 \times 25 \end{gathered}$ | $\begin{gathered} 870 \\ 29 \times 30 \end{gathered}$ | $\begin{gathered} 1.600 \\ 38 \times 42 \end{gathered}$ | $\begin{gathered} 1.130 \\ 34 \times 34 \end{gathered}$ |
| 100 | $\begin{gathered} F \\ B \times H \end{gathered}$ | $\begin{gathered} 500 \\ 20 \times 25 \end{gathered}$ | $\begin{gathered} 640 \\ 25 \times 26 \end{gathered}$ | $\begin{gathered} 850 \\ 29 \times 30 \end{gathered}$ | $\begin{gathered} 1.260 \\ 35 \times 36 \end{gathered}$ | $\begin{gathered} 2.320 \\ 48 \times 49 \end{gathered}$ | $\begin{gathered} 1.640 \\ 40 \times 41 \end{gathered}$ |
| 125 | $\begin{gathered} F \\ B \times H \end{gathered}$ | $\begin{gathered} 500 \\ 20 \times 25 \end{gathered}$ | $\begin{gathered} 950 \\ 30 \times 32 \end{gathered}$ | $\begin{gathered} 1.260 \\ 35 \times 36 \end{gathered}$ | $\begin{gathered} 1.870 \\ 43 \times 44 \end{gathered}$ | $\begin{gathered} 3.450 \\ 58 \times 60 \end{gathered}$ | $\begin{gathered} 2.440 \\ 49 \times 50 \\ \hline \end{gathered}$ |
| 150 | $\begin{gathered} F \\ B \times H \end{gathered}$ | $\begin{gathered} 670 \\ 20 \times 25 \end{gathered}$ | $\begin{gathered} 1.330 \\ 36 \times 37 \end{gathered}$ | $\begin{gathered} 1.760 \\ 42 \times 42 \end{gathered}$ | $\begin{gathered} 2.610 \\ 50 \times 52 \end{gathered}$ | $\begin{gathered} 4.810 \\ 69 \times 70 \end{gathered}$ | $\begin{gathered} 3.400 \\ 58 \times 59 \end{gathered}$ |
| 200 | $\begin{gathered} F \\ B \times H \end{gathered}$ | $\begin{gathered} 1.140 \\ 33 \times 35 \end{gathered}$ | $\begin{gathered} 2.270 \\ 48 \times 48 \end{gathered}$ | $\begin{gathered} 3.010 \\ 55 \times 55 \end{gathered}$ | $\begin{gathered} 4.440 \\ 67 \times 67 \end{gathered}$ | $\begin{aligned} & 8.210 \\ & 91 \times 91 \end{aligned}$ | $\begin{aligned} & 5.810 \\ & 76 \times 77 \end{aligned}$ |
| 250 | $\begin{gathered} F \\ B \times H \end{gathered}$ | $\begin{gathered} 1.730 \\ 42 \times 42 \end{gathered}$ | $\begin{gathered} 3.450 \\ 59 \times 59 \end{gathered}$ | $\begin{gathered} 4.580 \\ 68 \times 68 \end{gathered}$ | $\begin{gathered} 6.770 \\ 82 \times 83 \end{gathered}$ | $\begin{gathered} 12.510 \\ 112 \times 112 \end{gathered}$ | $\begin{gathered} 8.840 \\ 94 \times 94 \end{gathered}$ |
| 300 | $\begin{gathered} F \\ B \times H \end{gathered}$ | $\begin{gathered} 2.450 \\ 49 \times 50 \end{gathered}$ | $\begin{aligned} & 4.890 \\ & 70 \times 77 \end{aligned}$ | $\begin{gathered} 6.480 \\ 80 \times 81 \end{gathered}$ | $\begin{gathered} 9.580 \\ 98 \times 98 \end{gathered}$ | $\begin{gathered} 17.710 \\ 133 \times 133 \end{gathered}$ | $\begin{gathered} 12.520 \\ 112 \times 112 \end{gathered}$ |
| 400 | $\begin{gathered} F \\ B \times H \end{gathered}$ | $\begin{gathered} 4.250 \\ 65 \times 66 \end{gathered}$ | $\begin{gathered} 8.460 \\ 92 \times 92 \end{gathered}$ | $\begin{gathered} 11.220 \\ 106 \times 106 \end{gathered}$ | $\begin{gathered} 16.590 \\ 129 \times 129 \end{gathered}$ | $\begin{gathered} 30.560 \\ 175 \times 175 \end{gathered}$ | $\begin{gathered} 21.680 \\ 147 \times 148 \end{gathered}$ |

${ }^{1)}$ These values apply only to dead ends and branches of the nominal sizes specified.

### 8.5 Lengths of pipeline to be restrained

Forces are exerted at bends, branches, dead ends and tapers in pipelines and the size of these forces can be calculated on the basis of, for example,
DVGW directive GW 310.

In pipelines which already have restrained joints, such as welded or flanged joints for example, these forces are transmitted by the pipe joints. In pipelines with nonrestrained joints, e.g. push-in joints (TYTON joints) or screwed socket joints, these forces have to be:

- absorbed by means of concrete thrust blocks (see GW 310), or
- transmitted longitudinally and transferred to the surrounding soil by providing restraint at a number of sockets (socket restraint).

The number of sockets which have to be restrained by the provision of longitudinal restraint depends on the test pressure, the nominal size of the pipes and the standard to which the pipeline trench has been backfilled (type of soil, degree of compaction).

The forces generated by the internal pressure are resisted by the following:

- at bends, branches, dead ends and tapers: the frictional forces between the pipe wall and the surrounding soil,
- at bends: additionally, the bearing resistance of the soil which acts on the adjoining pipes.



## Coefficient of friction

The coefficient of friction $\mu$ for the friction between the soil and the pipe is between
0.1 and 0.6 . Our recommended assumed figures are as follows:
$\mu=0.5 \quad$ for non-cohesive sands, gravels and tills (soil types NB1 to NB3 under GW 310)
$\mu=0.25$ for very loamy sand, sandy loam, marl, loess or loess loam and clay, of at least semi-firm consistency (soil type B1 under GW 310)
$\mu=0.5 \quad$ for pipes with a cement mortar coating
$\mu=0 \quad$ when a pipeline is laid below the water table and/or in cohesive soils of soft and stiff consistency which are difficult to compact (soil types B2 to B4 under GW 310) $\rightarrow$ In such cases we recommend restraining the entire pipeline.

## Soil pressure

The soil pressure which is possible very much depends on the degree of compaction of the trench filling immediately surrounding the pipeline. This should be at least $D_{p r}=95 \%$ In this latter case, it can be expected that the values of allowable horizontal soil pressure (allowable $\sigma_{\text {h.w }}$ ) given in the graph from GW 310 (see page 63) will be reduced by 50\%.

## Notes

At least the following must always be restrained:

- in the case of bends: 2 sockets on each side,
- in the case of branches and dead ends: 2 sockets,
- in the case of tapers: 2 sockets on the side of the larger nominal size.

For a variety of parameters such as coefficient of friction, soil pressure, height of cover of pipes and system test pressure, the tables shown on the following pages give the lengths of pipeline to be restrained for ductile iron pipes. Where a bend at which the resultant force is directed towards the surface is to be restrained, the length of pipeline to be restrained is the same as for a branch or dead end (180 ${ }^{\circ}$ )
There are other calculations which can be carried out by going to www.eadips.org

The tables on the following pages apply provided
the following conditions are met:

- The pipeline trench is completely filled to the height H .
- The material used to fill the pipeline trench is carefully compacted ( $D_{p r}=95 \%$ )
- There is no water in the pipeline trench.
- Ductile iron pipes with a wall thickness of class K 9 are used

Pipeline trench completely filled


Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ when the following parameters apply

| Soil in the pipeline zone: | Sand, gravel or broken stone, <br> tightly compacted (NB1) <br> $\mu=0.50$ |
| :--- | :--- |
| Coefficient of friction: |  |
| Soil pressure: |  |
| Height of cover of pipeline: |  |
| Allowable $\mathrm{h}, \mathrm{w}=40 \mathrm{kN} / \mathrm{m}^{2}$ |  |
| $\mathrm{H}=1.00$ |  |
| (pipeline trench completely filled) |  |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 15 bars

| DN <br> bend | $\mathbf{8 0}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{2 0 0}$ | $\mathbf{2 5 0}$ | $\mathbf{3 0 0}$ | $\mathbf{4 0 0}$ | $\mathbf{5 0 0}$ | $\mathbf{6 0 0}$ | $\mathbf{7 0 0}$ | $\mathbf{8 0 0}$ | $\mathbf{9 0 0}$ | $\mathbf{1 0 0 0}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 12 | 12 | 12 | 13 | 16 | 19 | 24 | 30 | 34 | 39 | 44 | 48 | 52 |
| $90^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 19 | 24 | 29 | 34 | 38 | 43 | 47 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 19 | 24 | 29 | 33 | 38 | 42 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 14 | 19 | 24 | 29 | 33 | 38 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 14 | 19 | 24 | 28 | 33 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 16 |


| Soil in the pipeline zone: | Very loamy sand, sandy loam, loam, clay, <br> marl (B1) |
| :--- | :--- |
| Coefficient of friction: | $\mu=0.25$ |
| Soil pressure: | Allowable $\sigma_{\mathrm{h}, \mathrm{w}}=30 \mathrm{kN} / \mathrm{m}^{2}$ |
| Height of cover of pipeline: | $H=1.00[\mathrm{~m}]$ <br> (pipeline trench completely filled) |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 10 bars

| DN <br> bend | $\mathbf{8 0}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{2 0 0}$ | $\mathbf{2 5 0}$ | $\mathbf{3 0 0}$ | $\mathbf{4 0 0}$ | $\mathbf{5 0 0}$ | $\mathbf{6 0 0}$ | $\mathbf{7 0 0}$ | $\mathbf{8 0 0}$ | $\mathbf{9 0 0}$ | 1000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1 8 0 ^ { \circ }}$ | 12 | 12 | 12 | 13 | 17 | 21 | 24 | 32 | 39 | 45 | 52 | 58 | 63 | 69 |
| $90^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 15 | 18 | 26 | 33 | 40 | 46 | 53 | 58 | 64 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 18 | 25 | 32 | 39 | 45 | 51 | 57 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 17 | 25 | 31 | 38 | 44 | 50 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 15 | 17 | 24 | 30 | 37 | 43 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 16 |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 15 bars

| DN <br> bend | $\mathbf{8 0}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{2 0 0}$ | $\mathbf{2 5 0}$ | $\mathbf{3 0 0}$ | $\mathbf{4 0 0}$ | $\mathbf{5 0 0}$ | $\mathbf{6 0 0}$ | $\mathbf{7 0 0}$ | $\mathbf{8 0 0}$ | $\mathbf{9 0 0}$ | 1000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 15 | 18 | 21 | 27 | 32 | 38 | 49 | 59 | 69 | 78 | 87 | 96 | 104 |
| $90^{\circ}$ | 12 | 12 | 12 | 13 | 19 | 25 | 31 | 42 | 52 | 62 | 71 | 81 | 89 | 97 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 16 | 22 | 32 | 44 | 54 | 64 | 73 | 82 | 90 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 14 | 26 | 37 | 47 | 57 | 66 | 75 | 84 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 17 | 29 | 39 | 49 | 59 | 68 | 77 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 22 | 31 | 41 | 50 |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 21 bars

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 30 bars

| DN <br> bend | $\mathbf{8 0}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{2 0 0}$ | $\mathbf{2 5 0}$ | $\mathbf{3 0 0}$ | $\mathbf{4 0 0}$ | $\mathbf{5 0 0}$ | 600 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 15 | 18 | 21 | 27 | 32 | 38 | 49 | 59 | 69 |
| $90^{\circ}$ | 12 | 12 | 12 | 14 | 20 | 26 | 32 | 43 | 53 | 63 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 15 | 24 | 29 | 38 | 48 | 58 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 15 | 21 | 32 | 43 | 53 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 16 | 27 | 38 | 48 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 18 | 29 |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 45 bars

| DN <br> bend | $\mathbf{8 0}$ | 100 | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | 200 | 250 | 300 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 18 | 22 | 26 | 31 | 40 | 49 | 57 |
| $90^{\circ}$ | 12 | 16 | 20 | 25 | 34 | 43 | 51 |
| $45^{\circ}$ | 12 | 12 | 14 | 19 | 28 | 37 | 45 |
| $30^{\circ}$ | 12 | 12 | 12 | 14 | 23 | 32 | 40 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 17 | 26 | 35 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 14 |

Length of pipeline to be restrained $L[m]$ at test pressure of 21 bars

| DN <br> bend | 80 | 100 | 125 | 150 | 200 | 250 | 300 | 400 | 500 | 600 | 700 | 800 | 900 | 1000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 12 | 12 | 14 | 19 | 23 | 27 | 34 | 41 | 48 | 55 | 61 | 67 | 73 |
| $90^{\circ}$ | 12 | 12 | 12 | 12 | 13 | 17 | 21 | 29 | 36 | 43 | 49 | 56 | 62 | 68 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 15 | 23 | 30 | 37 | 44 | 51 | 57 | 63 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 15 | 25 | 33 | 40 | 46 | 52 | 58 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 20 | 27 | 34 | 41 | 48 | 54 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 16 | 23 | 29 | 36 |


| DN <br> bend | 80 | 100 | 125 | 150 | $\mathbf{2 0 0}$ | $\mathbf{2 5 0}$ | $\mathbf{3 0 0}$ | $\mathbf{4 0 0}$ | $\mathbf{5 0 0}$ | $\mathbf{6 0 0}$ | $\mathbf{7 0 0}$ | $\mathbf{8 0 0}$ | 900 | 1000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 17 | 20 | 25 | 29 | 37 | 45 | 53 | 68 | 83 | 96 | 110 | 122 | 134 | 145 |
| $90^{\circ}$ | 12 | 13 | 17 | 21 | 30 | 38 | 46 | 61 | 76 | 90 | 103 | 115 | 127 | 139 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 21 | 29 | 37 | 53 | 68 | 82 | 95 | 108 | 120 | 132 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 13 | 21 | 29 | 45 | 60 | 74 | 88 | 101 | 113 | 125 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 13 | 21 | 37 | 52 | 67 | 80 | 94 | 106 | 120 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 18 | 22 | 38 | 52 | 66 | 79 | 92 |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 30 bars

| DN <br> bend | 80 | 100 | 125 | 150 | 200 | 250 | 300 | 400 | 500 | 600 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 23 | 28 | 34 | 41 | 53 | 64 | 76 | 98 | 118 | 138 |
| $90^{\circ}$ | 17 | 22 | 28 | 34 | 47 | 58 | 70 | 92 | 113 | 132 |
| $45^{\circ}$ | 12 | 13 | 19 | 25 | 38 | 50 | 61 | 84 | 105 | 125 |
| $30^{\circ}$ | 12 | 12 | 12 | 17 | 30 | 42 | 53 | 76 | 97 | 118 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 21 | 33 | 45 | 68 | 89 | 110 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 14 | 37 | 59 | 81 |


| DN <br> bend | $\mathbf{8 0}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | 200 | 250 | 300 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 35 | 43 | 52 | 61 | 80 | 97 | 114 |
| $90^{\circ}$ | 29 | 36 | 46 | 55 | 73 | 91 | 108 |
| $45^{\circ}$ | 20 | 27 | 37 | 46 | 65 | 82 | 100 |
| $30^{\circ}$ | 12 | 19 | 29 | 38 | 57 | 74 | 92 |
| $22^{\circ}$ | 12 | 12 | 20 | 29 | 48 | 66 | 83 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 16 | 34 | 52 |


| Soil in the pipeline zone: | Very loamy sand, sandy loam, loam, clay, <br> marl $(B 1)$ |
| :--- | :--- |
| Coefficient of friction: | $\mu=0.50$ |
| Soil pressure: | Allowable $\sigma_{\mathrm{hw}}=30 \mathrm{kN} / \mathrm{m}^{2}$ |
| Height of cover of pipeline: | $H=1.00[\mathrm{~m}]$ <br> (pipeline trench completely filled) |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 10 bars

| DN <br> bend | $\mathbf{8 0}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{2 0 0}$ | $\mathbf{2 5 0}$ | $\mathbf{3 0 0}$ | $\mathbf{4 0 0}$ | $\mathbf{5 0 0}$ | $\mathbf{6 0 0}$ | $\mathbf{7 0 0}$ | $\mathbf{8 0 0}$ | $\mathbf{9 0 0}$ | $\mathbf{1 0 0 0}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 15 | 19 | 22 | 25 | 28 | 31 | 34 |
| $90^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 16 | 19 | 23 | 26 | 29 | 32 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 15 | 19 | 22 | 25 | 28 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 15 | 18 | 22 | 25 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 15 | 18 | 21 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 15 bars

| DN <br> bend | $\mathbf{8 0}$ | 100 | 125 | 150 | $\mathbf{2 0 0}$ | $\mathbf{2 5 0}$ | $\mathbf{3 0 0}$ | $\mathbf{4 0 0}$ | $\mathbf{5 0 0}$ | $\mathbf{6 0 0}$ | $\mathbf{7 0 0}$ | $\mathbf{8 0 0}$ | $\mathbf{9 0 0}$ | 1000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 15 | 18 | 24 | 29 | 34 | 39 | 43 | 47 | 52 |
| $90^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 15 | 21 | 26 | 31 | 36 | 40 | 45 | 49 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 16 | 22 | 27 | 32 | 37 | 41 | 45 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 18 | 23 | 28 | 33 | 38 | 42 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 14 | 19 | 25 | 29 | 34 | 39 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 16 | 20 | 25 |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 21 bars

| DN / <br> bend | $\mathbf{8 0}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{2 0 0}$ | $\mathbf{2 5 0}$ | $\mathbf{3 0 0}$ | $\mathbf{4 0 0}$ | $\mathbf{5 0 0}$ | $\mathbf{6 0 0}$ | $\mathbf{7 0 0}$ | $\mathbf{8 0 0}$ | $\mathbf{9 0 0}$ | 1000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 12 | 12 | 13 | 18 | 22 | 26 | 33 | 41 | 48 | 54 | 61 | 67 | 73 |
| $90^{\circ}$ | 12 | 12 | 12 | 12 | 15 | 19 | 23 | 30 | 38 | 45 | 52 | 58 | 64 | 70 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 14 | 19 | 26 | 34 | 41 | 48 | 54 | 60 | 66 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 15 | 23 | 30 | 37 | 44 | 51 | 57 | 63 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 18 | 26 | 33 | 40 | 47 | 53 | 60 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 19 | 26 | 33 | 40 | 46 |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 30 bars

| DN / <br> bend | $\mathbf{8 0}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{2 0 0}$ | $\mathbf{2 5 0}$ | $\mathbf{3 0 0}$ | $\mathbf{4 0 0}$ | 500 | 600 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 13 | 16 | 20 | 26 | 32 | 37 | 48 | 59 | 69 |
| $90^{\circ}$ | 12 | 12 | 13 | 16 | 23 | 28 | 34 | 45 | 56 | 66 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 18 | 24 | 30 | 41 | 52 | 62 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 14 | 20 | 26 | 37 | 48 | 58 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 16 | 22 | 33 | 44 | 54 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 18 | 29 | 40 |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 45 bars

| DN $/ 2$ <br> bend | 80 | 100 | 125 | 150 | 200 | 250 | 300 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 17 | 21 | 25 | 30 | 39 | 48 | 57 |
| $90^{\circ}$ | 14 | 18 | 22 | 27 | 36 | 45 | 54 |
| $45^{\circ}$ | 12 | 13 | 18 | 23 | 32 | 41 | 49 |
| $30^{\circ}$ | 12 | 12 | 14 | 18 | 28 | 37 | 45 |
| $22^{\circ}$ | 12 | 12 | 12 | 14 | 23 | 32 | 41 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 16 | 26 |

Soil in the pipeline zone:

Coefficient of friction:
Soil pressure:
Height of cover of pipeline:

Sand, gravel or broken stone, tightly compacted (NB1)
$\mu=0.50$
Allowable $\sigma_{\text {h.w }}=40 \mathrm{kN} / \mathrm{m}^{2}$
$H=1.50$ [m]
(pipeline trench completely filled)

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 10 bars

| DN / <br> Bend | $\mathbf{8 0}$ | 100 | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{2 0 0}$ | $\mathbf{2 5 0}$ | $\mathbf{3 0 0}$ | $\mathbf{4 0 0}$ | $\mathbf{5 0 0}$ | $\mathbf{6 0 0}$ | $\mathbf{7 0 0}$ | $\mathbf{8 0 0}$ | $\mathbf{9 0 0}$ | 1000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 15 | 18 | 20 | 22 | 25 |
| $90^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 15 | 18 | 20 | 22 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 14 | 16 | 19 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 15 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 15 bars

| DN $/$ <br> bend | $\mathbf{8 0}$ | 100 | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{2 0 0}$ | $\mathbf{2 5 0}$ | $\mathbf{3 0 0}$ | $\mathbf{4 0 0}$ | $\mathbf{5 0 0}$ | $\mathbf{6 0 0}$ | $\mathbf{7 0 0}$ | $\mathbf{8 0 0}$ | $\mathbf{9 0 0}$ | 1000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 16 | 20 | 24 | 27 | 31 | 34 | 37 |
| $90^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 17 | 21 | 25 | 28 | 31 | 35 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 17 | 21 | 24 | 28 | 31 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 14 | 18 | 21 | 25 | 28 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 14 | 18 | 21 | 25 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 21 bars

| DN / <br> bend | 80 | 100 | 125 | 150 | 200 | 250 | 300 | 400 | 500 | 600 | 700 | 800 | 900 | 1000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 15 | 18 | 23 | 28 | 33 | 38 | 43 | 48 | 52 |
| $90^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 15 | 20 | 26 | 31 | 36 | 41 | 45 | 50 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 16 | 22 | 27 | 32 | 37 | 42 | 46 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 18 | 24 | 29 | 34 | 38 | 43 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 15 | 20 | 25 | 30 | 35 | 40 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 17 | 22 | 27 |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 30 bars

| DN / <br> bend | $\mathbf{8 0}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{2 0 0}$ | $\mathbf{2 5 0}$ | $\mathbf{3 0 0}$ | $\mathbf{4 0 0}$ | 500 | 600 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 12 | 12 | 13 | 17 | 21 | 25 | 33 | 41 | 48 |
| $90^{\circ}$ | 12 | 12 | 12 | 12 | 15 | 19 | 23 | 31 | 38 | 45 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 15 | 19 | 27 | 34 | 42 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 15 | 23 | 31 | 38 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 19 | 27 | 35 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 21 |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 45 bars

| DN $/$ <br> bend | $\mathbf{8 0}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{2 0 0}$ | $\mathbf{2 5 0}$ | 300 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 12 | 17 | 20 | 27 | 32 | 39 |
| $90^{\circ}$ | 12 | 12 | 14 | 17 | 24 | 30 | 36 |
| $45^{\circ}$ | 12 | 12 | 12 | 13 | 20 | 26 | 32 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 16 | 22 | 29 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 18 | 25 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 |


| Soil in the pipeline zone: | Very loamy sand, sandy loam, loam, clay, <br> $\operatorname{marl}(B 1)$ |
| :--- | :--- |
| Coefficient of friction: | $\mu=0.25$ |
| Soil pressure: | Allowable $\sigma_{\mathrm{hw}}=30 \mathrm{kN} / \mathrm{m}^{2}$ |
| Height of cover of pipeline: | $H=1.50[\mathrm{~m}]$ <br> (pipeline trench completely filled) |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 10 bars

| DN / <br> bend | $\mathbf{8 0}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{2 0 0}$ | $\mathbf{2 5 0}$ | $\mathbf{3 0 0}$ | $\mathbf{4 0 0}$ | $\mathbf{5 0 0}$ | $\mathbf{6 0 0}$ | $\mathbf{7 0 0}$ | $\mathbf{8 0 0}$ | $\mathbf{9 0 0}$ | $\mathbf{1 0 0 0}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 14 | 17 | 22 | 27 | 32 | 37 | 41 | 46 | 50 |
| $90^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 18 | 23 | 28 | 33 | 38 | 42 | 46 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 18 | 23 | 28 | 32 | 37 | 41 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 17 | 22 | 27 | 32 | 36 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 17 | 22 | 26 | 31 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 15 bars

| DN / <br> bend | $\mathbf{8 0}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{2 0 0}$ | $\mathbf{2 5 0}$ | $\mathbf{3 0 0}$ | $\mathbf{4 0 0}$ | $\mathbf{5 0 0}$ | $\mathbf{6 0 0}$ | $\mathbf{7 0 0}$ | $\mathbf{8 0 0}$ | $\mathbf{9 0 0}$ | $\mathbf{1 0 0 0}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1 8 0 ^ { \circ }}$ | 12 | 12 | 12 | 13 | 18 | 22 | 26 | 34 | 41 | 48 | 56 | 62 | 69 | 75 |
| $90^{\circ}$ | 12 | 12 | 12 | 12 | 13 | 18 | 22 | 30 | 37 | 45 | 52 | 59 | 65 | 72 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 16 | 24 | 32 | 39 | 46 | 53 | 60 | 67 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 18 | 26 | 34 | 41 | 48 | 55 | 62 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 21 | 28 | 36 | 43 | 50 | 57 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 19 | 23 | 30 | 37 |


| DN / <br> bend | 80 | 100 | 125 | 150 | 200 | 250 | 300 | $\mathbf{4 0 0}$ | 500 | 600 | 700 | 800 | 900 | 1000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 13 | 16 | 19 | 25 | 31 | 36 | 47 | 58 | 68 | 78 | 88 | 97 | 106 |
| $90^{\circ}$ | 12 | 12 | 13 | 15 | 21 | 27 | 32 | 43 | 54 | 64 | 74 | 84 | 93 | 102 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 15 | 21 | 26 | 38 | 48 | 59 | 69 | 79 | 88 | 97 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 15 | 21 | 32 | 43 | 54 | 64 | 74 | 83 | 92 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 15 | 27 | 37 | 48 | 58 | 68 | 78 | 87 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 17 | 37 | 38 | 48 | 58 | 68 |

## Soil in the pipeline zone: <br> Coefficient of friction: <br> Soil pressure: <br> Height of cover of pipeline:

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 10 bars

| DN $/$ <br> bend | $\mathbf{8 0}$ | 100 | 125 | 150 | $\mathbf{2 0 0}$ | $\mathbf{2 5 0}$ | $\mathbf{3 0 0}$ | $\mathbf{4 0 0}$ | $\mathbf{5 0 0}$ | $\mathbf{6 0 0}$ | $\mathbf{7 0 0}$ | $\mathbf{8 0 0}$ | $\mathbf{9 0 0}$ | $\mathbf{1 0 0 0}$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 16 | 18 | 20 | 23 | 25 |
| $90^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 14 | 16 | 18 | 21 | 23 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 16 | 18 | 20 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 16 | 18 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 15 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 15 bars

| DN / <br> bend | 80 | 100 | 125 | 150 | 200 | 250 | 300 | 400 | 500 | 600 | 700 | 800 | 900 | 1000 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 16 | 20 | 24 | 28 | 31 | 34 | 38 |
| $90^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 14 | 18 | 22 | 26 | 29 | 32 | 36 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 15 | 19 | 23 | 26 | 30 | 33 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 17 | 20 | 24 | 27 | 31 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 14 | 18 | 21 | 25 | 28 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 15 | 18 |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 21 bars

| DN <br> bend | 80 | 100 | 125 | 150 | 200 | 250 | 300 | 400 | 500 | 600 | 700 | 800 | 900 | 1000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 15 | 18 | 23 | 29 | 35 | 39 | 44 | 48 | 53 |
| $90^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 13 | 16 | 21 | 27 | 32 | 37 | 42 | 46 | 51 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 18 | 24 | 29 | 34 | 39 | 44 | 48 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 16 | 21 | 26 | 32 | 36 | 41 | 46 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 18 | 24 | 29 | 34 | 38 | 43 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 19 | 24 | 29 | 34 |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 30 bars

| DN / <br> bend | $\mathbf{8 0}$ | 100 | 125 | 150 | 200 | 250 | $\mathbf{3 0 0}$ | 400 | 500 | 600 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 12 | 12 | 13 | 18 | 22 | 26 | 34 | 41 | 49 |
| $90^{\circ}$ | 12 | 12 | 12 | 12 | 16 | 20 | 24 | 32 | 39 | 47 |
| $45^{\circ}$ | 12 | 12 | 12 | 12 | 13 | 17 | 21 | 29 | 36 | 44 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 14 | 18 | 26 | 34 | 41 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 15 | 23 | 31 | 38 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 13 | 21 | 28 |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 45 bars

| DN $/$ <br> bend | $\mathbf{8 0}$ | 100 | 125 | 150 | 200 | 250 | 300 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 24 | 29 | 36 | 42 | 54 | 67 | 79 |
| $90^{\circ}$ | 20 | 25 | 31 | 38 | 50 | 63 | 75 |
| $45^{\circ}$ | 14 | 19 | 25 | 32 | 44 | 57 | 69 |
| $30^{\circ}$ | 12 | 13 | 20 | 26 | 39 | 51 | 64 |
| $22^{\circ}$ | 12 | 12 | 14 | 20 | 33 | 45 | 58 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 24 | 36 |

Length of pipeline to be restrained $\mathrm{L}[\mathrm{m}]$ at test pressure of 30 bars

| DN/ <br> bend | $\mathbf{8 0}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{2 0 0}$ | $\mathbf{2 5 0}$ | $\mathbf{3 0 0}$ | $\mathbf{4 0 0}$ | $\mathbf{5 0 0}$ | 600 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 16 | 19 | 23 | 28 | 36 | 44 | 52 | 68 | 83 | 98 |
| $90^{\circ}$ | 12 | 15 | 19 | 23 | 32 | 40 | 48 | 64 | 79 | 94 |
| $45^{\circ}$ | 12 | 12 | 13 | 17 | 26 | 34 | 42 | 58 | 73 | 88 |
| $30^{\circ}$ | 12 | 12 | 12 | 12 | 20 | 29 | 37 | 53 | 68 | 83 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 14 | 23 | 31 | 47 | 63 | 78 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 26 | 42 | 57 |

Length of pipeline to be restrained $L[m]$ at test pressure of 45 bars

| DN $/$ <br> bend | 80 | 100 | 125 | 150 | 200 | 250 | 300 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $180^{\circ}$ | 12 | 14 | 17 | 21 | 27 | 33 | 39 |
| $90^{\circ}$ | 12 | 12 | 15 | 18 | 25 | 31 | 37 |
| $45^{\circ}$ | 12 | 12 | 12 | 15 | 22 | 28 | 34 |
| $30^{\circ}$ | 12 | 12 | 12 | 13 | 19 | 25 | 31 |
| $22^{\circ}$ | 12 | 12 | 12 | 12 | 16 | 22 | 29 |
| $11^{\circ}$ | 12 | 12 | 12 | 12 | 12 | 12 | 18 |

### 8.6 Installation instructions for pipes with a ZMU

## Applicability

These installation instructions apply to ductile iron pipes to EN 545 with a cement mortar coating (ZMU) to EN 15542 . The installation instructions applicable to the given type of joint should be followed when assembling
joints between pipes.

## Recommendations for installation

Installation must be carried out in such a way that the cement mortar coating is not damaged. The following options are available for protecting the socket joints:

- rubber sleeves for protecting cement mortar,
- heat-shrink material or protective tapes (to DIN 30 672),
- mortar bandages (e.g. made by the Ergelit company) for special applications.

Rubber sleeves for protecting cement mortar
Rubber sleeves for protecting cement mortar can be used for TYTON ${ }^{\oplus}$, $\mathrm{BRS}^{\oplus}$ and VRS ${ }^{\oplus}$-T joints in pipes up to DN 800 in size. Before the joint is assembled, turn the sleeve inside out and, with the larger diameter end leading, pull it onto the spigot end sufficiently far for the cement mortar coating to project from the sleeve by about 100 cm . Fitting can be made easier by applying lubricant to the cement mortar coating.


Once the joint has been assembled and the seating of the gasket checked with the depth gauge, turn the sleeve back outside in, pull it along until it is resting against the end-face of the socket and hook it over the socket. It will then rest firmly and tightly against the pipes.

## Shrink-on material and protective tapes

Shrink-on material and protective tapes can be used on all joints. The shrink-on material must be suitable for the dimensions of the particular joint and for the intended use; see Chapter 6. p. 51.

Fitting a shrink-on sleeve
Pull the shrink-on sleeve onto the socket end before the joint is assembled. The surface to be covered should be prepared as detailed in directive GW 15, i.e. the area to which the sleeve is to be fitted should be freed of any rust, grease, dirt and loose particles. Preheat the surface to about $60^{\circ} \mathrm{C}$,
and thus dry it, with a propane gas flame.

After the joint has been assembled, pull the shrink-on sleeve
over the joint, leaving approximately half its length on the socket.


The protective lining present in the sleeve should not be removed until after the sleeve has been positioned on the socket and shortly before it is going to be heated. With a propane gas flame set to a soft setting, heat the shrink-on sleeve evenly all round at the point where the end-face of the socket is situated until the sleeve begins to shrink and the outline of the socket appears within it. Then, while keeping the temperature even by fanning the burner up and down in the circumferential direction, shrink on first the part of the sleeve on the socket and then, starting from the end face of the socket, the part on the barrel of the pipe.


The process has been satisfactorily carried out when:

- the whole of the sleeve has been shrunk onto the joint between the pipes,
- it is resting smoothly against the surface with no cold spots or air bubbles and the sealing adhesive has been forced out at both ends,
- the requisite overlap of 50 cm over the factory-applied coating has been achieved.

Covering a socket joint with a shrink-on sleeve of tape material
The shrink-on tape is available in pre-cut form with a sealing strip already incorporated or in 30 m rolls which include a sealing strip for each socket. When in 30 m rolls, the shrink-on tape has to be cut to the appropriate length on site (see p. 51). The surface to be covered should be prepared as detailed in directive GW 15, i.e. the area to which the tape is to be fitted should be freed of any rust, grease, dirt and loose particles. Preheat the surface to about $60^{\circ} \mathrm{C}$, and thus dry it, with a propane gas flame.

Detach the backing film from the tape for about 150 mm . Position the end of the tape centrally over the joint between the pipes, at right angles to the plane of the joint, and wrap the tape loosely round the joint, removing the rest of the backing film as you do so. The overlap between the ends of the tape should be at least 80 cm and should be situated at an easily accessible point in the top third of the pipes. At low ambient temperatures, it is useful for the adhesive side of the point of overlap and of the sealing strip to be heated for a short period.

Position the sealing strip centrally across the overlap and with a constantly moving soft yellow flame heat the strip evenly from the outside until the lattice pattern of the fabric becomes apparent. Then, wearing gloves, press the sealing strip hard against the tape. Moving the flame evenly in the circumferential direction of the pipes, shrink the tape first onto the socket, beginning on the side away from the sealing strip, and then, in the same way, onto the spigot end.

The process has been satisfactorily carried out when:

- the whole of the tape has been shrunk onto the joint between the pipes
- it is resting smoothly against the surface with no cold spots or air bubbles and the sealing adhesive has been forced out at both ends
- the requisite overlap of 50 cm over the factory-applied coating has been achieved.

With the types of socket protection described, the whole of the angular deflections specified in the installation instructions can still be used even after the protection has been applied.

Rather than the molecularly cross-linked Thermofit heat-shrinkable material, what may also be used are protective tapes of other kinds provided they meet the requirements of DIN 30672 and carry a DIN/DVGW registered number.

Wrapping with protective tapes
Once the joint has been fully assembled, the protective tape is wrapped around the joint in several layers in such a way that it covers the cement mortar coating for $\geq 50 \mathrm{~mm}$.

Wrapping with a mortar bandage (made by the Ergelit company)
Soak the mortar bandage in a bucket filled with water until no more air bubbles are released; maximum soak time should be two minutes.
Take the wet bandage out of the bucket and gently press the water out of it.

Wrap the bandage round the area to be covered (cover the cement mortar coating for $\geq 50 \mathrm{~mm}$ ) and shape it to the contours of the joint.

For a layer 6 mm thick, wrap the bandage round twice or in other words make 50\% of the bandage an overlap. The protective bandage will be able to take mechanical loads after about 1 to 3 hours.

Filling of the pipeline trench
The bedding for the pipeline should be laid in accordance with EN 805 or DVGW directive W 400-2.
Virtually any excavated material can be used as a filling material, even soil containing stones up to a maximum grain size of 100 mm (see DVGW directive W 400-2). Only in special cases does the pipeline need to be surrounded with sand or with some other foreign material.

In the region of surfaces carrying traffic, the filling of pipeline trenches should follow the directive for backfilling pipeline trenches (issued by the Forschungsgesellschaft für das Straßen- und Verkehrswesen of Cologne).

Push-injoints protected by rubber sleeves for protecting cement mortar or by shrink-on material should be surrounded by fine-grained material or should be protected by pipe protection mats.

## Cutting of pipes

Ensure that the pipes are suitable for cutting (see p. 82).
Before pipes are cut, the cement mortar coating must be removed for a length of 2 L or 2LS, as the case may be, as shown in the Table below (for collars, allowance must also be made for the dimension for sliding on the collar).


| DN | TYTON $^{\oplus} /$ | VRS $^{\oplus}-\mathrm{T}$ |
| :---: | :---: | :---: |
|  | $\mathrm{L}(\mathrm{mm})$ | $\mathrm{L}_{\mathrm{s}}(\mathrm{mm})$ |
| 80 | 95 | 165 |
| 100 | 100 | 175 |
| 125 | 100 | 185 |
| 150 | 105 | 190 |
| 200 | 110 | 200 |
| 250 | 115 | 205 |
| 300 | 120 | 210 |
| 350 | 120 | - |
| 400 | 120 | 230 |
| 500 | 130 | 245 |
| 600 | 145 | 300 |
| 700 | 205 | 315 |
| 800 | 220 | 330 |
| 900 | 230 | 345 |
| 1,000 | 245 | 360 |

The lengths of spigot ends free of cement mortar coating appropriate to TYTON ${ }^{\text {® }}$ gaskets apply as follows to sockets to DIN 28603
Form A
up to DN 600

Form B (long socket) DN 700 and above

## Procedure for removing the cement mortar coating

- At the dimensions given in the above table, mark lines indicating the cuts to be made in the cement mortar coating.
- Following the lines, make cuts into the cement mortar coating to about half the depth of the layer (to a depth of 2-3 mm). Important: Do not cut into the ductile iron wall of the pipe! Protective workwear, especially safety goggles, must be used all the time.
- Make two or three longitudinal cuts (as described above) into the cement mortar coating, distributing the cuts around the circumference.
- In the case of pipes which have had a primer applied between the zinc coating and the cement mortar coating, the cement mortar coating should be heated to approx. $160-200^{\circ} \mathrm{C}$ before it is detached. Such pipes are identified by a line below the marking for the coating standard, i.e. "EN 15 542".
- Detach the cement mortar coating by gentle blows with a hammer - starting at the longitudinal cuts.
- Split all the cuts apart with a cold chisel.
- Remove the cement mortar coating and free the spigot end of any residual cement mortar with a scraper and wire brush.
- The pipe can now be cut and the spigot end bevelled as indicated in the section entitled "Cutting of pipes" (see p. 82).

It is essential for the new zinc-coated spigot ends which are produced to be repainted with a suitable finishing coating!

## Fitting pipe saddles

To make house connections to ductile iron pipes with a cement mortar coating, what should preferably be used are saddles with an internal sealing sleeve.

Within the hole in the pipeline, this type of pipe saddle seals directly against the surface of the ductile iron pipe in the drilled hole made in the pipe. Fittings of this kind are available from many manufacturers, e.g. Erhard, EWE and Hawle.

For further information see DVGW-directive W 333.

On-site repairs to the cement mortar coating (ZMU)
All repairs to any detached parts of the ZMU must be carried out using the repair kit supplied by the pipe manufacturer.

Contents of the repair kit
approx. 4 kg of sand/cement mixture
plus approx. 5 m of 200 mm wide gauze
1 litre of diluted additive.

These components are specially adjusted for use with TRM pipes. They must not be replaced by any other material or used to produce classes of cement mortar different from those specified on the repair kit!

## Repair instructions

A proper repair can only be made at temperatures of above $5^{\circ} \mathrm{C}$.
Apart from the repair kit, what you will also need are:

## Rubber gloves

Dust-tight protective goggles
Wire brush
Spatula
Additional mixing vessel
Possibly water for mixing

If there is severe damage:

## Hammer

## Cold chisel

Preparing the damaged area
If there is only slight surface damage, simply remove any loose pieces of cement mortar and any pieces which are not firmly attached with the wire brush. Finally, moisten the damaged area.

If the damage is severe, it is advisable for the cement mortar to be completely removed (down to the bare metal) in the damaged area with a hammer and cold chisel. The protective goggles must be worn when doing the above! Remove the cement mortar in such a way that square edges are obtained:

## Right

## Damaged area



## Wrong

> Damaged area


Do not use excessive force when removing the cement mortar as this may cause the sound cement mortar to become detached in the region next to the damaged area.

Remove any loose material which is still present with the wire brush and moisten the damaged area.

## Mixing

First of all stir the diluted additive well. Then mix the mortar, adding as little additive and water as possible, until a mixture which can be applied easily with the spatula is obtained - the amount of water contained in the additive is normally all that is needed. To begin with, use only the additive solution and meter it in carefully. Then add extra water if necessary (e.g. at high temperatures in summer).

## Application

Once the mortar is easily workable, fill the damaged area with it and level off the surface. Finally, smooth the repaired area, and especially the parts at the edges, with a moistened, wide paintbrush or a moistened dusting brush.

If the damage covers a large area, the gauze is needed to fix the mortar in place in the damaged region. For this purpose the gauze should be positioned about 1 - 2 mm below the surface of the mortar. The gauze must not come into contact with the metal surface of the pipe because, if it does so, it will then act as a wick. Having completed the repair, seal the repair kit again so that it is airtight.

Drying and entry into service
Repairs covering a particularly large area should be covered with plastic film to allow them to dry slowly, thus minimising the risks of cracks forming.

There should be a wait of at least 12 hours before repaired pipes are installed or the damaged area should be provided with adequate protection against mechanical loads.

### 8.7 Installation instructions VRS ${ }^{\circledR}$-T joints DN 80 to DN 500

## Applicability

These installation instructions apply to ductile iron pipes and fittings of DN 80 to DN 500 nominal sizes with restrained VRS ${ }^{\oplus}$-T push-in joints. For recommendations for transport, storage and installation, see p. 60 ff .
For laying tools and other accessories, see Chapter 6.
For very high internal pressures and trenchless installation techniques (e.g. the press-pull, rocket plough or HDD techniques), an additional high pressure lock should be used in pipes of DN 80 to DN 250 nominal sizes (see the section entitled "High pressure lock" on p. 17). The number of joints to be restrained should be decided on in accordance with DVGW directive GW 368 (see p. 65 ff ).

For allowable tractive forces for trenchless installation techniques, see table below or DVGW directives GW 320-1, 321, 322-1, 322-2, 323 and 324.

| DN | $\begin{aligned} & \text { PFA } \\ & {[\text { bar }]^{1]}} \end{aligned}$ | Allowable tractive force $\mathrm{F}_{\text {all }}$ [kN] TRM | Max. angular deflectionat sockets ${ }^{3)}$ [ํ] | Min. radius of curves [m] | Number of fitters | Assembly time without joint protection [min] | Assembly time when using a protective sleeve [min] | Assembly time when using a shrink-on sleeve [min] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 80* | 110 | 115 | 5 | 69 | 1 | 5 | 6 | 15 |
| 100* | 100 | 150 | 5 | 69 | 1 | 5 | 6 | 15 |
| 125* | 100 | 225 | 5 | 69 | 1 | 5 | 6 | 15 |
| 150* | 75 | 240 | 5 | 69 | 1 | 5 | 6 | 15 |
| 200 | 63 | 350 | 4 | 86 | 1 | 6 | 7 | 17 |
| 250 | 44 | 375 | 4 | 86 | 1 | 7 | 8 | 19 |
| 300 | 40 | 380 | 4 | 86 | 2 | 8 | 9 | 21 |
| 400 | 30 | 650 | 3 | 115 | 2 | 10 | 12 | 25 |
| 500 | 30 | 860 | 3 | 115 | 2 | 12 | 14 | 28 |
| 600 | 32 | 1,525 | 2 | 172 | 2 | 15 | 18 | 30 |
| 700 | 25 | 1,650 | 1.5 | 230 | 2 | 16 | - | 31 |
| 800 | 16 | 1,460 | 1.5 | 230 | 2 | 17 | - | 32 |
| 900 | 16 | 1,845 | 1.5 | 230 | 2 | 18 | - | 33 |
| 1,000 | 10 | 1,560 | 1.5 | 230 | 2 | 20 | - | 35 |

${ }^{7}$ Basis for calculation was wall-thickness class K9. Higher pressures and tractive forces are possible in some cases and should be agreed with the pipe manufacturer. ${ }^{2}$ When the route is straight (max. of 0.5 deflection perjoint), the tractive forces can be raised by 50 kN . High-pressure lock is required on DN 80 to DN 250 pipes. ${ }^{3}$ At nominal dimension; * Wall-thickness classes K10

Construction of the joint


| VRS®-T-gasket | VRS®-T-locks |  |
| :---: | :---: | :---: |
|  | DN $80-$ DN 250 | DN 300 - DN 500 |
| EPDM to EN 681-1 | 1 Right lock (black) <br> 1 Left lock (red) <br> 1Catch | 2 Right locks (black) <br> 2 Left locks (red) <br> 2 Catchs |

(2) Cotich

Cleaning


Clean the surfaces of the seating for the gasket, the retaining groove and the retaining chamber which are indicated by the arrows and remove any excess paint (paint humps, bubbles or pimples) from them. Use a scraper (e.g. a bent screwdriver) to clean the retaining groove.


Clean the spigot end. Remove any fouling and any excess paint (paint humps, bubbles or pimples).

Positions of the openings in the socket end-face when the pipe is in the pipeline trench


DN 80 to DN 250


DN 300 to DN 500

For inserting the locks or bolting on the clamping ring, it is advisable for the openings in the end-face of the socket to be positioned as shown. For fittings, the position of the openings will depend on the particular installation situation. For WKG pipes with trace heating, care must be taken to see that the heating cable is positioned at the bottom of the pipe.

## Inserting the gasket

Lubricant should be used below TYTON ${ }^{\text {® }}$ gaskets. For this purpose. carefully wipe a thin film of the lubricant supplied with the pipes by the manufacturer over the sealing surface identified by the oblique lines. Note: Do not put any lubricant in the retaining groove (the narrow groove)! No lubricant is used with VRS ${ }^{\oplus}-T$ gaskets.


Clean the gasket and make a loop in it so that it is heart-shaped.

Fit the gasket into the socket so that the hard-rubber claw on the outside engages in the retaining groove in the socket. Then press the loop flat.

If you have any difficulty in pressing the loop flat, pull out a second loop on the opposite side.
These two small loops can then be pressed flat without any difficulty.


The inner edge of the hard-rubber claw of the gasket must not project below the locating collar.
Right


## Cross section of VRS ${ }^{\oplus}$-T gasket



## Wrong



## Cross section of TYTON ${ }^{\circledR}$ gasket



Apply a thin layer of lubricant to the gasket.


Spigot end with welded bead
Apply a thin layer of lubricant to the cleaned spigot end - and particularly to the bevel - and then pull or push the spigot end into the socket until it is in abutment with the end-wall of the socket. Pipes must not be in a deflected angular position when they are being pushed in or the locks are being inserted.


1) Insert the "right" lock in the opening in the socket and slide it to the right as far as possible.
2) Insert the "left" lock in the opening in the socket and slide it to the left as far as possible.
3) Press the catch into the opening in the socket.

On pipes of DN 300 size and above, steps 1 to 3 have to be carried out twice because $2 \times 2$ locks and 2 catches are used in this case.

Spigot end without a welded bead
First insert the two halves of the clamping ring into the retaining chamber separately and then connect them together loosely with the two bolts. Mark the depth of insertion (the depth of the socket) on the spigot end.

Apply lubricant to the cleaned spigot end - and particularly to the bevel - and then pull or push it in until it is fully home in the socket. Pipes must not be at an angular deflection when they are being pulled in. After the pulling-in, the mark previously made on the spigot end should be almost in line with the end-face of the socket.

Pull the clamping ring towards the end-face of the socket as far as possible and then tighten the bolts $\geq 60 \mathrm{Nm}$.

Tightening torque $\geq 60 \mathrm{Nm}$


Notes on clamping ring joints
Care should be taken to see that clamping ring joints are not used in above-ground pipelines or pipelines subject to pulsations or for trenchless installation techniques. For single socket bends, double socket bends, $90^{\circ}$ flange socket duckfoot bends and $90^{\circ}$ duckfoot bends with side outlets, the PFA is a maximum of 16 bars.
Please enquire for PFA's of more than 16 bars. For connections at bends where the operating pressure is $>16$ bars, an adaptor, a piece of cut pipe with two spigot ends, is turned through $180^{\circ}$ so that the end carrying the welded bead mates with the socket of the bend.

Before the remaining, socketed, piece of the cut pipe is installed, an uncut pipe is laid. The spigot end of the piece of cut pipe, which does not carry a welded bend, is then inserted in the socket of the uncut pipe. Our Applications Engineering Division should be consulted before clamping rings are used in culvert or bridge pipelines and before joints using them are laid on steep slopes, in casing tubes or pipes, in utility tunnels or in above-ground pipelines or pipelines subject to pulsations. Clamping rings should not be used in these cases or in trenchless installation techniques. The pieces of adapter pipe required should be provided with welded beads.


## Locking

Pull or push the pipe out of the socket, e.g. with a laying tool, until the locks or the clamping ring are firmly in abutment in the retaining chamber. The joint is now restrained.


Angular deflection
Once the joint has been fully assembled，pipes and fittings can be deflected angularly as follows：

DN 80 to DN150－max．of $5^{\circ}$
DN 200 to DN 300 －max．of $4^{\circ}$
DN 400 and DN 500 －max．of $3^{\circ}$

For a pipe length of $6 \mathrm{~m}, 1^{\circ}$ of angular deflection causes the axis of the pipe to lie approx． 10 cm off the axis of the pipe or fitting installed previously，i．e． $3^{\circ}=30 \mathrm{~cm}$ ． With 5 m long pipes， $1^{\circ}$ corresponds to approx． 9 cm ．


Note on installation
Make sure that，as a function of the internal pressure and the tolerances on joints，it is possible for extensions of up to about 8 mm to occur．To allow for the travel of the pipeline when it extends when pressure is applied，joints at bends should be set to the maximum allowable angular deflection in the negative direction．


## Cutting of pipes

Ensure that the pipes are suitable for cutting（see p．82）．If pipes have to be cut on site，the welded bead required for the $\mathrm{VRS}{ }^{\oplus}-\mathrm{T}$ push－in joint has to be applied using an electrode as specified by the pipe manufacturer．The welding work should be done in accordance with directive DVS 1502 or the technical recommendations for welding given from $p$ ． 83 ff on．

The distance between the end of the spigot end and the welded bead and the size of the welded bead must be as shown in the table below．
Electrode type，e．g．Castolin 7330－EC，UTP FN 86，ESAB OK 92．58，
Gricast 31 or 32
The electrode diameter should be 3.2 mm below DN 400 and
4.0 mm at DN 400 and above．

For electrode consumption see p． 76

| DN | 80 | 100 | 125 | 150 | 200 | 250 | 300 | 400 | 500 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L | $86 \pm 4$ | 91 $\pm 4$ | $96 \pm 4$ | 101 $\pm 4$ | 106さ4 | 106さ4 | $106 \pm 4$ | 115 $\pm 5$ | 120 5 |
| a | $8 \pm 2$ | $8 \pm 2$ | $8 \pm 2$ | $8 \pm 2$ | $9 \pm 2$ | $9 \pm 2$ | $9 \pm 2$ | $10 \pm 2$ | 10さ2 |
| b | $5^{00.5}$ | $5^{0.5}$ | $5^{\text {º．}}$ | $5^{+0.5}$ | $5.5^{10.5}$ | $5.5{ }^{+0.5}$ | $5.5{ }^{\circ 0 .}$－ | $6^{+0.5}$ | $6^{+0.1}$ |

To ensure that there is a good welded bead at a uniform distance from the end，a copper welding guide must be fastened to the spigot end at the specified distance from the end（see table）as a guide for application．The area to be welded must be bright metal．Any fouling or zinc coating must be removed by filing or grinding． When the welding guide is removed，the cut edge of the spigot end should be matched to the form of an original spigot end and the area of the welded bead should be cleaned．Finally，the appropriate protective coating should be applied to both these areas．

## Disassembly

Push the pipe as far as possible into the socket along its axis．Remove the catch through the opening in the socket end－face．Slide the locks round and remove them through the opening．If a high－pressure lock is fitted，slide it round from the bottom of the pipe to the opening with a flat object（e．g．a screwdriver）and remove it．

## Disassembly of clamping ring joints

Push the pipe into the socket along its axis until it is in abutment．
Remove the clamping bolts and then loosen the halves of the clamping ring by hitting them with a hammer．Ensure that the halves of the clamping ring remain loose during disassembly（if necessary by again hitting them with a hammer as the spigot end is pulled out）．They can also be stopped from jamming on the spigot end during disassembly by inserting a square steel bar between the lugs at the ends of the halves．Do not under any circumstances hit the socket or the barrel of the pipe with the hammer！

## High－pressure lock

An additional high－pressure lock should be used whenever very high internal pressures are expected（e．g．in the case of turbine pipelines）and whenever trenchless installation techniques are used（e．g．the press－pull，rocket plough or horizontal directional drilling techniques）．Before the left and right locks are inserted，the high－pressure lock is inserted in the retaining chamber through the opening in the end－face of the socket and is positioned at the bottom of the pipe． The locks can then be inserted and the high－pressure lock is thus situated between their flat ends．The locks are then fixed in place in the usual way with the catch．

The illustration below shows a fully assembled VRS ${ }^{\oplus}-T$ socket with a high－pressure lock．The high－pressure lock can be used for pipes of nominal sizes from DN 80 to DN 250.


High－pressure lock


### 8.8 Installation instructions <br> BLS ${ }^{\circledR}$ joints DN 600 - DN 1000

## Applicability

These installation instructions apply to DN 600 - DN 1,000 ductile iron pipes and fittings with restrained BLS ${ }^{\oplus}$ push-in joints.
For recommendations for transport, storage and installation,
see p. 60 ff. For laying tools and other accessories, see Chapter 6.
Construction of the joi


Number n of locking segments per joint

| DN | 600 | 700 | 800 | 900 | 1,000 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $n$ | 9 | 10 | 10 | 13 | 14 |

## Cleaning

Clean the surfaces of the seating for the gasket, the retaining groove and the retaining chamber which are indicated by the arrows and remove any excess paint (paint humps, bubbles or pimples).


Use a scraper (e.g. a bent screwdriver) to clean the retaining groove.

Clean the spigot end. Remove any fouling and any excess paint (paint humps, bubbles or pimples)


Positions of the openings in the socket end-face
The opening in the end-face of the socket should always be situated at the top of the pipe.


Inserting the gasket

Lubricant should be used below TYTON® gaskets.
For this purpose, carefully wipe a thin film of the lubricant supplied with the pipes by the manufacturer over the sealing surface identified by the oblique lines.


Note: Do not put any lubricant in the retaining groove
(the narrow groove)!

Clean the TYTON ${ }^{\oplus}$ gasket and make a loop in it so that it is heart-shaped


Fit the TYTON ${ }^{\oplus}$ gasket into the socket so that the hard-rubber claw on the outside engages in the retaining groove in the socket. Then press the loop flat.

If you have any difficulty in pressing the loop flat, pull out a second loop on the opposite side.
These two small loops can then be pressed flat without any difficulty. The inner edge of the hard-rubber claw
of the TYTON ${ }^{\circledR}$ gasket must not project below the locating collar.

Right


## Wrong



Apply a thin layer of lubricant to the TYTON ${ }^{\circledR}$ gasket.


Assembling the joint
Apply a thin film of lubricant to the cleaned spigot end - and particularly to the bevel - and then pull or push it in until it is fully home in the socket. The pipes must not be at an angular deflection when being pulled in or when the lock segments are being fitted.


First insert the locking segments through the opening in the end-face of the socket and distribute them around the circumference of the pipe, working alternately left and right. Then move all the segments round in one direction until the last segment can be inserted through the openings in the end-face of the socket and can be moved to a position where it provides secure locking.

Only a small part of the humps on the last locking segment should be visible through the opening in the end-face of the socket. Should segments jam, they should be moved to their intended position by gentle taps with a hammer by moving the pipe as it hangs from the sling.


Do not under any circumstances hit the socket or the barrel of the pipe with the hammer!

## Locking

Pull back all the locking segments in the outward direction until they are in abutment against the slope of the retaining chamber. Then fit the clamping strap around the outside of the segments as shown in the illustration. Tighten the clamping strap only sufficiently far enough to still allow the locking segments to be moved. Now line up the locking segments. They should be resting against the barrel of the pipe over their full area and should not be overlapping. Then tighten the clamping strap until the locking segments are bearing firmly against the pipe around the whole of its circumference.

It should now no longer be possible to move the locking segments. By pulling on it axially (e.g. by means of a locking clamp), pull the pipe out of the joint until the welded bead comes to rest against the segments. When the pipe is in an undeflected state, the locking segments should all be approximately the same longitudinal distance away from the end-face of the socket.

Note: A metal clip rather than the clamping strap should be used in all trenchless techniques.

## Retaining chamber



Angular deflection
Once the joint has been fully assembled, pipes and fittings can be deflected angularly as follows:

DN 600 - max. of $2.0^{\circ}$
DN 700 - max. of $1.5^{\circ}$
DN 800 - max. of $1.5^{\circ}$
DN 900 - max. of $1.5^{\circ}$
DN 1000 - max. of $1.5^{\circ}$

For a pipe length of $6 \mathrm{~m}, 1^{\circ}$ of angular deflection causes the axis of the pipe to lie approx. 10 cm off the axis of the pipe installed previously, i.e. $3^{\circ}=30 \mathrm{~cm}$.


Note on installation
Please remember that, as a function of the internal pressure, it is possible for extensions of up to about 8 mm per joint to occur as a result of the locking segments adjusting.

To allow for the travel of the pipeline when it extends when pressure is applied, joints at bends should be set to the maximum allowable angular deflection in the negative direction.


## Cutting of pipes

Ensure that the pipes are suitable for cutting (see p. 82). If pipes have to be cut on site, the welded bead required for the BLS ${ }^{\oplus}$ push-in joint has to be applied using an electrode as specified by the pipe manufacturer. The welding work should be done in accordance with directive DVS 1502 or the technical recommendations for welding given from $p$. 83 ff on.

The distance between the end of the spigot end and the welded bead and the size of the welded bead must be as shown in the table below. Electrode type, e.g. Castolin 7330-EC, UTP FN 86, ESAB OK 92.58, Gricast 31 or 32.

| DN | 600 | 700 | 800 | 900 | 1,000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L | 116 | 134 | 143 | 149 | 159 |
| a | $9 \pm 1$ | $9 \pm 1$ | $9 \pm 1$ | $9 \pm 1$ | $9 \pm 1$ |
| $b$ | 6 | 6 | 6 | 6 | 6 |

To ensure that there is a good welded bead at a uniform distance from the end, a copper welding guide must be fastened to the spigot end at the specified distance from the end (see table) as a guide for application.

The area to be welded must be bright metal. Any fouling or zinc coating must be removed by filing or grinding.


When the welding guide is removed, the cut edge of the spigot end should be matched to the form of an original spigot end and it and the area of the welded bead should be cleaned. Finally, the appropriate protective coating should be applied to both these areas.

## Disassembly

Push the pipe into the socket along its axis until it is in abutment and remove the locking segments through the opening in the socket end-face.

## Special pipelines

Our Applications Engineering Division should be consulted if for example joints of this kind are to be used in casing tubes or pipes, on bridges, for the horizontal direction drilling technique or in culvert pipelines.

Pipelines on steep slopes should be installed from the top down, meaning that after each individual pipe has been extended the locking will be maintained by gravity. If this procedure cannot be followed, suitable steps must be taken to prevent the locking from being cancelled out by gravity.

Combining fittings belonging to other systems with BLS ${ }^{\circledast}$ joints Our Applications Engineering Division should be consulted if pipe ends of the present type are to be combined with fitting sockets belonging to other systems.

Electrode consumption

| DN nominal size | Electrode consumption per bead Ø 3.2 mm [unit] | Electrode consumption per bead $\emptyset 4.0$ mm [unit] | Time required per welded bead [min] |
| :---: | :---: | :---: | :---: |
| 80 | 5 |  | 15 |
| 100 | 6 |  | 18 |
| 125 | 8 |  | 24 |
| 150 | 9 | - | 27 |
| 200 | 12 |  | 36 |
| 250 | 15 |  | 43 |
| 300 | 17 |  | 50 |
| 400 | 8 + | 11 | 57 |
| 500 | $11+$ | 14 | 75 |
| 600 | 13 + | 16 | 87 |
| 700 | 16 + | 19 | 105 |
| 800 | 18 + | 22 | 120 |
| 900 | $21+$ | 25 | 138 |
| 1,000 | 23 + | 27 | 150 |

The welded bead should normally be applied in two passes, the root pass normally being welded with a $\emptyset 4.0$ mm electrode on pipes of DN 400 size and above.

The electrode consumptions and times required given in the table are only a guide.

### 8.9 Installation instructions TYTON ${ }^{\circledR}$ push-injoints

## Applicability

These installation instructions apply to ductile iron pipes and fittings to EN 545 and DIN 28650 with TYTON ${ }^{\text {® }}$ push-in joints to DIN 28 603. There are separate installation instructions for installation and assembly when using restrained joints (VRS ${ }^{\oplus}$-T and BRS ${ }^{\oplus}$ joints) and/or for pipes with a cement mortar coating (ZMU). For recommendations for transport, storage and installation, see p. 60 ff . For laying tools and other accessories, see Chapter 6.

Construction of the joint


Cleaning


Clean the surfaces of the seating for the gasket and the retaining groove which are indicated by the arrows and remove any excess paint (paint humps, bubbles or pimples) from them. Use a scraper (e.g. a bent screwdriver) to clean the retaining groove.


Clean the spigot end back to the line marking. Remove any fouling and any excess paint (paint humps, bubbles or pimples)


Carefully apply a thin coat of the lubricant supplied by the pipe manufacturer only to the sealing surface identified by the oblique lines.
Note: Do not apply any lubricant to the retaining groove (the narrow groove).


Assembling the joint
Inserting the TYTON ${ }^{\circledR}$ gasket.

Clean the TYTON ${ }^{\circledR}$ gasket and make a loop in it so that it is heart-shaped.

Fit the TYTON ${ }^{\oplus}$ gasket into the socket so that the hard-rubber claw on the outside engages in the retaining groove in the socket.

Then press the loop flat.

If you have any difficulty in pressing the loop flat, pull out a second loop on the opposite side. These two small loops can then be pressed flat without any difficulty. The inner edge of the hard-rubber claw of the gasket must not project below the locating collar.

## Right



Once the joint has been assembled, check the seating of the gasket with the depth gauge around the entire circumference.

The gauge should penetrate into the gap between the spigot end and the socket to a uniform depth all round the circumference. If it is able to penetrate deeper at one or more points, it is possible that the gasket has been pushed out of the retaining groove at these points and hence that there will be leaks there. If this is the case, the joint must be disassembled and the seating of the gasket checked.

Angular deflection
Once the joint has been fully assembled, pipes and fittings can be deflected angularly as follows:

Upto DN 300 - max. of $5^{\circ}$
DN 400 - max. of $4^{\circ}$
DN 1000 - max. of $3^{\circ}$

For a pipe length of $6 \mathrm{~m}, 1^{\circ}$ of angular deflection causes the axis of the pipe to lie 10 cm off the axis of the pipe or fitting installed previously, i.e. $3^{\circ}=30 \mathrm{~cm}$. With 5 m long pipes, $1^{\circ}$ corresponds to approx. 9 cm .


## Cutting of pipes

Ensure that the pipes are suitable for cutting (see p. 82). Cut pipes must be bevelled at the cut end to match the original spigot end.

The bevel must be made as shown in the diagram.


The cut surface must be re-painted (see p. 82)
Copy the line markings from the original spigot end to the new spigot end which has been cut.

Disassembly
If newly installed pipes or fittings have to be disassembled, this can be done without any special tools. Either use the laying tool to do this or move the pipe or fitting gently to and fro while pulling on it.

Pipelines fitted with TYTON ${ }^{\circledR}$ push-in joints which have already been in place for quite some time can be disassembled as follows.

With a laying tool


With a clamp and a jack


### 8.10 Installation instructions for flanged joints

## Applicability

These installation instructions apply to ductile iron pipes and fittings to EN 545 with flanges to EN 1092-2.

Construction of the joint


## $\square=$

Washers to EN ISO 7091


Clean the bolt holes and the surfaces of the sealing ridge and the gasket which are indicated by the arrows and remove any excess paint (paint humps, bubbles or pimples) from them.

Assembling the joint
For recommendations for transport, storage and installation, see p. 60.
For better assembly and greater reliability in operation, only gaskets with a steel inlay should be fitted.

Flanged pipes and fittings must be carefully supported.
Rigid joints in pipes are unable to withstand differing loads and differing amounts of settlement. Under no circumstances must the pipes or fittings be supported on stones or other similar material.

## Positioning the bolt holes

The rule for the positioning of bolt holes which applies to flanged pipes and flanged fittings is that no bolt holes must be situated on the vertical or horizontal centrelines of the flanges.

Note in the installation of flanged fittings
To make it easier for flanged fittings to be installed properly, their flanges have two oppositely situated notches made in them. These notches must be in line with one another horizontally or vertically at the time of installation.


Right


Wrong

Installing double flanged tapers


The example shown is an FFR 300/200 PN 10 taper
Because of the differing numbers of bolt holes in the two flanges of double flanged tapers, the next valve or fitting will be skewed around its axis if the taper is not correctly installed. The amounts of skew may, depending on the nominal size, be up to $22.5^{\circ}$.

Important!
With large nominal sizes such skews are almost imperceptible.

Tightening torques
The tightening torque $M_{D}$ depends on the gasket material, the nominal size DN and the pressure rating PN .

It can be calculated as follows:
$\mathrm{M}_{\mathrm{D}} \mathrm{PN} 10=\mathrm{DN} / 3[\mathrm{Nm}] \quad \mathrm{M}_{\mathrm{D}} \mathrm{PN} 16=\mathrm{DN} / 1.5[\mathrm{Nm}]$
$M_{D} P N 25=D N / 1[\mathrm{Nm}] \quad M_{D} P N 40=D N / 0.5[\mathrm{Nm}]$

### 8.10 Installation instructions <br> BRS ${ }^{\oplus}$ push-injoints

## Applicability

These installation instructions apply to ductile iron pipes and fittings to EN 545 and DIN 28650 with restrained BRS ${ }^{\oplus}$ push-in joints to DIN 28 603. There are separate installation instructions for the installation and assembly of other restrained joints and/or of pipes with a cement mortar coating (ZMU).

For recommendations for transport, storage and installation, see p. 60 ff. For laying tools and other accessories, see Chapter 6.
The number of joints which have to be restrained should be decided on in accordance with DVGW directive GW 368 (see p. 65).

Our Applications Engineering Division should always be consulted before joints of the present type are used in culvert or bridge pipelines and before they are laid on steep slopes or in casing tubes or pipes or in utility tunnels or in unstable soil.

Construction of the joint


Important! There are three notable features by which the TYTON ${ }^{\star}$-SIT-PLUS ${ }^{\oplus}$ gasket can be recognised:

The marking "TYTON®-SIT-PLUS"


## Cleaning

Clean the surfaces of the seating for the gasket and the retaining groove which are indicated by the arrows and remove any excess paint (paint humps, bubbles or pimples) from them.


Use a scraper (e.g. a bent screwdriver) to clean the retaining groove.


Clean the spigot end back to the line marking. Remove any fouling and any excess paint (paint humps, bubbles or pimples).

Assembling the joint
Insert the TYTON ${ }^{\circledR}$-SIT-PLUS ${ }^{\oplus}$ gasket as specified in the installation instructions for the TYTON ${ }^{\oplus}$ push-in joint (see p. 77).


Stainless steel segment

Clean the TYTON ${ }^{\oplus}$-SIT-PLUS ${ }^{\oplus}$ gasket, make a loop in it so that it is heart-shaped, and fit it into the seating for the gasket.

Important! The point of the loop must always be between two segments.

Apply a thin layer of lubricant to the TYTON ${ }^{\star}$-SIT-PLUS ${ }^{\text {® }}$ gasket once it has been fitted into the seating. Take the profiled identifying ring marked with a stripe of white paint and slide it onto the spigot end.

Apply a thin layer of lubricant to the spigot end - and particularly to the bevel and then insert the spigot end into the socket until it is resting against the TYTON ${ }^{\star}$-SIT-PLUS ${ }^{\circledR}$ gasket and is centralised.

Fit the laying tool to the socket and the spigot end and use it to pull the spigot end of the pipe or fitting being inserted into the socket of the pipe already laid. Avoid any angular deflection when doing so.


Push the spigot end into the socket until the first marking line can no longer be seen. It is now no longer permissible for either part of the joint to be turned.

Locking
Pull or press the pipe out of the socket, e.g. with a laying tool, until the stainless steel segments engage.

Do not remove whatever is being used to lift the pipe until the joint has been fully assembled.


The joint is now restrained.


Once the joint has been assembled, check that the TYTON ${ }^{\bullet}$-SIT-PLUS ${ }^{\oplus}$ gasket is correctly seated around the entire circumference with the depth gauge supplied.
The gauge should penetrate into the gap between the spigot end and the socket to a uniform depth all round the circumference.
The depth of penetration is usually greater in the region of the segments than in the rest of the gasket. If the depth of penetration is unduly large at one or more points, there may be a hump in the gasket and hence a possible leak at these points. If this is the case, the joint must be disassembled and the seating of the gasket checked.

## Important:

Do not re-use TYTON ${ }^{\star}$-SIT-PLUS ${ }^{\circledR}$ gaskets from joints which
have been disassembled!

Identification of the joint
As a durable means of identifying the restrained push-injoint, we supply a profiled rubber ring carrying a stripe of white paint on its circumferential surface. The ring should be positioned as shown in the illustration before the joint is assembled.


## Angular deflection

Once the joint has been fully assembled, pipes and fittings can be deflected angularly as follows:
DN 80 to DN 350 - max. of $3^{\circ}$
DN 400 to DN 600 -max. of $2^{\circ}$

For a pipe length of $6 \mathrm{~m}, 1^{\circ}$ of angular deflection causes the axis of the pipe to lie approx. 10 cm off the axis of the pipe or fitting installed previously, i.e. $3^{\circ}=30 \mathrm{~cm}$. With 5 m long pipes, $1^{\circ}$ corresponds to approx. 9 cm .


## Note on installation

Make sure that, as a function of the internal pressure and the tolerances on joints, it is possible for extensions of up to about 8 mm per joint to occur. To allow for the travel of the pipeline when it extends when pressure is applied, joints at bends should be set to the maximum allowable angular deflection in the negative direction.


## Cutting of pipes

Ensure that the pipes are suitable for cutting (see p. 82).
Copy the line markings from the original spigot end to the new spigot end which has been cut.

## Disassembly

Push the pipe into the socket until it is in abutment.
Apply lubricant to the disassembly plates and, using the striking block. drive them into the gap between the socket and the pipe all round. Then disassemble the joint with the laying tool or the dissembling clamp.

Striking block with
disassembly plates


A dismantling tool consists of a striking block and the number of disassembly plates shown in the table below.


| DN | 80 | 100 | 125 | 150 | 200 | 250 | 300 | 350 | 400 | 500 | 600 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Number <br> of plates | 4 | 4 | 5 | 6 | 8 | 10 | 12 | 14 | 16 | 19 | 23 |

### 8.11 Installation instructions Bolted gland joints

Applicability
These installation instructions apply to ductile iron fittings to EN 545 with bolted gland joints to DIN 28602.
For recommendations for transport, storage and installation, see p. 60.
For laying tools and other accessories, see Chapter 6.

Construction of the joint


Cleaning


Clean the surfaces of the seating for the gasket which are indicated by the arrows and remove any excess paint (paint humps, bubbles or pimples) from them. Use a tool such as a wire brush to clean the seating for the gasket.

Clean the front pressure-applying face of the bolted gland ring thoroughly.


Clean the spigot end for a length of at least 300 mm . Remove any fouling and any excess paint (paint humps, bubbles or pimples).


Assembling the joint
Slide the bolted gland ring and the gasket onto the spigot end.
Important! Do not use any lubricant!


Using a piece of lifting equipment, insert the spigot end into the socket, centralise it and check the depth of insertion. Press the gasket into the sealing chamber to a uniform depth all round.


Slide the bolted gland ring in behind the gasket and centralise it with two hardwood wedges, which can easily be fitted in at the top between the bolted gland ring and the spigot end. When the bolted gland ring is accurately centralised, it is then easy for the tee-head bolts to be inserted.


Insert the tee-head bolts through the flange and the bolted gland ring. Tighten the nuts as far as you can finger-tight, evenly all round. Then tighten the nuts in sequence with a ring spanner, always tightening two diametrically opposed nuts at a time by about half a turn to one full turn.


The gasket has been correctly compressed when the bolted gland ring has been pressed into the gasket to a depth of at least 6 mm .

How deep it has been pressed in can be found by measuring the overall depth of the bolted gland ring, and the depth from the outer face of the bolted gland ring to the gasket once the bolts have been tightened. The depth for which it is pressed in should be as even as possible all round for the given bolted gland joint.


At least three measurements therefore have to be made at each joint. Check the correct depth of insertion again.
Re-paint the tee-head bolts and the nuts with a standard bitumen paint.

Angular deflection
Once the joint has been assembled with the pipe centralised, pipes and fittings can be deflected angularly by.

| Up to | DN 500 | - | $\max$. of $3^{\circ}$ |
| :--- | :--- | :--- | :--- |
|  | DN 700 | - | $\max$. of $2^{\circ}$ |
|  | DN 1,000 | - | $\max$. of $1.5^{\circ}$ |

For a pipe length of $6 \mathrm{~m}, 1^{\circ}$ of angular deflection causes the axis of the pipe to lie approx. 10 cm off the axis of the pipe or fitting installed previously, e.g. $3^{\circ}=30 \mathrm{~cm}$. With 5 m long pipes, $1^{\circ}$ corresponds to approx. 9 cm .


Cutting of pipes
Ensure that the pipes are suitable for cutting (see p. 82)

## Disassembly

Unscrew the nuts and slide back the bolted gland ring.
Pull the spigot end out of the socket.

### 8.12 Cutting of pipes

Suitability for cutting (6 m pipes)
Up to and including a nominal size of DN 300, the pipes supplied can be cut, in the region of the barrel, at points more than 1 m away from the socket, to enable a spigot end for a joint to be formed. Above a nominal size of DN 300 only pipes which carry a continuous longitudinal stripe can be cut. Pipes of this kind ("Schnittrohre" or cuttable pipes) have to be ordered separately. An additional identifier for a cuttable pipe is an "SR" marked on the end-face of the socket.


Suitability for cutting ( 5 m pipes)
Up to and including a nominal size of DN 300, the pipes supplied are within the permitted tolerance range, and can therefore be cut, in the region of the barrel, over $2 / 3$ of their length measured from the spigot end.

Above a nominal size of DN 300 the diameter of the pipes should be checked before they are cut (use a steel measuring tape to compare the circumference of the pipe at the spigot end and at the intended cutting point). Specially marked dimensionally accurate (cuttable) pipes of the kind available as standard up to and including DN 300 can also be ordered. The marking is a red longitudinal strip (approx. 0.5 m long) extending over the socket to the barrel.


Tools
The best way of cutting ductile iron pipes is with cutters using abrasive discs and powered in a variety of ways, e.g. by compressed air, electric motors or petrol engines.

The cutting disc we recommend is the C 24 RT Spezial type made of silicon carbide. These are cutting discs for stone but have proved successful in practice for cutting ductile iron pipes. Protective goggles and respiratory protection must be worn when cutting pipes with a cement mortar coating or lining. All swarf must be carefully removed from inside the pipe.

With pipes of fairly large nominal sizes it may happen that the new spigot ends produced are slightly oval after the pipes have been cut. If this happens, the spigot ends should be re-rounded with suitable devices applied to the inside or outside of the pipe, e.g. hydraulic jacks or re-rounding clamps.
The device should not be removed until after the joint has been fully assembled.


Grinding of cut ends
The cut ends of pipes shortened on site must be bevelled with a grinding disc to match the original spigot ends.
The bevelling should be done as shown in the diagrams.


Repaint the bare metal surface with a paint corresponding to the external protection which the pipe has. A quick drying finishing layer which complies with the requirements of the German Foodstuffs Law is suitable for this purpose.

To speed up the drying process, it is advisable to warm first the pipe ends, and then the paint when it has been applied, with a gas flame.
Then copy the line markings on the original spigot end to the new spigot end which has been cut.


Dimensions for line markings

|  | DN | 80 | 100 | 125 | 150 | 200 | 250 | 300 | 350 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FormA <br> Standard <br> socket | X | $\mathbf{Y}$ | 89 | 73 | 76 | 79 | 85 | 90 | 95 |
|  | 825 | 86 | 89 | 92 | 98 | 103 | 108 | 108 |  |


|  | DN | 400 | 500 | 600 | 700 | 800 | 900 | 1,000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Form A <br> Standard <br> socket | X | 95 | 105 | 105 | 135 | 145 | 160 | 170 |
|  | Y | 108 | 118 | 118 | 148 | 158 | 173 | 183 |
| Form B <br> Long socket | X | - | - | - | 148 | 157 | 167 | 177 |
|  | Y | - | - | - | 161 | 170 | 180 | 190 |

No line marking is used on pipes with VRS ${ }^{\circledR}$-T joints. In place of it, a welded bead has to be applied to cut ends of pipes of this kind. On this point see the installation instructions for $\mathrm{VRS}^{\oplus}-\mathrm{T}$ joints (see p. 71 ff ) and the technical recommendations for welding on the next page.

For cutting pipes with a cement mortar coating, the directions given from $p$. 69 should also be followed.

### 8.13 Technical recommendations <br> for manual metal arc welding

Applicability
Welding work can be done on ductile iron pipes to EN 545 in the following cases:

- on water pipelines having allowable operating pressures (PFA) of up to 16 bars
- for welding on DN 2" ductile iron or steel connections
- for welding on DN 80 to DN 300 ductile iron or steel outlets
- puddle flanges for building pipes into structures
- welded beads for restrained push-injoints

These recommendations do not apply to sand-cast fittings and pipes or to grey ductile iron pipes.

## Pipes with a minimum wall thickness of less than 4.5 mm must not be welded!

## Process and electrodes

The process used should be manual metal arc welding using nickel-based stick electrodes, preferably ones complying with EN ISO 1071.
The recommended electrode types are for example:
Castolin 7330-EC, UTP FN 86, ESAB OK 92.58, Gricast 31 or 32.

Basically, the following standards of the German Welding Society (DVS) also apply:

DVS 1502, Parts 1 \& 2
DVS 1148

The welders used should be qualified under DVS 1148.
${ }^{11}$ Please consult our Applications Engineering Division before you carry out any welding work for the first time.

Preparing for welding work
When welding is being done, the temperature of the pipe wall must not be less than $+20^{\circ} \mathrm{C}$.
The workplace must be dry.

The area to be welded must be bright metal. Remove any fouling or zinc coatings by filing or grinding.

Pinholes should not be welded over. They must be ground out down to solid metal and filled with weld metal. Connectors should be matched to the outside diameter of the barrel of the pipe in such a way that, if at all possible, the gap does not exceed 0.5 mm .

Execution of welding work
Type of current
Either AC or DC can be used for welding work. Follow the guidelines for use issued by the electrode manufacturer.

## Welding parameters

The current levels and rates of deposition specified by the electrode manufacturer should be taken as the guideline values

## Preheating

Preheating is generally an advantage. The area to be welded should be preheated as detailed in Table 1 before the tack welding and before the root pass is welded.

Table 1
Conditions for crack-free welds on ductile iron pipes.

| Making of weld | In at least two passes (inc. for pipe to connectionjoints) |  |  |
| :---: | :---: | :---: | :---: |
| Thickness of pipe wall (actual) | Not filled with water *) |  | Filled with flowing water |
|  | Not cement-mortar lined | Cement-mortar lined | Cement-mortar lined |
| $\geq 4.7$... 6 mm | at $20^{\circ} \mathrm{C}$ | At $20^{\circ} \mathrm{C}$ | Not allowed |
| $6 . .10 \mathrm{~mm}$ | at $20^{\circ} \mathrm{C}$ | At $20^{\circ} \mathrm{C}$ | At $20^{\circ} \mathrm{C}$ |
| $10 . . .12 \mathrm{~mm}$ | Preheat to $150^{\circ} \mathrm{C}$ | At $20^{\circ} \mathrm{C}$ | At $20^{\circ} \mathrm{C}$ |
| $>12 \mathrm{~mm}$ | Preheat to $150^{\circ} \mathrm{C}$ | Preheat to $150^{\circ} \mathrm{C}$ | Preheat to $150^{\circ} \mathrm{C}$ |

*) Also applies to partly filled pipelines when the areas for welding are above the water table
**) Preheating is advisable when the pipe wall temperature is below $20^{\circ} \mathrm{C}$

## Tack welding

Fix the parts to be welded in place with suitable clamping devices. They must be tack welded at at least two points. The angles of the tack welds should be as shallow as possible so that they can be welded over; this can be achieved by grinding them if necessary. Check the tack welds to ensure they are free of cracks. Any cracks in tack welds must be ground out.

## Welding

Any weld must be made as far as possible in a single operation. Interruptions in the welding work should be avoided. Make sure that the preheating temperature is maintained during the welding. If there are interruptions in the welding work, preheat again as in Table 1 before resuming welding.

Welding on of DN 2" ductile iron or steel branch connections
Branch connections are supplied in a ready-to-weld state and can be welded on with fillet welds once the zone for the welding has been prepared and the branch connection has been matched to the outside diameter of the main pipe.
The weld should be made in two passes. The a dimension of the first pass (root pass) should be 3 mm .
The second pass should be a weave pass between the main pipe and the branch connection over the top of the root pass. The finished weld should be flat to slightly concave. The test of the weld for leaktightness should be carried out before the hole is drilled in the main pipe. On water pipelines it should be made at the system test pressure (STP), which is the nominal pressure +5 bars.


Welding on of DN 80 to DN 300 ductile iron or steel outlets
The nominal size of the outlets may not be more than half the nominal size of the main pipe. Outlets are to be welded on with fillet welds. The welding should generally be done in two passes. The a dimension of the first pass (root pass) should be at least 3 mm . The second pass should be first a weave pass between the root pass and the main pipe and then a weave pass between the root pass and the outlet. The finished weld should be flat to slightly concave and its a dimension should be $0.7 \mathrm{~s}-05$ ( $s=$ thickness of the outlet). On outlets of DN 250 and DN 300 nominal size, a final pass may also be welded to give the a dimension.

It may be an advantage for the welding-on of outlets of fairly large sizes to be done with a buffer layer. The test of the weld for leaktightness should be carried out before the hole is drilled in the main pipe. On water pipelines it should be made at the system test pressure (STP), which is the nominal pressure +5 bars.
When new pipelines are being laid it is advisable for outlets to be welded on out of the pipeline trench. In this case the hole in the main pipe can be drilled before the outlet is welded on. The internal pressure test on the outlet can then be carried out together with the pressure test on the pipeline.


Welding on of ductile iron or steel puddle flanges
Pipes with puddle flanges are used to allow pipes to be built into structures. By welding it is possible for puddle flanges to be fastened in place at any desired point along the barrel of a pipe. Puddle flanges are supplied in annular sections and should be fitted tightly to the pipe.

## Welding

Puddle flanges should be welded on with at least two-pass fillet welds and the a dimension of the welds should not be less than 4 mm . On pipes of fairly large sizes with corresponding wall thicknesses it is advisable for a buffer layer to be used.

The length of the weld should be decided on in line with the operating
requirement (allowable thrust ${ }_{z u}=130 \mathrm{~N} / \mathrm{mm}^{2}$ ).
After being welded on, annular sections should be welded together.


## Application of welded beads

When pipes with positive locking restrained push-injoints are cut on site, the welded beads have to be applied to the new spigot ends.
The procedure, accessories and dimensions for this are given in the installation instructions under "Cutting of pipes".

Heat treatment after welding
No heat treatment of welded joints or welded parts is required after they have been welded. The area of the weld should be cleaned once it has cooled and, after checking, should be carefully repainted with a protective paint such for example as a bitumen-based one.

## Checking of welds

Welds should generally undergo a visual inspection and, where necessary, a non-destructive test for surface flaws and cracks.
Welds which are not called upon to be leaktight, such as those fixing puddle flanges for example, should be randomly checked for surface flaws.

Flaws, such as surface pores or cracks in or next to the weld, which are found in the course of checking or testing should be fully ground out before they are repaired. Flaws may only be repaired once.

### 8.14 Pressure testing

Under EN 805, pipelines have to be subjected to an internal pressure test, For water pipelines, the codes governing the execution of this pressure test are EN 805 or DVGW directive W 400-2.

Test sections
It may be necessary for pipelines of quite a considerable length to be divided into sections. The test sections should be decided on in such a way that

- the test pressure is reached at the lowest point of each test section.
- at least 1.1 times the system test pressure (MDP) is reached at the highest point of each test section.
- the amount of water required for the test can be supplied and drained away.
- the maximum length of a test section is not more than $2.5-3 \mathrm{~km}$.

The pipeline should be vented as thoroughly as possible, using "pigs" if necessary, and should be filled with drinking water from the lowest point.

## Backfilling and restraint

If necessary, pipelines must be covered with backfill material before the pressure test to avoid any changes in length. Backfilling around the joints is optional.

At their ends and at bends, branches and tapers, non-restrained pipelines must be anchored to resist the forces generated by the internal pressure. The thrust blocks required for this purpose should be dimensioned as directed in GW 310.

There is no need for thrust blocks to be installed for restrained systems provided that GW 368 has been observed in deciding on the lengths to be restrained.

There is no point in carrying out a pressure test against a closed shut-off valve. The temperature at the outer wall of the pipeline should be kept as constant as possible and must not exceed $20^{\circ} \mathrm{C}$.


## Filling the pipeline

It is useful for the pipeline to be filled from the lowest point so that the air contained in it is able to escape easily from venting points of adequate size provided at the highest points of the pipeline.

We recommend the following filling rates in $1 / \mathrm{s}$

| DN | 100 | 150 | 200 | 250 | 300 | 400 | 500 | 600 | 700 | 800 | 900 | 1,000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Filling <br> rate | 0.3 | 0.7 | 1.5 | 2 | 3 | 6 | 9 | 14 | 19 | 25 | 32 | 40 |

For drinking water pipelines, initial disinfection should be carried out in conjunction with the pressure test. This requires a concentration of at least 50 mg of chlorine per litre of water. Depending on how dirty the pipeline is, the level of chlorine may be increased to up to 150 mg per litre of water. The relationship between the amount of water added and the increase in pressure obtained may serve as an indication of any leaks or of inadequate venting. As the pressure increases, the water consumption should therefore be noted bar by bar.

| in litres |  |  |  |
| :--- | :--- | :--- | :--- |
|  | bar | mm |  |
|  | $0-1$ |  |  |
|  | $1-2$ |  |  |
| Water <br> consumption <br> forl bar | $2-3$ |  |  |

Where a pipeline has been properly laid and is properly vented, the amount of water which needs to be pumped in per bar of increased pressure is approximately constant. Allowing for the compressibility of water and the elastic properties of the pipes, this amount is (theoretically) approximately 50 ml per cubic metre of space within the pipeline per bar. In practice, this figure is around 1.5 to 2 times higher because air trapped in the joints of pipes and fittings and in valves has to be compressed.

The Table shows the amounts of water required, in litres per bar of increased pressure, for pipeline lengths from 100 to $1,000 \mathrm{~m}$, including a 100\% allowance for trapped air.

| DN | Amounts of water in litres per bar of increased pressure. for pipeline lengths [m] given in the column headings |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 100 | 200 | 300 | 400 | 500 | 600 | 700 | 800 | 900 | 1,000 |
| 80 | 0.05 | 0.09 | 0.14 | 0.19 | 0.24 | 0.28 | 0.33 | 0.38 | 0.42 | 0.47 |
| 100 | 0.07 | 0.13 | 0.20 | 0.26 | 0.33 | 0.39 | 0.45 | 0.52 | 0.59 | 0.65 |
| 125 | 0.12 | 0.24 | 0.36 | 0.48 | 0.60 | 0.72 | 0.84 | 0.96 | 1.05 | 1.20 |
| 150 | 0.18 | 0.35 | 0.53 | 0.70 | 0.87 | 1.05 | 1.22 | 1.40 | 1.54 | 1.75 |
| 200 | 0.32 | 0.64 | 0.97 | 1.28 | 1.60 | 1.93 | 2.25 | 2.55 | 2.90 | 3.20 |
| 250 | 0.52 | 1.04 | 1.57 | 2.10 | 2.60 | 3.15 | 3.65 | 4.20 | 4.70 | 5.20 |
| 300 | 0.78 | 1.56 | 2.35 | 3.15 | 3.90 | 4.67 | 5.45 | 6.25 | 7.05 | 7.80 |
| 350 | 1.06 | 2.12 | 3.20 | 4.25 | 5.30 | 6.38 | 7.43 | 8.50 | 9.55 | 10.60 |
| 400 | 1.44 | 2.90 | 4.30 | 5.80 | 7.20 | 8.65 | 10.10 | 11.55 | 13.00 | 14.40 |
| 500 | 2.35 | 4.70 | 7.05 | 9.40 | 11.80 | 13.10 | 16.20 | 18.80 | 21.10 | 23.50 |
| 600 | 3.45 | 7.00 | 10.50 | 14.00 | 17.15 | 21.00 | 24.50 | 28.00 | 31.50 | 35.00 |

Performing a pressure test
The following procedures for performing a pressure test on ductile iron pipes are described in DVGW directive W 400-2:

- standard procedure (for pipes of all nominal sizes, with or without a cement mortar lining)
- shortened standard procedure (for pipes of nominal sizes up to DN 600 with a cement mortar lining)

We describe below the two procedures which are most frequently followed, the standard procedure and the shortened standard procedure.
In both these procedures the level of test pressure is as follows:

- for pipelines with an allowable operating pressure of up to 10 bars: $1.5 \times$ nominal pressure
- for pipelines with an allowable operating pressure of above 10 bars: nominal pressure +5 bars.

The standard procedure
The standard procedure is carried out in three phases:

- preliminary test
- pressure drop test
- maintest

Preliminary test
The purpose of the preliminary test is to saturate the cement mortar lining and to extend the pipeline. To do this, the test pressure is kept constant for a period of 24 hours by pumping in more water as and when required. If any leaks are found or any changes in length exceeding the allowable limits occur, the pipeline must be de-pressurised and the reason found and remedied.

## Pressure drop test

The purpose of the pressure drop test is to establish that the pipeline is free of air. Pockets of air in the pipeline may result in incorrect measurements and may mask small leaks.

A volume of water $\Delta V$ sufficient to cause a drop in pressure $\Delta p$ of at least 0.5 bars is drawn off from the pipeline. The volume of water $\Delta \mathrm{V}$ drawn off is measured. The pipeline must then be re-pressurised to the test pressure.

The pipeline is considered to have been adequately vented if $\Delta \mathrm{V}$ is no greater than the allowable change in volume $\Delta \mathrm{V}_{\text {zul. }}$ If it is greater, then the pipeline must be vented again.
$\Delta V_{z u l}$ is calculated as follows:
$\Delta V_{z u l}=1,5 \cdot a \cdot \Delta p \cdot L$
$\Delta \mathrm{V}_{\mathrm{zul}}=$ allowable change in volume $\left[\mathrm{cm}^{3}\right]$
$\Delta \mathrm{p}=$ measured drop in pressure [bar]
$\mathrm{L} \quad=$ length of the section tested [m]
a $=$ pressure constant characteristic of the size of pipe
[cm³/(bar x m)]
$\rightarrow$ see Table below

| DN | $a$ | DN | $a$ |
| :---: | :---: | :---: | :---: |
| 80 | 0.314 | 400 | 9.632 |
| 100 | 0.492 | 500 | 15.614 |
| 125 | 0.792 | 600 | 23.178 |
| 150 | 1.163 | 700 | 32.340 |
| 200 | 2.147 | 800 | 43.243 |
| 250 | 3.482 | 900 | 55.679 |
| 300 | 5.172 | 1,000 | 69.749 |
| 350 | 7.147 | 1,200 | 103.280 |

Maintest
Following the pressure drop test, the main test is then carried out.

The duration of the test is as follows:

| Up to | DN 400 | 3 h |
| :--- | :--- | :--- |
|  | DN 500 to DN 700 | 12 h |
| more than | DN 700 | 24 h |

The test conditions are considered to have been met if the pressure loss at the end of the test is no higher than is specified below:

| Nominal pressure | Test pressure | Max. pressure loss |
| :---: | :---: | :---: |
| 10 | 15 bar | 0.1 bar |
| 16 | 21 bar | 0.15 bar |
| more than 16 | $\mathrm{PN}+5 \mathrm{bar}$ | 0.2 bar |

Test report
A test report should be produced. Templates for test reports are included in DVGW directive W 400-2. The details required, such as the following, can be seen in these templates:

- description of the pipeline
- test parameters
- description of the performance of the test
- findings during the test
- note indicating report has been checked

The shortened standard procedure
The advantage of the shortened standard procedure is above all that it saves an enormous amount of time. The time required is only about 1.5 hours.

The shortened standard procedure is carried out in three phases:

- saturation phase
- pressure drop test
- leak test


## Saturation phase

To achieve a high level of saturation, the test pressure is kept constant for half an hour by pumping in more water as and when required. The key factor in saturation is first and foremost the level of the test pressure. Unduly low pressure cannot be compensated for by increasing the length of the saturation phase.

## Pressure drop test

The purpose of the pressure drop test is to establish that the pipeline is free of air. Pockets of air in the pipeline may result in incorrect measurements and may mask small leaks.

A volume of water $\Delta V_{z u}$ (see below) is drawn off from the pipeline at the test pressure. The resulting drop in pressure $\Delta \mathrm{p}$ is measured. This becomes the allowable drop in pressure $\Delta p_{z u}$, in the subsequent leak test. The pipeline must be re-pressurised to the test pressure after the pressure drop test.
$\Delta V_{z u}$ is calculated as follows:
$\Delta V_{z u l}=(D N \cdot L) /(100 \cdot k)$

| $\Delta V_{z u l}$ | $=$ | allowable change in volume $\left[\mathrm{cm}^{3}\right]$ |
| :--- | :--- | :--- |
| L | $=$ | length of the section tested $[\mathrm{m}]$ |
| $100 \times \mathrm{k}$ | $=$ | proportionality factor, $\mathrm{k}=1 \mathrm{~m} / \mathrm{cm}^{3}$ |

The pipeline is considered to have been adequately vented if, when the volume of water $\Delta \mathrm{V}_{\text {zu }}$ is drawn off, the drop in pressure is equal to or greater than the minimum levels specified for $\Delta p$ in the table below.

| Nominal size DN | Minimum drop in pressure $p$ <br> [bar] |
| :---: | :---: |
| 80 | 1.4 |
| 100 | 1.2 |
| 150 | 0.8 |
| 200 | 0.6 |
| 300 | 0.4 |
| 400 | 0.3 |
| 500 | 0.2 |
| 600 | 0.1 |

Leak test
The pipeline is considered not to leak if the loss of pressure $\Delta p$ goes down at a constant rate over equal intervals of time and if, over the duration of the leak test, it does not exceed the level $\Delta \mathrm{p}_{\mathrm{zu}}$ found in the pressure drop test.
The duration of the test is one hour.


Test report
A test report should be produced. Templates for test reports are included in DVGW directive W 400-2. The details required, such as the following, can be seen in these templates:

- description of the pipeline
- test parameters
- description of the performance of the test
- findings during the test
- note indicating report has been checked


### 8.15 Disinfection of drinking water pipelines

Disinfection needs to be carried out both on the drinking water itself and on the infrastructure used to supply it. There are a variety of disinfectants and different methods of disinfection which can be used to produce the disinfectant effect. Only when satisfactory test results have been obtained is the disinfection of a pipeline considered to have been successfully completed.

General
Water supply companies have to provide drinking water which is in a satisfactory state hygienically. This requirement is laid down in the German Foodstuffs and Consumer Goods Law, the Federal Epidemic Control Law and the European Drinking Water Directive. Under these codes, drinking water must be of a nature such that its consumption does not harm public health. A prerequisite for this is that the drinking water pipelines are in a hygienically satisfactory condition.
This is achieved by disinfecting the pipelines.

Disinfection covers all the measures which reduce the number of bacteria in such a way that they do not adversely affect the quality of the water transported in the pipelines. Such measures do relate to the drinking water but they also relate to the infrastructure used to supply it. Under the Foodstuffs and Consumer Goods Law, pipelines are "requisites which are used in distributing drinking water and which thus come into contact with it".

Drinking water pipelines must be disinfected in accordance with DVGW directive W 291. For ductile iron pipes with a cement mortar lining, it is useful for disinfection to be carried out at the same time as the pressure test. When drinking water pipelines are being laid, the greatest possible care should be taken at the outset to stop pipes which will later be carrying water from getting dirty.

You should stop pipes from getting dirty as a result of actions by the personnel, as a result of items of equipment used (dirty rags used to wipe out sockets, etc.) or as a result of pollutants in the air (e.g. oily exhaust fumes from two-stroke pipe cutters). The ends of pipelines should be sealed off tightly in such a way that neither groundwater nor dirty water nor animal life can get in.

Disinfection is essential in the following cases:

- before drinking water pipelines are put into service
- after repairs and other work on the pipeline network
- if the drinking water becomes stagnant
- if drinking water pipelines become polluted with bacteria


## Flushing out of drinking water pipelines

Under DVGW directive W 291, flushing out with drinking water is the simplest means of reducing the concentration of bacteria and is normally all that is needed for pipelines of small nominal sizes up to DN 150. It is possible that this will make any additional disinfection unnecessary.

When flushing out takes place, ensure that the flow velocity is high enough (at least $1.5 \mathrm{~m} / \mathrm{s}$ ). The flushing action can be boosted by simultaneous pigging or by flushing out with a mixture of air and water.

The volume of water available to flush out the pipeline should be at least 3 to 5 times the capacity of the pipeline (for pipes of DN 150 size and below) or 2 to 3 times the capacity of the pipeline (for pipes of DN 200 size and above).

Attention should be paid to the following points when flushing out pipelines:

- You should only use items of equipment, such as hoses, which are suitable for drinking water and have been flushed out and, if at all possible, disinfected.
- Sloping pipelines should be flushed out from the top downwards.
- Any air which is injected should be free of oil and dust.
- Water from the section flushed out must not get into the supply network or to consumers.
- There must not be any non-allowable drop in pressure on the pipeline network.
- It must not be possible for dirty water to be sucked back into the pipeline when it is being drained.
- After flushing with a mixture of air and water, the pipeline must be fully vented.


## Disinfectants

The choice of disinfectant should be made on the basis of the local conditions. These include for example whether the disinfectant can be properly handled and will be properly effective and whether it can be satisfactorily disposed of. The following are the disinfectants most frequently used for disinfecting drinking water pipelines:

Sodium hypochlorite, potassium permanganate, hydrogen peroxide and chlorine dioxide.

Due to the checks required under the German Hazardous Materials Regulations, a critical view has to be taken of the use of disinfectants containing chlorine. If you cannot manage without a disinfectant, you should use mainly hydrogen peroxide or potassium permanganate. Both of these can be used as a working solution in a concentration which is below the threshold for hazardous materials (see Schlicht, issue $2 / 2003$ of the magazine bbr).

## Sodium hypochlorite ( NaOCl )

Sodium hypochlorite is the most widely used disinfectant.
It is commercially available as a sodium hypochlorite solution (chlorine bleach solution).The solution should contain at least $12 \%$ of free chlorine ( 150 to 160 g of chlorine per litre). Note that when the solution is stored there is a steady fall in the free chlorine content. When solution has been in store for any great length of time, the chlorine content should therefore be checked. A well-tried disinfectant solution for ductile iron pipes with a cement mortar lining is for example a concentration of 50 mg of chlorine per litre of water.

For rechlorination, we recommend using a higher concentration (up to about 150 mg of chlorine per litre of water). The pH of the sodium hypochlorite solution is between 11.5 and 12.5. When a pipeline is being disinfected, such a solution necessarily increases the pH of the water being treated.

We do not advise reducing the pH by mixing acids with the solution because this may cause chlorine gas to be released and may cause an accident. Mixing with very hard water may result in the precipitation of calcium carbonate.
Disinfectant solutions containing chlorine must always be treated to make them safe before they are allowed to make their way into the sewers or any waterways or bodies of water. This can be done by dilution or by chemical neutralisation with sodium thiosulphate. Dechlorination is also possible by filtration through activated carbon filters.

## Hydrogen peroxide $\left(\mathrm{H}_{2} \mathrm{O}_{2}\right)$

Hydrogen peroxide is a colourless liquid which mixes well with water. The commercially available solutions used have concentration of $35 \%$ and $50 \%$. Hydrogen peroxide gradually breaks down into water and oxygen and this process is speeded up by the effects of heat, light and dust and by heavy metal compounds and organic materials. The solution must therefore be stored where none of these things can affect it.

Disinfectants containing hydrogen peroxide solutions are commercially available under a variety of brand names. Commercially available hydrogen peroxide solutions are always diluted before being used for disinfection. They should not be used on site in a concentration of more than $5 \%$. Concentrations of 150 mg per litre of water and standing times of 24 hours have proved suitable for newly laid pipelines. Unlike solutions containing chlorine, hydrogen peroxide can be drained into the sewers at these concentrations. There is normally no need for the solution to be treated before it is drained into the sewers.

## Potassium permanganate $\left(\mathrm{KMnO}_{4}\right)$

Potassium permanganate is available in the form of violet crystals and has a virtually unlimited shelf life in this form. Its solubility in water is very much dependent on temperature ( $28 \mathrm{~g} /$ litre of water at $0^{\circ} \mathrm{C}, 91 \mathrm{~g} /$ litre of water at $30^{\circ} \mathrm{C}$ ). Depending on its concentration, the solution is coloured as follows: deep violet for strong solutions, reddish violet for medium strength solutions and pink for weak solutions.

Being easy to work with and dispose of, potassium permanganate has been increasingly widely used for disinfection in recent years. Disinfection with a potassium permanganate solution is carried in much the same way as with chlorine, except that 3 to $4 \%$ concentrations are used in this case. The concentration used should be about 10 mg of potassium permanganate to 1 litre of water. Potassium permanganate solutions can be completely reduced by adding ascorbic acid (vitamin C). This can be recognised by a change in the colour of the solution from violet to colourless.

## Chlorine dioxide $\left(\mathrm{ClO}_{2}\right)$

Chlorine dioxide is a gas which is freely soluble in water and which is produced from two separate components, namely a sodium chlorite solution and sodium peroxide sulphate. Always follow the manufacturer's instructions when working with the ready-made solution. The container for the concentrated chloride dioxide stock solution ( 0.3 weight\%) must be such that no chlorine dioxide gas is able to escape.

## Chemical properties

In well sealed containers, the individual components for producing chlorine dioxide will remain stable and can be stored almost indefinitely. Chlorine dioxide itself is produced by mixing component 1 and component 2 . Chlorine dioxide may break down into ionic end products when acted on by light and heat. The ready-mixed solution should therefore be stored in a cool, dark place. Under these conditions, a $0.3 \%$ aqueous solution of chlorine dioxide of neutral pH can be kept for around 40 days at $22^{\circ} \mathrm{C}$.

## Stock solution

An aqueous solution of $0.3 \%$ or $3 \mathrm{~g} / \mathrm{litre}$ of $\mathrm{ClO}_{2}$; this is added to the water to obtain the desired concentration of disinfectant.

## Disposal

When water distribution systems are being disinfected, the excess chlorine dioxide and the chlorite, one of the by-products of its chemical reaction, must be de-activated (e.g. with calcium sulphite filters or activated carbon filters) before they are drained into the sewers or an open receiving water.

## Disinfection procedures

Stand-in-place procedure
In this procedure disinfection is achieved by leaving the solution to stand in the pipeline for a fairly long period (not less than 12 hours). It is important in this procedure to ensure that the proportion in which the disinfectant solution is mixed with the water remains constant.
Infeed of the disinfectant solution must not be stopped until the entire pipeline is filled with it. Of course, no disinfectant solution must be allowed to get into any part
of the pipeline network which is in use!

While the solution is left to stand in the pipeline, you should also operate any gate valves or hydrants so that they too are disinfected. If there are very stubborn bacterial deposits in the pipeline it will need to be disinfected more than once. The concentration of the disinfectant solution may be increased in this case. It is also essential for the pipeline to be flushed out again with an adequate volume of water at a high flow velocity. The disinfection process must be repeated until no microbiological contamination is found in the samples taken. When sodium hypochlorite is used, there should still be evidence of chlorine in the water at the end of the stand-in-place period.

## Flow procedure

With pipelines of large nominal sizes, it may be advantageous for the pipelines to be flushed out and disinfected at the same time over quite a long period of time. If this is done, the concentration of the disinfectant in the water flowing out must be checked repeatedly in the course of the flushing-out process.
The total pipeline content should be replaced to 2 to 3 times.

Disinfection during the pressure test
The combining of the disinfection and pressure testing of a pipeline has proved to be a successful technique, the water which is used for the pressure testing being water which already has disinfectant admixed with it. The high pressure forces the disinfectant solution into the pores of the cement mortar lining. With this technique it is essential for the pipeline being disinfected to be isolated from all pipelines which are in service.

## Disinfection measures when work is done on existing pipelines

 When repairs are made or new pipes are connected in at a later date, there are often compelling reasons why a section of a network has to go back into service very quickly, meaning that disinfection cannot be carried out by the procedures described above. Other measures then have to be taken to ensure that the drinking pipeline will be in a satisfactory state hygienically once the work has been completed. For instance, the parts which are installed may already have been washed in clean water or disinfectant solution. Once the work is completed the pipeline should then be flushed out with water at a suitably high flow velocity. Should any additional disinfection of the pipeline be necessary, care must be taken to see that no disinfectant solution gets into any of the adjoining parts of the system. The pipeline may not be put back into operation until it has been thoroughly flushed out.
## Disposal

Disinfectant solutions must be disposed of without any harm being done to the environment. Basically, all the relevant DIN standards and DVGW directive must be observed. Particular note should be taken of DVGW directive W 291 and the European Drinking Water Directive.
Close attention should also be paid to all product-specific information from disinfectant manufacturers, to the safety data sheets and to accident prevention regulations.

Microbiological checks and release for use
Once pipelines have been disinfected, i.e. once the flushing-out has been completed, water samples must be taken from them for microbiological examination. The samples should be taken from the ends of the pipelines and, where the pipelines are of any great length, from individual sections as well. When taking samples, it is imperative that you take the steps specified in the standards document known as "German Standard Methods for the Examination of Water. Wastewater and Sludge" (DEV). These include the draining, cleaning and flame sterilisation of the valves used for sampling.

Under the existing directives and guidelines, disinfection can be regarded as successful if microbiological examination of the water shows that the colony count does not exceed the benchmark figure of 100 per ml of water. At the same time, the water must not contain any Escherichia coli (E. coli) or any coliform bacteria. If either of these requirements is not met, disinfection of the pipeline must be repeated.

Only when the results of the appropriate microbiological examinations show that everything is microbiologically safe can the drinking water pipeline be released for use. In all examinations, the guidelines laid down in the European Drinking Water Directive must be followed.

The disinfection process
To sum up, you must observe the following steps in your procedure when disinfecting drinking water pipelines (see also DVGW directive W 291):

- Flush out the pipeline
- Disinfect the pipeline
- Drain off and if necessary neutralise the disinfectant solution after the appropriate stand-in-place time
- Flush out the pipeline
- Take samples and perform a microbiological examination

Only when the tests give satisfactory results can the pipeline which has been connected in be put into service.
In view of the important function performed by the disinfection of drinking water pipelines, it is essential for the process described above to be adhered to exactly.

### 8.16 Hydraulic calculation of drinking water pipelines

Calculations are needed to ensure that a pipeline will perform properly in hydraulic terms. High flow velocities result in considerable pressure losses. Particularly when pipelines are long, the flow velocity has a major impact on the economics of the supply system as a whole.

Low flow velocities result in the water standing still (stagnating) for long periods. This being the case, it has to be ensured that there is a sufficiently high exchange of water for hygienic reasons (to prevent turbidity and microbial contamination).

The texts governing the hydraulic dimensioning of water pipelines are DVGW directive GW 303-1 and DVGW directive GW 400-1. The optimum flow velocities as a function of the type of pipeline (main pipeline, connecting pipeline, etc.) are specified in GW 400-1. These are mainly between $1.0 \mathrm{~m} / \mathrm{s}$ and $2.0 \mathrm{~m} / \mathrm{s}$.

GW 303-1 has something to say about, amongst other things, the operating roughness ( $k 2$, which is referred to as $k i$ - integral roughness - in it) of pipeline networks. What are subsumed under integral roughness are all the features of a pipeline or pipeline network which set up a resistance to flow, such as the roughness of the walls, socket transitions, deposits, and the effect of components inserted in pipelines (valves, bends, tapers, etc.). The following standard values have been laid down which apply equally to all pipeline materials:
$\mathrm{ki}=0.1 \mathrm{~mm} \quad$ for trunk mains and feeder mains which
run for a considerable distance
$\mathrm{ki}=0.4 \mathrm{~mm} \quad$ for pipelines which run largely for a considerable distance
$\mathrm{ki}=1.0 \mathrm{~mm} \quad$ for new networks; this is an approximation which takes into account a high level of interconnection.

From the tables given below it is possible to make a rough estimate of the flow velocity ( $v$ ) and the pressure losses ( $I$ ). as a function of the DN, integral roughness (ki) and the volumetric flow rate (Q)

A calculation tool for the hydraulic calculation of ductile iron pipes is available for downloading free of charge at www.eadips.org

Pressure loss table for DN 80

| Q [l/s] | DN80 |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | v [m/s] | $\begin{gathered} k=0.1 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{k}_{\mathrm{k}}=0.4 \\ \mathrm{~J} / \mathrm{m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{k}_{\mathrm{k}}=1.0 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ |
| 0.50 | 0.10 | 0.232 | 0.258 | 0.303 |
| 0.60 | 0.12 | 0.320 | 0.360 | 0.427 |
| 0.70 | 0.14 | 0.420 | 0.477 | 0.572 |
| 0.80 | 0.16 | 0.532 | 0.610 | 0.737 |
| 0.90 | 0.18 | 0.656 | 0.758 | 0.924 |
| 1.00 | 0.20 | 0.791 | 0.992 | 1.130 |
| 1.25 | 0.25 | 1.181 | 1.400 | 1.738 |
| 1.50 | 0.30 | 1.641 | 1.975 | 2.474 |
| 1.75 | 0.35 | 2.171 | 2.645 | 3.339 |
| 2.00 | 0.40 | 2.770 | 3.412 | 4.334 |
| 2.25 | 0.45 | 3.438 | 4.274 | 5.457 |
| 2.50 | 0.50 | 4.173 | 5.233 | 6.710 |
| 2.75 | 0.55 | 4.976 | 6.287 | 8.091 |
| 3.00 | 0.60 | 5.846 | 7.437 | 9.601 |
| 3.25 | 0.65 | 6.784 | 8.683 | 11.240 |
| 3.50 | 0.70 | 7.788 | 10.030 | 13.010 |
| 3.75 | 0.75 | 8.859 | 11.460 | 14.910 |
| 4.00 | 0.80 | 9.996 | 13.000 | 16.930 |
| 4.25 | 0.85 | 11.200 | 14.630 | 19.090 |
| 4.50 | 0.90 | 12.470 | 16.350 | 21.370 |
| 4.75 | 0.94 | 13.810 | 18.170 | 23.780 |
| 5.00 | 0.99 | 15.210 | 20.090 | 26.330 |
| 5.25 | 1.04 | 16.680 | 22.100 | 29.000 |
| 5.50 | 1.09 | 18.210 | 24.210 | 31.800 |
| 5.75 | 1.14 | 19.810 | 26.410 | 34.720 |
| 6.00 | 1.19 | 21.480 | 28.710 | 37.780 |
| 6.25 | 1.24 | 23.210 | 31.100 | 40.970 |
| 6.50 | 1.29 | 25.010 | 33.590 | 44.280 |
| 6.75 | 1.34 | 26.870 | 36.180 | 47.730 |
| 7.00 | 1.39 | 28.800 | 38.860 | 51.300 |
| 7.25 | 1.44 | 30.800 | 41.640 | 55.010 |
| 7.50 | 1.49 | 32.860 | 44.510 | 58.840 |
| 7.75 | 1.54 | 34.980 | 47.480 | 62.800 |
| 8.00 | 1.59 | 37.180 | 50.540 | 66.890 |
| 8.25 | 1.64 | 39.430 | 53.700 | 71.100 |
| 8.50 | 1.69 | 41.760 | 56.960 | 75.450 |
| 8.75 | 1.74 | 44.150 | 60.310 | 79.930 |
| 9.00 | 1.79 | 46.600 | 63.760 | 84.530 |
| 9.25 | 1.84 | 49.120 | 67.300 | 89.270 |
| 9.50 | 1.89 | 51.710 | 70.940 | 94.130 |
| 9.75 | 1.94 | 54.360 | 74.670 | 99.120 |
| 10.00 | 1.99 | 57.070 | 78.500 | 104.200 |
| 10.25 | 2.04 | 59.860 | 82.430 | 109.500 |
| 10.50 | 2.09 | 62.710 | 86.450 | 114.900 |
| 10.75 | 2.14 | 65.620 | 90.570 | 120.400 |
| 11.00 | 2.19 | 68.600 | 94.780 | 126.000 |
| 11.50 | 2.29 | 74.750 | 103.500 | 137.700 |
| 12.00 | 2.39 | 81.170 | 112.600 | 149.900 |
| 12.50 | 2.49 | 87.850 | 122.100 | 162.500 |
| 13.00 | 2.59 | 94.790 | 131.900 | 175.800 |
| 13.50 | 2.69 | 102.000 | 142.200 | 189.500 |
| 14.00 | 2.79 | 109.500 | 152.800 | 203.700 |
| 14.50 | 2.88 | 117.200 | 163.800 | 218.500 |
| 15.00 | 2.98 | 125.200 | 175.200 | 233.700 |
| 15.50 | 3.08 | 133.400 | 187.000 | 249.500 |
| 16.00 | 3.18 | 141.900 | 199.100 | 265.800 |
| 16.50 | 3.28 | 150.700 | 211.700 | 282.600 |
| 17.00 | 3.38 | 159.700 | 224.600 | 300.000 |
| 17.50 | 3.48 | 169.000 | 237.900 | 317.800 |
| 18.00 | 3.58 | 178.600 | 251.600 | 336.200 |
| 18.50 | 3.68 | 188.400 | 265.600 | 355.100 |
| 19.00 | 3.78 | 198.500 | 280.100 | 374.500 |
| 19.50 | 3.88 | 208.800 | 294.900 | 394.400 |
| 20.00 | 3.98 | 219.400 | 310.200 | 414.800 |
| 20.50 | 4.08 | 230.300 | 325.800 | 435.800 |
| 21.00 | 4.18 | 241.400 | 341.700 | 457.200 |
| 21.50 | 4.28 | 252.800 | 358.100 | 479.200 |
| 22.00 | 4.38 | 264.500 | 374.900 |  |
| 22.50 | 4.48 | 276.400 | 392.000 |  |
| 23.00 | 4.58 | 288.600 | 409.500 |  |
| 23.50 | 4.68 | 301.000 | 427.400 |  |
| 24.00 | 4.77 | 313.700 | 445.700 |  |
| 24.50 | 4.87 | 326.600 | 464.300 |  |
| 25.00 | 4.97 | 339.900 | 483.400 |  |
| 25.50 | 5.07 | 353.300 |  |  |
| 26.00 | 5.17 | 367.100 |  |  |
| 26.50 | 5.27 | 381.100 |  |  |
|  |  |  |  |  |

Pressure loss table for DN 100

| Q [1/s] | DN 100 |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | v [m/s] | $\begin{gathered} \mathrm{k}_{\mathrm{k}}=0.1 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{k}_{\mathrm{k}}=0.4 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{k}_{\mathrm{r}}=1.0 \\ \mathrm{Jm} / \mathrm{km}] \end{gathered}$ |
| 0.60 | 0.08 | 0.110 | 0.120 | 0.137 |
| 0.70 | 0.09 | 0.144 | 0.158 | 0.183 |
| 0.80 | 0.10 | 0.182 | 0.201 | 0.235 |
| 0.90 | 0.11 | 0.224 | 0.249 | 0.293 |
| 1.00 | 0.13 | 0.269 | 0.302 | 0.357 |
| 1.25 | 0.16 | 0.400 | 0.456 | 0.546 |
| 1.50 | 0.19 | 0.554 | 0.639 | 0.774 |
| 1.75 | 0.22 | 0.730 | 0.852 | 1.041 |
| 2.00 | 0.25 | 0.929 | 1.095 | 1.347 |
| 2.25 | 0.29 | 1.149 | 1.367 | 1.693 |
| 2.50 | 0.32 | 1.392 | 1.669 | 2.077 |
| 2.75 | 0.35 | 1.656 | 2.000 | 2.501 |
| 3.00 | 0.38 | 1.941 | 2.361 | 2.964 |
| 3.25 | 0.41 | 2.247 | 2.751 | 3.466 |
| 3.50 | 0.45 | 2.575 | 3.171 | 4.007 |
| 3.75 | 0.48 | 2.924 | 3.620 | 4.587 |
| 4.00 | 0.51 | 3.294 | 4.099 | 5.207 |
| 4.25 | 0.54 | 3.684 | 4.607 | 5.865 |
| 4.50 | 0.57 | 4.096 | 5.144 | 6.563 |
| 4.75 | 0.60 | 4.528 | 5.710 | 7.300 |
| 5.00 | 0.64 | 4.982 | 6.306 | 8.076 |
| 5.25 | 0.67 | 5.456 | 6.932 | 8.891 |
| 5.50 | 0.70 | 5.950 | 7.587 | 9.745 |
| 5.75 | 0.73 | 6.466 | 8.271 | 10.640 |
| 6.00 | 0.76 | 7.002 | 8.984 | 11.570 |
| 6.25 | 0.80 | 7.558 | 9.727 | 12.540 |
| 6.50 | 0.83 | 8.136 | 10.500 | 13.550 |
| 6.75 | 0.86 | 8.733 | 11.300 | 14.600 |
| 7.00 | 0.89 | 9.352 | 12.130 | 15.690 |
| 7.25 | 0.92 | 9.991 | 12.990 | 16.820 |
| 7.50 | 0.95 | 10.650 | 13.880 | 17.990 |
| 7.75 | 0.99 | 11.330 | 14.800 | 19.190 |
| 8.00 | 1.02 | 12.030 | 15.750 | 20.440 |
| 8.25 | 1.05 | 12.750 | 16.730 | 21.720 |
| 8.50 | 1.08 | 13.490 | 17.730 | 23.050 |
| 8.75 | 1.11 | 14.250 | 18.770 | 24.410 |
| 9.00 | 1.15 | 15.040 | 19.840 | 25.810 |
| 9.25 | 1.18 | 15.840 | 20.930 | 27.250 |
| 9.50 | 1.21 | 16.660 | 22.050 | 28.730 |
| 9.75 | 1.24 | 17.510 | 23.210 | 30.250 |
| 10.00 | 1.27 | 18.370 | 24.390 | 31.810 |
| 10.25 | 1.31 | 19.260 | 25.600 | 33.410 |
| 10.50 | 1.34 | 20.160 | 26.850 | 35.050 |
| 10.75 | 1.37 | 21.090 | 28.120 | 36.720 |
| 11.00 | 1.40 | 22.030 | 29.420 | 38.440 |
| 11.50 | 1.46 | 23.980 | 32.110 | 41.980 |
| 12.00 | 1.53 | 26.020 | 34.910 | 45.690 |
| 12.50 | 1.59 | 28.130 | 37.840 | 49.550 |
| 13.00 | 1.66 | 30.330 | 40.880 | 53.570 |
| 13.50 | 1.72 | 32.610 | 44.030 | 57.740 |
| 14.00 | 1.78 | 34.970 | 47.310 | 62.070 |
| 14.50 | 1.85 | 37.410 | 50.700 | 66.550 |
| 15.00 | 1.91 | 39.930 | 54.210 | 71.200 |
| 15.50 | 1.97 | 42.530 | 57.840 | 76.000 |
| 16.00 | 2.04 | 45.220 | 61.590 | 80.950 |
| 16.50 | 2.10 | 47.990 | 65.450 | 86.070 |
| 17.00 | 2.16 | 50.830 | 69.430 | 91.330 |
| 17.50 | 2.23 | 53.760 | 73.520 | 96.760 |
| 18.00 | 2.29 | 56.770 | 77.740 | 102.300 |
| 18.50 | 2.36 | 59.860 | 82.070 | 108.100 |
| 19.00 | 2.42 | 63.040 | 86.520 | 114.000 |
| 19.50 | 2.48 | 66.290 | 91.090 | 120.000 |
| 20.00 | 2.55 | 69.630 | 95.770 | 126.200 |
| 20.50 | 2.61 | 73.040 | 100.600 | 132.600 |
| 21.00 | 2.67 | 76.540 | 105.500 | 139.100 |
| 21.50 | 2.74 | 80.120 | 110.500 | 145.800 |
| 22.00 | 2.80 | 83.780 | 115.700 | 152.600 |
| 22.50 | 2.86 | 87.520 | 120.900 | 159.600 |
| 23.00 | 2.93 | 91.340 | 126.300 | 166.800 |
| 23.50 | 2.99 | 95.240 | 131.800 | 174.100 |
| 24.00 | 3.06 | 99.230 | 137.500 | 181.500 |
| 24.50 | 3.12 | 103.300 | 143.200 | 189.100 |
| 25.00 | 3.18 | 107.400 | 149.100 | 196.900 |
| 25.50 | 3.25 | 111.700 | 155.000 | 204.900 |
| 26.00 | 3.31 | 116.000 | 161.100 | 212.900 |
| 26.50 | 3.37 | 120.400 | 167.300 | 221.200 |
| 27.00 | 3.44 | 124.800 | 173.700 | 229.600 |
|  |  |  |  |  |

Pressure loss table for DN 125

| Q [//s] | DN 125 |  |  |  | Q [1/s] | DN125 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | v [m/s] | $\begin{gathered} \mathrm{ki}=0.1 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{k}=0.4 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{k}=1.0 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ |  | v [m/s] | $\begin{gathered} \mathrm{k}_{\mathrm{k}}=0.1 \\ \mathrm{~J} \mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} k_{k}=0.4 \\ J[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{k}_{\mathrm{k}}=1.0 \\ \mathrm{~J} \mathrm{~m} / \mathrm{km}] \end{gathered}$ |
| 1.00 | 0.08 | 0.090 | 0.098 | 0.112 | 31.00 | 2.50 | 50.71 | 68.96 | 89.97 |
| 1.25 | 0.10 | 0.134 | 0.147 | 0.170 | 31.50 | 2.54 | 52.31 | 71.18 | 92.89 |
| 1.50 | 0.12 | 0.184 | 0.205 | 0.240 | 32.00 | 2.58 | 53.93 | 73.43 | 95.85 |
| 1.75 | 0.14 | 0.242 | 0.272 | 0.321 | 32.50 | 2.62 | 55.58 | 75.72 | 98.85 |
| 2.00 | 0.16 | 0.307 | 0.348 | 0.414 | 33.00 | 2.66 | 57.25 | 78.05 | 101.90 |
| 2.25 | 0.18 | 0.379 | 0.433 | 0.518 | 33.50 | 2.70 | 58.94 | 80.41 | 105.00 |
| 2.50 | 0.20 | 0.458 | 0.527 | 0.635 | 34.00 | 2.74 | 60.67 | 82.81 | 108.20 |
| 2.75 | 0.22 | 0.544 | 0.630 | 0.762 | 34.50 | 2.78 | 62.41 | 85.24 | 111.30 |
| 3.00 | 0.24 | 0.636 | 0.742 | 0.902 | 35.00 | 2.82 | 64.18 | 87.70 | 114.60 |
| 3.25 | 0.26 | 0.736 | 0.862 | 1.053 | 35.50 | 2.87 | 65.98 | 90.21 | 117.90 |
| 3.50 | 0.28 | 0.841 | 0.992 | 1.216 | 36.00 | 2.91 | 67.80 | 92.74 | 121.20 |
| 3.75 | 0.30 | 0.954 | 1.130 | 1.390 | 36.50 | 2.95 | 69.64 | 95.31 | 124.60 |
| 4.00 | 0.32 | 1.073 | 1.277 | 1.576 | 37.00 | 2.99 | 71.51 | 97.92 | 128.00 |
| 4.25 | 0.34 | 1.198 | 1.433 | 1.773 | 37.50 | 3.03 | 73.40 | 100.60 | 131.50 |
| 4.50 | 0.36 | 1.330 | 1.598 | 1.983 | 38.00 | 3.07 | 75.32 | 103.20 | 135.00 |
| 4.75 | 0.38 | 1.468 | 1.772 | 2.203 | 38.50 | 3.11 | 77.26 | 106.00 | 138.60 |
| 5.00 | 0.40 | 1.613 | 1.954 | 2.436 | 39.00 | 3.15 | 79.23 | 108.70 | 142.20 |
| 5.25 | 0.42 | 1.765 | 2.146 | 2.680 | 39.50 | 3.19 | 81.22 | 111.50 | 145.80 |
| 5.50 | 0.44 | 1.922 | 2.346 | 2.935 | 40.00 | 3.23 | 83.24 | 114.30 | 149.50 |
| 5.75 | 0.46 | 2.086 | 2.555 | 3.203 | 40.50 | 3.27 | 85.28 | 117.20 | 153.30 |
| 6.00 | 0.48 | 2.257 | 2.772 | 3.481 | 41.00 | 3.31 | 87.34 | 120.00 | 157.10 |
| 6.25 | 0.50 | 2.434 | 2.999 | 3.772 | 41.50 | 3.35 | 89.43 | 123.00 | 160.90 |
| 6.50 | 0.52 | 2.617 | 3.234 | 4.074 | 42.00 | 3.39 | 91.55 | 125.90 | 164.80 |
| 6.75 | 0.54 | 2.806 | 3.479 | 4.387 | 42.50 | 3.43 | 93.69 | 128.90 | 168.70 |
| 7.00 | 0.56 | 3.002 | 3.732 | 4.713 | 43.00 | 3.47 | 95.85 | 131.90 | 172.70 |
| 7.25 | 0.59 | 3.204 | 3.993 | 5.049 | 43.50 | 3.51 | 98.04 | 135.00 | 176.70 |
| 7.50 | 0.61 | 3.413 | 4.264 | 5.398 | 44.00 | 3.55 | 100.30 | 138.10 | 180.80 |
| 7.75 | 0.63 | 3.628 | 4.543 | 5.758 | 44.50 | 3.59 | 102.50 | 141.20 | 184.90 |
| 8.00 | 0.65 | 3.849 | 4.831 | 6.130 | 45.00 | 3.63 | 104.80 | 144.40 | 189.10 |
| 8.25 | 0.67 | 4.076 | 5.128 | 6.513 | 45.50 | 3.67 | 107.00 | 147.60 | 193.30 |
| 8.50 | 0.69 | 4.310 | 5.434 | 6.908 | 46.00 | 3.71 | 109.30 | 150.90 | 197.60 |
| 8.75 | 0.71 | 4.550 | 5.749 | 7.314 | 46.50 | 3.75 | 111.70 | 154.10 | 201.90 |
| 9.00 | 0.73 | 4.796 | 6.072 | 7.732 | 47.00 | 3.79 | 114.00 | 157.40 | 206.20 |
| 9.25 | 0.75 | 5.048 | 6.404 | 8.162 | 47.50 | 3.83 | 116.40 | 160.80 | 210.60 |
| 9.50 | 0.77 | 5.307 | 6.745 | 8.603 | 48.00 | 3.87 | 118.80 | 164.20 | 215.10 |
| 9.75 | 0.79 | 5.572 | 7.095 | 9.056 | 48.50 | 3.91 | 121.30 | 167.60 | 219.60 |
| 10.00 | 0.81 | 5.843 | 7.454 | 9.521 | 49.00 | 3.95 | 123.70 | 171.00 | 224.10 |
| 10.50 | 0.85 | 6.404 | 8.197 | 10.480 | 49.50 | 4.00 | 126.20 | 174.50 | 228.70 |
| 11.00 | 0.89 | 6.990 | 8.976 | 11.490 |  |  |  |  |  |
| 11.50 | 0.93 | 7.601 | 9.790 | 12.550 |  |  |  |  |  |
| 12.00 | 0.97 | 8.237 | 10.640 | 13.650 |  |  |  |  |  |
| 12.50 | 1.01 | 8.897 | 11.520 | 14.800 |  |  |  |  |  |
| 13.00 | 1.05 | 9.583 | 12.440 | 16.000 |  |  |  |  |  |
| 13.50 | 1.09 | 10.290 | 13.400 | 17.240 |  |  |  |  |  |
| 14.00 | 1.13 | 11.030 | 14.390 | 18.530 |  |  |  |  |  |
| 14.50 | 1.17 | 11.790 | 15.410 | 19.870 |  |  |  |  |  |
| 15.00 | 1.21 | 12.570 | 16.470 | 21.250 |  |  |  |  |  |
| 15.50 | 1.25 | 13.380 | 17.570 | 22.680 |  |  |  |  |  |
| 16.00 | 1.29 | 14.220 | 18.700 | 24.150 |  |  |  |  |  |
| 16.50 | 1.33 | 15.070 | 19.860 | 25.670 |  |  |  |  |  |
| 17.00 | 1.37 | 15.960 | 21.060 | 27.240 |  |  |  |  |  |
| 17.50 | 1.41 | 16.870 | 22.300 | 28.850 |  |  |  |  |  |
| 18.00 | 1.45 | 17.800 | 23.570 | 30.510 |  |  |  |  |  |
| 18.50 | 1.49 | 18.760 | 24.880 | 32.220 |  |  |  |  |  |
| 19.00 | 1.53 | 19.740 | 26.220 | 33.970 |  |  |  |  |  |
| 19.50 | 1.57 | 20.750 | 27.590 | 35.770 |  |  |  |  |  |
| 20.00 | 1.61 | 21.780 | 29.010 | 37.620 |  |  |  |  |  |
| 20.50 | 1.65 | 22.830 | 30.450 | 39.510 |  |  |  |  |  |
| 21.00 | 1.69 | 23.910 | 31.930 | 41.450 |  |  |  |  |  |
| 21.50 | 1.74 | 25.020 | 33.450 | 43.440 |  |  |  |  |  |
| 22.00 | 1.78 | 26.150 | 35.000 | 45.470 |  |  |  |  |  |
| 22.50 | 1.82 | 27.310 | 36.590 | 47.540 |  |  |  |  |  |
| 23.00 | 1.86 | 28.490 | 38.210 | 49.670 |  |  |  |  |  |
| 23.50 | 1.90 | 29.690 | 39.870 | 51.840 |  |  |  |  |  |
| 24.00 | 1.94 | 30.920 | 41.560 | 54.060 |  |  |  |  |  |
| 24.50 | 1.98 | 32.170 | 43.290 | 56.320 |  |  |  |  |  |
| 25.00 | 2.02 | 33.450 | 45.060 | 58.630 |  |  |  |  |  |
| 25.50 | 2.06 | 34.750 | 46.850 | 60.990 |  |  |  |  |  |
| 26.00 | 2.10 | 36.080 | 48.690 | 63.390 |  |  |  |  |  |
| 26.50 | 2.14 | 37.430 | 50.560 | 65.840 |  |  |  |  |  |
| 27.00 | 2.18 | 38.810 | 52.460 | 68.340 |  |  |  |  |  |
| 27.50 | 2.22 | 40.210 | 54.400 | 70.880 |  |  |  |  |  |
| 28.00 | 2.26 | 41.640 | 56.370 | 73.470 |  |  |  |  |  |
| 28.50 | 2.30 | 43.090 | 58.380 | 76.100 |  |  |  |  |  |
| 29.00 | 2.34 | 44.560 | 60.430 | 78.780 |  |  |  |  |  |
| 29.50 | 2.38 | 46.060 | 62.510 | 81.510 |  |  |  |  |  |
| 30.00 | 2.42 | 47.590 | 64.620 | 84.290 |  |  |  |  |  |
| 30.50 | 2.46 | 49.130 | 66.770 | 87.110 |  |  |  |  |  |

Pressure loss table for DN 150 cont.

|  | DN 150 |  |  |  | Q [//s] | DN 150 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Q [//s] | v [m/s] | $\begin{gathered} k_{k}=0.1 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} k=0.4 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{k}_{\mathrm{k}}=1.0 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ |  | v [m/s] | $\begin{gathered} \mathrm{k}_{\mathrm{k}}=0.1 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{k}=0.4 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{k}_{\mathrm{k}}=1.0 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ |
| 1.50 | 0.08 | 0.076 | 0.083 | 0.094 | 12.50 | 0.70 | 3.542 | 4.439 | 5.604 |
| 1.75 | 0.10 | 0.100 | 0.109 | 0.125 | 13.00 | 0.73 | 3.812 | 4.791 | 6.055 |
| 2.00 | 0.11 | 0.127 | 0.139 | 0.161 | 13.50 | 0.75 | 4.091 | 5.155 | 6.523 |
| 2.25 | 0.13 | 0.156 | 0.173 | 0.201 | 14.00 | 0.78 | 4.380 | 5.533 | 7.009 |
| 2.50 | 0.14 | 0.188 | 0.210 | 0.246 | 14.50 | 0.81 | 4.678 | 5.925 | 7.512 |
| 2.75 | 0.15 | 0.223 | 0.250 | 0.295 | 15.00 | 0.84 | 4.986 | 6.329 | 8.033 |
| 3.00 | 0.17 | 0.260 | 0.294 | 0.348 | 15.50 | 0.87 | 5.303 | 6.747 | 8.571 |
| 3.25 | 0.18 | 0.301 | 0.341 | 0.406 | 16.00 | 0.89 | 5.630 | 7.179 | 9.126 |
| 3.50 | 0.20 | 0.343 | 0.392 | 0.468 | 16.50 | 0.92 | 5.967 | 7.623 | 9.699 |
| 3.75 | 0.21 | 0.389 | 0.446 | 0.534 | 17.00 | 0.95 | 6.313 | 8.081 | 10.290 |
| 4.00 | 0.22 | 0.437 | 0.503 | 0.605 | 17.50 | 0.98 | 6.668 | 8.552 | 10.900 |
| 4.25 | 0.24 | 0.487 | 0.564 | 0.680 | 18.00 | 1.01 | 7.033 | 9.037 | 11.520 |
| 4.50 | 0.25 | 0.540 | 0.628 | 0.760 | 18.50 | 1.03 | 7.407 | 9.535 | 12.170 |
| 4.75 | 0.27 | 0.596 | 0.695 | 0.843 | 19.00 | 1.06 | 7.791 | 10.050 | 12.830 |
| 5.00 | 0.28 | 0.654 | 0.766 | 0.932 | 19.50 | 1.09 | 8.184 | 10.570 | 13.500 |
| 5.25 | 0.29 | 0.715 | 0.840 | 1.024 | 20.00 | 1.12 | 8.587 | 11.110 | 14.200 |
| 5.50 | 0.31 | 0.778 | 0.917 | 1.121 | 20.50 | 1.14 | 8.999 | 11.660 | 14.910 |
| 5.75 | 0.32 | 0.844 | 0.998 | 1.222 | 21.00 | 1.17 | 9.421 | 12.220 | 15.640 |
| 6.00 | 0.34 | 0.912 | 1.082 | 1.328 | 21.50 | 1.20 | 9.852 | 12.800 | 16.390 |
| 6.25 | 0.35 | 0.983 | 1.170 | 1.438 | 22.00 | 1.23 | 10.290 | 13.390 | 17.150 |
| 6.50 | 0.36 | 1.056 | 1.260 | 1.552 | 22.50 | 1.26 | 10.740 | 14.000 | 17.930 |
| 6.75 | 0.38 | 1.131 | 1.355 | 1.671 | 23.00 | 1.28 | 11.200 | 14.610 | 18.730 |
| 7.00 | 0.39 | 1.209 | 1.452 | 1.794 | 23.50 | 1.31 | 11.670 | 15.240 | 19.550 |
| 7.25 | 0.40 | 1.290 | 1.553 | 1.922 | 24.00 | 1.34 | 12.150 | 15.890 | 20.380 |
| 7.50 | 0.42 | 1.373 | 1.657 | 2.053 | 24.50 | 1.37 | 12.640 | 16.550 | 21.240 |
| 7.75 | 0.43 | 1.458 | 1.764 | 2.190 | 25.00 | 1.40 | 13.130 | 17.220 | 22.100 |
| 8.00 | 0.45 | 1.546 | 1.875 | 2.330 | 25.50 | 1.42 | 13.640 | 17.900 | 22.990 |
| 8.25 | 0.46 | 1.637 | 1.989 | 2.475 | 26.00 | 1.45 | 14.160 | 18.600 | 23.890 |
| 8.50 | 0.47 | 1.729 | 2.107 | 2.624 | 26.50 | 1.48 | 14.680 | 19.310 | 24.820 |
| 8.75 | 0.49 | 1.824 | 2.228 | 2.778 | 27.00 | 1.51 | 15.220 | 20.030 | 25.750 |
| 9.00 | 0.50 | 1.922 | 2.352 | 2.936 | 27.50 | 1.54 | 15.760 | 20.770 | 26.710 |
| 9.25 | 0.52 | 2.022 | 2.479 | 3.098 | 28.00 | 1.56 | 16.310 | 21.520 | 27.680 |
| 9.50 | 0.53 | 2.125 | 2.610 | 3.265 | 28.50 | 1.59 | 16.880 | 22.280 | 28.680 |
| 9.75 | 0.54 | 2.229 | 2.744 | 3.436 | 29.00 | 1.62 | 17.450 | 23.060 | 29.680 |
| 10.00 | 0.56 | 2.337 | 2.882 | 3.611 | 29.50 | 1.65 | 18.030 | 23.850 | 30.710 |
| 10.50 | 0.59 | 2.559 | 3.166 | 3.975 | 30.00 | 1.68 | 18.620 | 24.650 | 31.750 |
| 11.00 | 0.61 | 2.790 | 3.465 | 4.356 | 30.50 | 1.70 | 19.220 | 25.470 | 32.810 |
| 11.50 | 0.64 | 3.031 | 3.776 | 4.755 | 31.00 | 1.73 | 19.830 | 26.300 | 33.890 |
| 12.00 | 0.67 | 3.282 | 4.101 | 5.171 | 31.50 | 1.76 | 20.450 | 27.140 | 34.990 |
|  |  |  |  |  | 32.00 | 1.79 | 21.080 | 28.000 | 36.100 |
|  |  |  |  |  | 32.50 | 1.81 | 21.720 | 28.870 | 37.230 |
|  |  |  |  |  | 33.00 | 1.84 | 22.370 | 29.750 | 38.380 |
|  |  |  |  |  | 33.50 | 1.87 | 23.020 | 30.650 | 39.540 |
|  |  |  |  |  | 34.00 | 1.90 | 23.690 | 31.560 | 40.730 |
|  |  |  |  |  | 34.50 | 1.93 | 24.370 | 32.490 | 41.930 |
|  |  |  |  |  | 35.00 | 1.95 | 25.050 | 33.420 | 43.150 |
|  |  |  |  |  | 35.50 | 1.98 | 25.750 | 34.370 | 44.380 |
|  |  |  |  |  | 36.00 | 2.01 | 26.450 | 35.330 | 45.630 |
|  |  |  |  |  | 36.50 | 2.04 | 27.160 | 36.310 | 46.900 |
|  |  |  |  |  | 37.00 | 2.07 | 27.890 | 37.300 | 48.190 |
|  |  |  |  |  | 37.50 | 2.09 | 28.620 | 38.300 | 49.490 |
|  |  |  |  |  | 38.00 | 2.12 | 29.360 | 39.320 | 50.820 |
|  |  |  |  |  | 38.50 | 2.15 | 30.110 | 40.350 | 52.160 |
|  |  |  |  |  | 39.00 | 2.18 | 30.870 | 41.390 | 53.510 |
|  |  |  |  |  | 39.50 | 2.21 | 31.640 | 42.450 | 54.890 |
|  |  |  |  |  | 40.00 | 2.23 | 32.420 | 43.520 | 56.280 |
|  |  |  |  |  | 40.50 | 2.26 | 33.210 | 44.600 | 57.690 |
|  |  |  |  |  | 41.00 | 2.29 | 34.010 | 45.700 | 59.120 |
|  |  |  |  |  | 41.50 | 2.32 | 34.820 | 46.810 | 60.560 |
|  |  |  |  |  | 42.00 | 2.35 | 35.630 | 47.930 | 62.020 |
|  |  |  |  |  | 42.50 | 2.37 | 36.460 | 49.070 | 63.500 |
|  |  |  |  |  | 43.00 | 2.40 | 37.290 | 50.220 | 65.000 |
|  |  |  |  |  | 43.50 | 2.43 | 38.140 | 51.380 | 66.510 |
|  |  |  |  |  | 44.00 | 2.46 | 38.990 | 52.550 | 68.040 |
|  |  |  |  |  | 44.50 | 2.48 | 39.860 | 53.740 | 69.590 |
|  |  |  |  |  | 45.00 | 2.51 | 40.730 | 54.950 | 71.160 |
|  |  |  |  |  | 45.50 | 2.54 | 41.610 | 56.160 | 72.740 |
|  |  |  |  |  | 46.00 | 2.57 | 42.500 | 57.390 | 74.340 |
|  |  |  |  |  | 46.50 | 2.60 | 43.400 | 58.630 | 75.960 |
|  |  |  |  |  | 47.00 | 2.62 | 44.310 | 59.890 | 77.590 |
|  |  |  |  |  | 47.50 | 2.65 | 45.230 | 61.160 | 79.250 |
|  |  |  |  |  | 48.00 | 2.68 | 46.160 | 62.440 | 80.920 |
|  |  |  |  |  | 48.50 | 2.71 | 47.100 | 63.740 | 82.610 |
|  |  |  |  |  | 49.00 | 2.74 | 48.050 | 65.040 | 84.310 |
|  |  |  |  |  | 49.50 | 2.76 | 49.010 | 66.370 | 86.030 |
|  |  |  |  |  | 50.00 | 2.79 | 49.980 | 67.700 | 87.780 |
|  |  |  |  |  | 51.00 | 2.85 | 51.940 | 70.410 | 91.310 |

Pressure loss table for DN 200

| Q [//s] | DN200 |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | v [m/s] | $\begin{gathered} \mathrm{ki}=0.1 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{ki}=0.4 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{ki}=1.0 \\ \mathrm{~J} \mathrm{~m} / \mathrm{km}] \end{gathered}$ |
| 2.50 | 0.08 | 0.045 | 0.048 | 0.054 |
| 3.00 | 0.09 | 0.062 | 0.067 | 0.076 |
| 3.50 | 0.11 | 0.081 | 0.089 | 0.102 |
| 4.00 | 0.12 | 0.103 | 0.114 | 0.131 |
| 4.50 | 0.14 | 0.127 | 0.141 | 0.164 |
| 5.00 | 0.15 | 0.154 | 0.172 | 0.200 |
| 5.50 | 0.17 | 0.183 | 0.205 | 0.240 |
| 6.00 | 0.18 | 0.214 | 0.241 | 0.284 |
| 6.50 | 0.20 | 0.247 | 0.280 | 0.331 |
| 7.00 | 0.22 | 0.282 | 0.321 | 0.382 |
| 7.50 | 0.23 | 0.319 | 0.366 | 0.436 |
| 8.00 | 0.25 | 0.359 | 0.413 | 0.494 |
| 8.50 | 0.26 | 0.401 | 0.463 | 0.556 |
| 9.00 | 0.28 | 0.445 | 0.516 | 0.621 |
| 10.00 | 0.31 | 0.539 | 0.630 | 0.762 |
| 11.00 | 0.34 | 0.642 | 0.755 | 0.917 |
| 12.00 | 0.37 | 0.753 | 0.892 | 1.087 |
| 13.00 | 0.40 | 0.872 | 1.039 | 1.271 |
| 14.00 | 0.43 | 1.000 | 1.197 | 1.470 |
| 15.00 | 0.46 | 1.136 | 1.367 | 1.682 |
| 16.00 | 0.49 | 1.280 | 1.548 | 1.909 |
| 17.00 | 0.52 | 1.432 | 1.740 | 2.151 |
| 18.00 | 0.55 | 1.593 | 1.942 | 2.407 |
| 19.00 | 0.58 | 1.762 | 2.156 | 2.677 |
| 20.00 | 0.62 | 1.938 | 2.381 | 2.961 |
| 21.00 | 0.65 | 2.123 | 2.618 | 3.260 |
| 22.00 | 0.68 | 2.316 | 2.865 | 3.573 |
| 23.00 | 0.71 | 2.517 | 3.123 | 3.901 |
| 24.00 | 0.74 | 2.726 | 3.392 | 4.242 |
| 25.00 | 0.77 | 2.943 | 3.673 | 4.598 |
| 26.00 | 0.80 | 3.168 | 3.964 | 4.969 |
| 27.00 | 0.83 | 3.402 | 4.267 | 5.354 |
| 28.00 | 0.86 | 3.643 | 4.581 | 5.753 |
| 29.00 | 0.89 | 3.892 | 4.905 | 6.166 |
| 30.00 | 0.92 | 4.149 | 5.241 | 6.594 |
| 31.00 | 0.95 | 4.414 | 5.588 | 7.036 |
| 32.00 | 0.98 | 4.688 | 5.946 | 7.493 |
| 33.00 | 1.02 | 4.969 | 6.315 | 7.964 |
| 34.00 | 1.05 | 5.258 | 6.695 | 8.449 |
| 35.00 | 1.08 | 5.555 | 7.086 | 8.948 |
| 36.00 | 1.11 | 5.860 | 7.488 | 9.462 |
| 37.00 | 1.14 | 6.174 | 7.901 | 9.990 |
| 38.00 | 1.17 | 6.495 | 8.326 | 10.530 |
| 39.00 | 1.20 | 6.824 | 8.761 | 11.090 |
| 40.00 | 1.23 | 7.161 | 9.208 | 11.660 |
| 41.00 | 1.26 | 7.506 | 9.665 | 12.250 |
| 42.00 | 1.29 | 7.859 | 10.130 | 12.850 |
| 43.00 | 1.32 | 8.219 | 10.610 | 13.460 |
| 44.00 | 1.35 | 8.588 | 11.100 | 14.090 |
| 45.00 | 1.38 | 8.965 | 11.610 | 14.730 |
| 46.00 | 1.42 | 9.350 | 12.120 | 15.390 |
| 47.00 | 1.45 | 9.742 | 12.640 | 16.060 |
| 48.00 | 1.48 | 10.140 | 13.180 | 16.750 |
| 49.00 | 1.51 | 10.550 | 13.720 | 17.450 |
| 50.00 | 1.54 | 10.970 | 14.280 | 18.160 |
| 52.50 | 1.62 | 12.040 | 15.720 | 20.010 |
| 55.00 | 1.69 | 13.170 | 17.230 | 21.950 |
| 57.50 | 1.77 | 14.340 | 18.810 | 23.980 |
| 60.00 | 1.85 | 15.570 | 20.460 | 26.090 |
| 62.50 | 1.92 | 16.840 | 22.180 | 28.300 |
| 65.00 | 2.00 | 18.170 | 23.970 | 30.600 |
| 70.00 | 2.15 | 20.960 | 27.750 | 35.460 |
| 75.00 | 2.31 | 23.960 | 31.800 | 40.680 |
| 80.00 | 2.46 | 27.150 | 36.140 | 46.260 |
| 85.00 | 2.62 | 30.540 | 40.750 | 52.200 |
| 90.00 | 2.77 | 34.120 | 45.640 | 58.490 |
| 95.00 | 2.92 | 37.910 | 50.800 | 65.150 |
| 100.00 | 3.08 | 41.890 | 56.240 | 72.160 |
| 105.00 | 3.23 | 46.070 | 61.960 | 79.530 |
| 110.00 | 3.39 | 50.440 | 67.950 | 87.260 |
| 115.00 | 3.54 | 55.020 | 74.230 | 95.350 |
| 120.00 | 3.69 | 59.790 | 80.770 | 103.800 |
| 125.00 | 3.85 | 64.760 | 87.600 | 112.600 |
| 130.00 | 4.00 | 69.930 | 94.700 | 121.800 |
| 135.00 | 4.15 | 75.290 | 102.100 | 131.300 |
| 140.00 | 4.31 | 80.850 | 109.700 | 141.200 |
| 145.00 | 4.46 | 86.610 | 117.700 | 151.400 |

Pressure loss table for DN 250

| Q [//s] | DN 250 |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | v [m/s] | $\mathrm{k}_{1}=0.1 \mathrm{~J}[\mathrm{~m} / \mathrm{km}]$ | $\mathrm{k}_{\mathrm{i}}=0.4 \mathrm{~J}[\mathrm{~m} / \mathrm{km}]$ | $\left.\mathrm{k}_{\mathrm{i}}=1.0 \mathrm{~J} \mathrm{~m} / \mathrm{km}\right]$ |
| 4.00 | 0.08 | 0.035 | 0.038 | 0.042 |
| 4.50 | 0.09 | 0.043 | 0.047 | 0.053 |
| 5.00 | 0.10 | 0.052 | 0.057 | 0.064 |
| 5.50 | 0.11 | 0.062 | 0.068 | 0.077 |
| 6.00 | 0.12 | 0.072 | 0.079 | 0.090 |
| 6.50 | 0.13 | 0.084 | 0.092 | 0.105 |
| 7.00 | 0.14 | 0.095 | 0.105 | 0.121 |
| 7.50 | 0.15 | 0.108 | 0.120 | 0.138 |
| 8.00 | 0.16 | 0.121 | 0.135 | 0.156 |
| 8.50 | 0.17 | 0.135 | 0.151 | 0.176 |
| 9.00 | 0.18 | 0.150 | 0.168 | 0.196 |
| 10.00 | 0.20 | 0.181 | 0.204 | 0.240 |
| 11.00 | 0.22 | 0.215 | 0.244 | 0.288 |
| 12.00 | 0.24 | 0.252 | 0.288 | 0.341 |
| 13.00 | 0.26 | 0.292 | 0.334 | 0.398 |
| 14.00 | 0.28 | 0.334 | 0.385 | 0.459 |
| 15.00 | 0.30 | 0.379 | 0.438 | 0.525 |
| 16.00 | 0.31 | 0.426 | 0.496 | 0.596 |
| 17.00 | 0.33 | 0.476 | 0.556 | 0.670 |
| 18.00 | 0.35 | 0.529 | 0.620 | 0.749 |
| 19.00 | 0.37 | 0.584 | 0.688 | 0.833 |
| 20.00 | 0.39 | 0.642 | 0.758 | 0.920 |
| 21.00 | 0.41 | 0.702 | 0.833 | 1.013 |
| 22.00 | 0.43 | 0.765 | 0.910 | 1.109 |
| 23.00 | 0.45 | 0.831 | 0.992 | 1.210 |
| 24.00 | 0.47 | 0.899 | 1.076 | 1.315 |
| 25.00 | 0.49 | 0.970 | 1.164 | 1.425 |
| 26.00 | 0.51 | 1.043 | 1.256 | 1.539 |
| 27.00 | 0.53 | 1.119 | 1.350 | 1.658 |
| 28.00 | 0.55 | 1.197 | 1.449 | 1.781 |
| 29.00 | 0.57 | 1.278 | 1.550 | 1.908 |
| 30.00 | 0.59 | 1.361 | 1.655 | 2.039 |
| 31.00 | 0.61 | 1.447 | 1.764 | 2.176 |
| 32.00 | 0.63 | 1.536 | 1.876 | 2.316 |
| 33.00 | 0.65 | 1.627 | 1.991 | 2.461 |
| 34.00 | 0.67 | 1.720 | 2.110 | 2.610 |
| 35.00 | 0.69 | 1.816 | 2.232 | 2.763 |
| 36.00 | 0.71 | 1.915 | 2.357 | 2.921 |
| 37.00 | 0.73 | 2.016 | 2.486 | 3.084 |
| 38.00 | 0.75 | 2.119 | 2.619 | 3.250 |
| 39.00 | 0.77 | 2.225 | 2.754 | 3.421 |
| 40.00 | 0.79 | 2.334 | 2.894 | 3.597 |
| 41.00 | 0.81 | 2.445 | 3.036 | 3.777 |
| 42.00 | 0.83 | 2.558 | 3.182 | 3.961 |
| 43.00 | 0.85 | 2.674 | 3.332 | 4.150 |
| 44.00 | 0.87 | 2.792 | 3.484 | 4.343 |
| 45.00 | 0.89 | 2.913 | 3.641 | 4.540 |
| 46.00 | 0.90 | 3.037 | 3.800 | 4.742 |
| 47.00 | 0.92 | 3.163 | 3.963 | 4.948 |
| 48.00 | 0.94 | 3.291 | 4.130 | 5.158 |
| 49.00 | 0.96 | 3.422 | 4.300 | 5.373 |
| 50.00 | 0.98 | 3.556 | 4.473 | 5.592 |
| 52.50 | 1.03 | 3.900 | 4.921 | 6.160 |
| 55.00 | 1.08 | 4.260 | 5.391 | 6.755 |
| 57.50 | 1.13 | 4.635 | 5.882 | 7.377 |
| 60.00 | 1.18 | 5.026 | 6.394 | 8.026 |
| 62.50 | 1.23 | 5.433 | 6.927 | 8.703 |
| 65.00 | 1.28 | 5.854 | 7.482 | 9.408 |
| 70.00 | 1.38 | 6.745 | 8.655 | 10.900 |
| 75.00 | 1.48 | 7.696 | 9.9140 | 12.500 |
| 80.00 | 1.57 | 8.710 | 11.260 | 14.210 |
| 85.00 | 1.67 | 9.785 | 12.690 | 16.030 |
| 90.00 | 1.77 | 10.920 | 14.200 | 17.960 |
| 95.00 | 1.87 | 12.120 | 15.800 | 20.000 |
| 100.00 | 1.97 | 13.380 | 17.490 | 22.140 |
| 105.00 | 2.07 | 14.700 | 19.260 | 24.400 |
| 110.00 | 2.16 | 16.090 | 21.110 | 26.770 |
| 115.00 | 2.26 | 17.530 | 23.050 | 29.250 |
| 120.00 | 2.36 | 19.040 | 25.080 | 31.830 |
| 125.00 | 2.46 | 20.600 | 27.190 | 34.530 |
| 130.00 | 2.56 | 22.230 | 29.390 | 37.330 |
| 135.00 | 2.66 | 23.920 | 31.670 | 40.250 |
| 140.00 | 2.75 | 25.680 | 34.030 | 43.270 |
| 145.00 | 2.85 | 27.490 | 36.490 | 46.410 |
| 150.00 | 2.95 | 29.360 | 39.020 | 49.650 |
| 155.00 | 3.05 | 31.300 | 41.650 | 53.010 |
| 160.00 | 3.15 | 33.300 | 44.350 | 56.470 |

Pressure loss table for DN 300

| Q [//s] | DN300 |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | v [m/s] | $\begin{gathered} \mathrm{k}=0.1 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \\ \hline \end{gathered}$ | $\begin{gathered} k=0.4 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{k}_{\mathrm{k}}=1.0 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ |
| 6.00 | 0.08 | 0.030 | 0.032 | 0.036 |
| 7.00 | 0.10 | 0.039 | 0.043 | 0.048 |
| 8.00 | 0.11 | 0.050 | 0.054 | 0.061 |
| 9.00 | 0.12 | 0.062 | 0.067 | 0.077 |
| 10.00 | 0.14 | 0.075 | 0.082 | 0.094 |
| 11.00 | 0.15 | 0.089 | 0.098 | 0.113 |
| 12.00 | 0.16 | 0.104 | 0.115 | 0.133 |
| 13.00 | 0.18 | 0.120 | 0.133 | 0.155 |
| 14.00 | 0.19 | 0.137 | 0.153 | 0.179 |
| 15.00 | 0.20 | 0.155 | 0.174 | 0.204 |
| 16.00 | 0.22 | 0.174 | 0.197 | 0.231 |
| 17.00 | 0.23 | 0.194 | 0.220 | 0.260 |
| 18.00 | 0.25 | 0.216 | 0.246 | 0.290 |
| 19.00 | 0.26 | 0.238 | 0.272 | 0.322 |
| 20.00 | 0.27 | 0.261 | 0.300 | 0.356 |
| 22.00 | 0.30 | 0.311 | 0.359 | 0.428 |
| 24.00 | 0.33 | 0.365 | 0.424 | 0.507 |
| 26.00 | 0.35 | 0.423 | 0.493 | 0.593 |
| 28.00 | 0.38 | 0.485 | 0.568 | 0.685 |
| 30.00 | 0.41 | 0.551 | 0.649 | 0.784 |
| 32.00 | 0.44 | 0.620 | 0.734 | 0.889 |
| 34.00 | 0.46 | 0.694 | 0.825 | 1.002 |
| 36.00 | 0.49 | 0.772 | 0.921 | 1.121 |
| 38.00 | 0.52 | 0.853 | 1.022 | 1.246 |
| 40.00 | 0.55 | 0.939 | 1.128 | 1.378 |
| 42.00 | 0.57 | 1.028 | 1.240 | 1.517 |
| 44.00 | 0.60 | 1.121 | 1.357 | 1.663 |
| 46.00 | 0.63 | 1.218 | 1.479 | 1.815 |
| 48.00 | 0.65 | 1.319 | 1.606 | 1.974 |
| 50.00 | 0.68 | 1.424 | 1.738 | 2.139 |
| 52.50 | 0.72 | 1.561 | 1.911 | 2.355 |
| 55.00 | 0.75 | 1.703 | 2.092 | 2.582 |
| 57.50 | 0.78 | 1.852 | 2.281 | 2.819 |
| 60.00 | 0.82 | 2.006 | 2.479 | 3.066 |
| 62.50 | 0.85 | 2.167 | 2.684 | 3.324 |
| 65.00 | 0.89 | 2.333 | 2.898 | 3.592 |
| 70.00 | 0.95 | 2.684 | 3.349 | 4.159 |
| 75.00 | 1.02 | 3.059 | 3.833 | 4.768 |
| 80.00 | 1.09 | 3.458 | 4.350 | 5.418 |
| 85.00 | 1.16 | 3.880 | 4.899 | 6.110 |
| 90.00 | 1.23 | 4.327 | 5.481 | 6.844 |
| 95.00 | 1.30 | 4.797 | 6.095 | 7.619 |
| 100.00 | 1.36 | 5.291 | 6.741 | 8.435 |
| 105.00 | 1.43 | 5.808 | 7.421 | 9.294 |
| 110.00 | 1.50 | 6.350 | 8.132 | 10.190 |
| 115.00 | 1.57 | 6.915 | 8.877 | 11.130 |
| 120.00 | 1.64 | 7.504 | 9.654 | 12.120 |
| 125.00 | 1.70 | 8.116 | 10.460 | 13.140 |
| 130.00 | 1.77 | 8.752 | 11.300 | 14.210 |
| 135.00 | 1.84 | 9.412 | 12.180 | 15.310 |
| 140.00 | 1.91 | 10.100 | 13.090 | 16.460 |
| 145.00 | 1.98 | 10.800 | 14.030 | 17.650 |
| 150.00 | 2.05 | 11.530 | 15.000 | 18.890 |
| 155.00 | 2.11 | 12.290 | 16.000 | 20.160 |
| 160.00 | 2.18 | 13.070 | 17.040 | 21.480 |
| 165.00 | 2.25 | 13.870 | 18.110 | 22.830 |
| 170.00 | 2.32 | 14.690 | 19.210 | 24.230 |
| 175.00 | 2.39 | 15.540 | 20.340 | 25.670 |
| 180.00 | 2.45 | 16.410 | 21.510 | 27.150 |
| 185.00 | 2.52 | 17.310 | 22.710 | 28.670 |
| 190.00 | 2.59 | 18.230 | 23.940 | 30.240 |
| 195.00 | 2.66 | 19.170 | 25.210 | 31.840 |
| 200.00 | 2.73 | 20.140 | 26.510 | 33.490 |
| 205.00 | 2.79 | 21.130 | 27.840 | 35.180 |
| 210.00 | 2.86 | 22.150 | 29.200 | 36.910 |
| 215.00 | 2.93 | 23.180 | 30.590 | 38.680 |
| 220.00 | 3.00 | 24.250 | 32.020 | 40.500 |
| 225.00 | 3.07 | 25.330 | 33.480 | 42.350 |
| 230.00 | 3.14 | 26.440 | 34.970 | 44.250 |
| 235.00 | 3.20 | 27.570 | 36.500 | 46.190 |
| 240.00 | 3.27 | 28.730 | 38.050 | 48.170 |
| 245.00 | 3.34 | 29.910 | 39.640 | 50.190 |
| 250.00 | 3.41 | 31.110 | 41.270 | 52.250 |
| 255.00 | 3.48 | 32.340 | 42.920 | 54.360 |
| 260.00 | 3.54 | 33.590 | 44.610 | 56.500 |
| 265.00 | 3.61 | 34.860 | 46.330 | 58.690 |
| 270.00 | 3.68 | 36.160 | 48.080 | 60.920 |
|  |  |  |  |  |

Pressure loss table for DN 400

| Q [//s] | DN 400 |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | v [m/s] | $\begin{gathered} \mathrm{k}_{\mathrm{k}}=0.1 \\ \mathrm{~J} \mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{k}_{\mathrm{k}}=0.4 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{k}_{\mathrm{k}}=1.0 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ |
| 9.00 | 0.07 | 0.016 | 0.017 | 0.019 |
| 10.00 | 0.08 | 0.020 | 0.021 | 0.023 |
| 12.50 | 0.10 | 0.029 | 0.032 | 0.035 |
| 15.00 | 0.12 | 0.041 | 0.044 | 0.050 |
| 17.50 | 0.14 | 0.054 | 0.059 | 0.067 |
| 20.00 | 0.16 | 0.068 | 0.075 | 0.086 |
| 25.00 | 0.20 | 0.102 | 0.114 | 0.132 |
| 30.00 | 0.24 | 0.142 | 0.161 | 0.188 |
| 35.00 | 0.27 | 0.189 | 0.215 | 0.253 |
| 40.00 | 0.31 | 0.241 | 0.277 | 0.328 |
| 45.00 | 0.35 | 0.300 | 0.347 | 0.413 |
| 50.00 | 0.39 | 0.364 | 0.424 | 0.508 |
| 55.00 | 0.43 | 0.434 | 0.509 | 0.612 |
| 60.00 | 0.47 | 0.510 | 0.602 | 0.726 |
| 65.00 | 0.51 | 0.592 | 0.703 | 0.849 |
| 70.00 | 0.55 | 0.679 | 0.811 | 0.982 |
| 75.00 | 0.59 | 0.773 | 0.926 | 1.125 |
| 80.00 | 0.63 | 0.872 | 1.050 | 1.277 |
| 85.00 | 0.67 | 0.977 | 1.181 | 1.440 |
| 90.00 | 0.71 | 1.088 | 1.319 | 1.611 |
| 95.00 | 0.75 | 1.204 | 1.466 | 1.793 |
| 100.00 | 0.78 | 1.326 | 1.620 | 1.984 |
| 105.00 | 0.82 | 1.454 | 1.781 | 2.185 |
| 110.00 | 0.86 | 1.587 | 1.950 | 2.395 |
| 115.00 | 0.90 | 1.726 | 2.127 | 2.615 |
| 120.00 | 0.94 | 1.871 | 2.312 | 2.845 |
| 125.00 | 0.98 | 2.022 | 2.504 | 3.085 |
| 130.00 | 1.02 | 2.178 | 2.704 | 3.334 |
| 135.00 | 1.06 | 2.339 | 2.911 | 3.593 |
| 140.00 | 1.10 | 2.507 | 3.126 | 3.861 |
| 145.00 | 1.14 | 2.680 | 3.349 | 4.140 |
| 150.00 | 1.18 | 2.859 | 3.579 | 4.427 |
| 155.00 | 1.22 | 3.043 | 3.817 | 4.725 |
| 160.00 | 1.26 | 3.233 | 4.063 | 5.032 |
| 165.00 | 1.29 | 3.429 | 4.316 | 5.349 |
| 170.00 | 1.33 | 3.630 | 4.577 | 5.675 |
| 175.00 | 1.37 | 3.837 | 4.846 | 6.012 |
| 180.00 | 1.41 | 4.050 | 5.122 | 6.358 |
| 185.00 | 1.45 | 4.268 | 5.406 | 6.713 |
| 190.00 | 1.49 | 4.492 | 5.697 | 7.078 |
| 195.00 | 1.53 | 4.721 | 5.996 | 7.453 |
| 200.00 | 1.57 | 4.956 | 6.303 | 7.838 |
| 205.00 | 1.61 | 5.197 | 6.617 | 8.232 |
| 210.00 | 1.65 | 5.443 | 6.939 | 8.636 |
| 215.00 | 1.69 | 5.695 | 7.269 | 9.049 |
| 220.00 | 1.73 | 5.953 | 7.606 | 9.473 |
| 225.00 | 1.77 | 6.216 | 7.951 | 9.905 |
| 230.00 | 1.80 | 6.484 | 8.303 | 10.350 |
| 235.00 | 1.84 | 6.759 | 8.664 | 10.800 |
| 240.00 | 1.88 | 7.039 | 9.031 | 11.260 |
| 245.00 | 1.92 | 7.324 | 9.407 | 11.730 |
| 250.00 | 1.96 | 7.616 | 9.790 | 12.210 |
| 260.00 | 2.04 | 8.215 | 10.580 | 13.210 |
| 270.00 | 2.12 | 8.837 | 11.400 | 14.240 |
| 280.00 | 2.20 | 9.481 | 12.250 | 15.310 |
| 290.00 | 2.28 | 10.150 | 13.130 | 16.410 |
| 300.00 | 2.35 | 10.840 | 14.040 | 17.560 |
| 310.00 | 2.43 | 11.550 | 14.980 | 18.740 |
| 320.00 | 2.51 | 12.280 | 15.950 | 19.970 |
| 330.00 | 2.59 | 13.040 | 16.960 | 21.230 |
| 340.00 | 2.67 | 13.820 | 17.990 | 22.530 |
| 350.00 | 2.75 | 14.620 | 19.050 | 23.870 |
| 360.00 | 2.83 | 15.440 | 20.150 | 25.250 |
| 370.00 | 2.90 | 16.290 | 21.270 | 26.670 |
| 380.00 | 2.98 | 17.150 | 22.430 | 28.120 |
| 390.00 | 3.06 | 18.050 | 23.620 | 29.620 |
| 400.00 | 3.14 | 18.960 | 24.830 | 31.150 |
| 410.00 | 3.22 | 19.890 | 26.080 | 32.720 |
| 420.00 | 3.30 | 20.850 | 27.360 | 34.330 |
| 430.00 | 3.37 | 21.830 | 28.670 | 35.980 |
| 440.00 | 3.45 | 22.830 | 30.000 | 37.670 |
| 450.00 | 3.53 | 23.860 | 31.370 | 39.390 |
| 460.00 | 3.61 | 24.910 | 32.770 | 41.160 |
| 470.00 | 3.69 | 25.980 | 34.200 | 42.960 |
| 480.00 | 3.77 | 27.070 | 35.670 | 44.800 |
| 490.00 | 3.85 | 28.180 | 37.160 | 46.690 |
| 500.00 | 3.92 | 29.320 | 38.680 | 48.610 |
|  |  |  |  |  |

Pressure loss table for DN 500

| Q [//s] | DN500 |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | v [m/s] | $\begin{gathered} \mathrm{k}^{2}=0.1 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{k}=0.4 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{k}_{1}=1.00 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ |
| 15.00 | 0.008 | 0.0014 | 0.0015 | 0.0016 |
| 17.50 | 0.009 | 0.0018 | 0.0019 | 0.0022 |
| 20.00 | 0.100 | 0.0023 | 0.0025 | 0.0028 |
| 25.00 | 0.130 | 0.0035 | 0.0037 | 0.0042 |
| 30.00 | 0.150 | 0.0048 | 0.0052 | 0.0060 |
| 35.00 | 0.180 | 0.0063 | 0.0070 | 0.0080 |
| 40.00 | 0.200 | 0.0081 | 0.0090 | 0.1040 |
| 45.00 | 0.230 | 0.1000 | 0.1120 | 0.1300 |
| 50.00 | 0.250 | 0.1210 | 0.1370 | 0.1600 |
| 55.00 | 0.280 | 0.1450 | 0.1640 | 0.1920 |
| 60.00 | 0.300 | 0.1700 | 0.1930 | 0.2270 |
| 65.00 | 0.330 | 0.1970 | 0.2250 | 0.2660 |
| 70.00 | 0.350 | 0.2250 | 0.2590 | 0.3070 |
| 75.00 | 0.380 | 0.2560 | 0.2960 | 0.3510 |
| 80.00 | 0.400 | 0.2880 | 0.3350 | 0.3980 |
| 85.00 | 0.430 | 0.3230 | 0.3760 | 0.4490 |
| 90.00 | 0.450 | 0.3590 | 0.4200 | 0.5020 |
| 95.00 | 0.480 | 0.3970 | 0.4660 | 0.5580 |
| 100.00 | 0.500 | 0.4360 | 0.5140 | 0.6170 |
| 105.00 | 0.530 | 0.4780 | 0.5650 | 0.6790 |
| 110.00 | 0.550 | 0.5210 | 0.6180 | 0.7440 |
| 115.00 | 0.580 | 0.5660 | 0.6740 | 0.8120 |
| 120.00 | 0.600 | 0.6130 | 0.7320 | 0.8830 |
| 125.00 | 0.630 | 0.6620 | 0.7920 | 0.9570 |
| 130.00 | 0.650 | 0.7130 | 0.8540 | 1.0034 |
| 135.00 | 0.680 | 0.7650 | 0.9190 | 1.1140 |
| 140.00 | 0.700 | 0.8190 | 0.9870 | 1.1970 |
| 145.00 | 0.730 | 0.8750 | 1.0056 | 1.2830 |
| 150.00 | 0.750 | 0.9320 | 1.1280 | 1.3720 |
| 155.00 | 0.780 | 0.9920 | 1.2030 | 1.4630 |
| 160.00 | 0.800 | 1.0053 | 1.2800 | 1.5580 |
| 165.00 | 0.830 | 1.1160 | 1.3590 | 1.6560 |
| 170.00 | 0.850 | 1.1810 | 1.4400 | 1.7570 |
| 175.00 | 0.880 | 1.2470 | 1.5240 | 1.8600 |
| 180.00 | 0.900 | 1.3160 | 1.6100 | 1.9670 |
| 185.00 | 0.930 | 1.3860 | 1.6990 | 2.0076 |
| 190.00 | 0.950 | 1.4570 | 1.7900 | 2.1890 |
| 195.00 | 0.980 | 1.5310 | 1.8830 | 2.3040 |
| 200.00 | 1.000 | 1.6060 | 1.9790 | 2.4230 |
| 205.00 | 1.003 | 1.6830 | 2.0077 | 2.5440 |
| 210.00 | 1.005 | 1.7620 | 2.1770 | 2.6690 |
| 215.00 | 1.008 | 1.8430 | 2.2800 | 2.7960 |
| 220.00 | 1.100 | 1.9250 | 2.3850 | 2.9270 |
| 225.00 | 1.130 | 2.0009 | 2.4920 | 3.0060 |
| 230.00 | 1.150 | 2.0095 | 2.6020 | 3.1960 |
| 235.00 | 1.180 | 2.1830 | 2.7140 | 3.3350 |
| 240.00 | 1.200 | 2.2720 | 2.8290 | 3.4780 |
| 245.00 | 1.230 | 2.3640 | 2.9460 | 3.6230 |
| 250.00 | 1.250 | 2.4570 | 3.0065 | 3.7710 |
| 260.00 | 1.300 | 2.6480 | 3.3110 | 4.0076 |
| 270.00 | 1.350 | 2.8460 | 3.5660 | 4.3930 |
| 280.00 | 1.400 | 3.0051 | 3.8300 | 4.7220 |
| 290.00 | 1.450 | 3.2630 | 4.1040 | 5.0063 |
| 300.00 | 1.500 | 3.4820 | 4.3870 | 5.4160 |
| 310.00 | 1.550 | 3.7090 | 4.6800 | 5.7800 |
| 320.00 | 1.600 | 3.9420 | 4.9820 | 6.1570 |
| 330.00 | 1.650 | 4.1820 | 5.2940 | 6.5450 |
| 340.00 | 1.700 | 4.4290 | 5.6150 | 6.9450 |
| 350.00 | 1.750 | 4.6830 | 5.9450 | 7.3580 |
| 360.00 | 1.800 | 4.9450 | 6.2850 | 7.7820 |
| 370.00 | 1.850 | 5.2130 | 6.6350 | 8.2170 |
| 380.00 | 1.900 | 5.4880 | 6.9940 | 8.6650 |
| 390.00 | 1.950 | 5.7700 | 7.3620 | 9.1250 |
| 400.00 | 2.000 | 6.0059 | 7.7400 | 9.5960 |
| 410.00 | 2.006 | 6.3550 | 8.1270 | 10.0080 |
| 420.00 | 2.110 | 6.6590 | 8.5230 | 10.5700 |
| 430.00 | 2.160 | 6.9690 | 8.9290 | 11.0080 |
| 440.00 | 2.210 | 7.2860 | 9.3450 | 11.6000 |
| 450.00 | 2.260 | 7.6100 | 9.7700 | 12.1300 |
| 460.00 | 2.310 | 7.9410 | 10.2000 | 12.6700 |
| 470.00 | 2.360 | 8.2790 | 10.6500 | 13.2300 |
| 480.00 | 2.410 | 8.6240 | 11.1000 | 13.7900 |
| 490.00 | 2.460 | 8.9760 | 11.5600 | 14.3700 |
| 500.00 | 2.510 | 9.3350 | 12.0040 | 14.9600 |
| 525.00 | 2.630 | 10.2600 | 13.2600 | 16.4900 |
| 550.00 | 2.760 | 11.2300 | 14.5400 | 18.0090 |
| 575.00 | 2.880 | 12.2500 | 15.8800 | 19.7700 |
|  |  |  |  |  |

Pressure loss table for DN 600

| Q [//s] | DN 600 |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | v [m/s] | $\begin{gathered} \mathrm{ki}=0.1 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{ki}=0.4 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{ki}=1.0 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ |
| 25.00 | 0.09 | 0.014 | 0.015 | 0.017 |
| 30.00 | 0.10 | 0.020 | 0.021 | 0.024 |
| 35.00 | 0.12 | 0.026 | 0.028 | 0.032 |
| 40.00 | 0.14 | 0.033 | 0.036 | 0.041 |
| 45.00 | 0.16 | 0.041 | 0.045 | 0.051 |
| 50.00 | 0.17 | 0.050 | 0.055 | 0.063 |
| 55.00 | 0.19 | 0.059 | 0.066 | 0.075 |
| 60.00 | 0.21 | 0.069 | 0.077 | 0.089 |
| 65.00 | 0.23 | 0.080 | 0.090 | 0.104 |
| 70.00 | 0.24 | 0.092 | 0.103 | 0.120 |
| 75.00 | 0.26 | 0.104 | 0.118 | 0.137 |
| 80.00 | 0.28 | 0.118 | 0.133 | 0.155 |
| 85.00 | 0.30 | 0.131 | 0.149 | 0.174 |
| 90.00 | 0.31 | 0.146 | 0.166 | 0.195 |
| 95.00 | 0.33 | 0.161 | 0.184 | 0.216 |
| 100.00 | 0.35 | 0.177 | 0.203 | 0.239 |
| 110.00 | 0.38 | 0.212 | 0.244 | 0.288 |
| 120.00 | 0.42 | 0.249 | 0.288 | 0.342 |
| 130.00 | 0.45 | 0.288 | 0.336 | 0.400 |
| 140.00 | 0.49 | 0.331 | 0.388 | 0.462 |
| 150.00 | 0.52 | 0.376 | 0.443 | 0.529 |
| 160.00 | 0.56 | 0.425 | 0.501 | 0.601 |
| 170.00 | 0.59 | 0.476 | 0.564 | 0.677 |
| 180.00 | 0.63 | 0.529 | 0.630 | 0.758 |
| 190.00 | 0.66 | 0.586 | 0.700 | 0.843 |
| 200.00 | 0.70 | 0.645 | 0.773 | 0.933 |
| 210.00 | 0.73 | 0.707 | 0.850 | 1.027 |
| 220.00 | 0.76 | 0.772 | 0.930 | 1.126 |
| 230.00 | 0.80 | 0.840 | 1.015 | 1.229 |
| 240.00 | 0.83 | 0.910 | 1.102 | 1.337 |
| 250.00 | 0.87 | 0.983 | 1.194 | 1.450 |
| 260.00 | 0.90 | 1.059 | 1.289 | 1.567 |
| 270.00 | 0.94 | 1.137 | 1.388 | 1.688 |
| 280.00 | 0.97 | 1.218 | 1.490 | 1.814 |
| 290.00 | 1.01 | 1.302 | 1.596 | 1.945 |
| 300.00 | 1.04 | 1.389 | 1.705 | 2.080 |
| 310.00 | 1.08 | 1.478 | 1.819 | 2.219 |
| 320.00 | 1.11 | 1.570 | 1.935 | 2.363 |
| 330.00 | 1.15 | 1.665 | 2.056 | 2.512 |
| 340.00 | 1.18 | 1.763 | 2.180 | 2.665 |
| 350.00 | 1.22 | 1.863 | 2.308 | 2.823 |
| 360.00 | 1.25 | 1.966 | 2.439 | 2.985 |
| 370.00 | 1.29 | 2.071 | 2.574 | 3.152 |
| 380.00 | 1.32 | 2.180 | 2.712 | 3.324 |
| 390.00 | 1.36 | 2.291 | 2.854 | 3.499 |
| 400.00 | 1.39 | 2.405 | 3.000 | 3.680 |
| 410.00 | 1.43 | 2.521 | 3.150 | 3.865 |
| 420.00 | 1.46 | 2.640 | 3.303 | 4.054 |
| 430.00 | 1.49 | 2.762 | 3.459 | 4.248 |
| 440.00 | 1.53 | 2.887 | 3.620 | 4.447 |
| 450.00 | 1.56 | 3.014 | 3.783 | 4.650 |
| 460.00 | 1.60 | 3.144 | 3.951 | 4.857 |
| 470.00 | 1.63 | 3.277 | 4.122 | 5.070 |
| 480.00 | 1.67 | 3.412 | 4.297 | 5.286 |
| 490.00 | 1.70 | 3.550 | 4.475 | 5.507 |
| 500.00 | 1.74 | 3.691 | 4.657 | 5.733 |
| 520.00 | 1.81 | 3.981 | 5.032 | 6.198 |
| 540.00 | 1.88 | 4.282 | 5.422 | 6.681 |
| 560.00 | 1.95 | 4.593 | 5.825 | 7.183 |
| 580.00 | 2.02 | 4.915 | 6.244 | 7.702 |
| 600.00 | 2.09 | 5.248 | 6.676 | 8.240 |
| 625.00 | 2.17 | 5.679 | 7.238 | 8.937 |
| 650.00 | 2.26 | 6.127 | 7.822 | 9.663 |
| 675.00 | 2.35 | 6.592 | 8.429 | 10.420 |
| 700.00 | 2.43 | 7.074 | 9.058 | 11.200 |
| 725.00 | 2.52 | 7.573 | 9.710 | 12.010 |
| 750.00 | 2.61 | 8.089 | 10.380 | 12.850 |
| 775.00 | 2.69 | 8.621 | 11.080 | 13.720 |
| 800.00 | 2.78 | 9.170 | 11.800 | 14.610 |
| 825.00 | 2.87 | 9.736 | 12.540 | 15.540 |
| 850.00 | 2.95 | 10.320 | 13.310 | 16.490 |
| 875.00 | 3.04 | 10.920 | 14.100 | 17.470 |
| 900.00 | 3.13 | 11.540 | 14.910 | 18.480 |
| 925.00 | 3.22 | 12.170 | 15.740 | 19.520 |
| 950.00 | 3.30 | 12.820 | 16.600 | 20.580 |
| 975.00 | 3.39 | 13.490 | 17.470 | 21.680 |
| 1,000.00 | 3.48 | 14.170 | 18.370 | 22.800 |
| 1,050.00 | 3.65 | 15.590 | 20.240 | 25.130 |

Pressure loss table for DN 700

| Q [//s] | DN700 |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | v [m/s] | $\begin{gathered} \hline \mathrm{k}=0.1 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{k} \mathrm{k}=0.4 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \hline \mathrm{k}=1.0 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ |
| 30.00 | 0.08 | 0.010 | 0.010 | 0.011 |
| 35.00 | 0.09 | 0.013 | 0.013 | 0.015 |
| 40.00 | 0.10 | 0.016 | 0.017 | 0.019 |
| 45.00 | 0.12 | 0.020 | 0.021 | 0.024 |
| 50.00 | 0.13 | 0.024 | 0.026 | 0.029 |
| 55.00 | 0.14 | 0.028 | 0.031 | 0.035 |
| 60.00 | 0.15 | 0.033 | 0.036 | 0.041 |
| 65.00 | 0.17 | 0.038 | 0.042 | 0.048 |
| 70.00 | 0.18 | 0.044 | 0.048 | 0.055 |
| 75.00 | 0.19 | 0.050 | 0.055 | 0.063 |
| 80.00 | 0.21 | 0.056 | 0.062 | 0.071 |
| 85.00 | 0.22 | 0.063 | 0.070 | 0.080 |
| 90.00 | 0.23 | 0.070 | 0.077 | 0.089 |
| 95.00 | 0.24 | 0.077 | 0.086 | 0.099 |
| 100.00 | 0.26 | 0.084 | 0.095 | 0.110 |
| 110.00 | 0.28 | 0.101 | 0.113 | 0.132 |
| 120.00 | 0.31 | 0.118 | 0.134 | 0.156 |
| 130.00 | 0.33 | 0.137 | 0.156 | 0.182 |
| 140.00 | 0.36 | 0.157 | 0.179 | 0.211 |
| 150.00 | 0.38 | 0.178 | 0.205 | 0.241 |
| 160.00 | 0.41 | 0.201 | 0.232 | 0.274 |
| 170.00 | 0.44 | 0.225 | 0.260 | 0.308 |
| 180.00 | 0.46 | 0.250 | 0.291 | 0.345 |
| 190.00 | 0.49 | 0.277 | 0.323 | 0.383 |
| 200.00 | 0.51 | 0.304 | 0.356 | 0.424 |
| 210.00 | 0.54 | 0.333 | 0.391 | 0.467 |
| 220.00 | 0.56 | 0.364 | 0.428 | 0.511 |
| 230.00 | 0.59 | 0.395 | 0.467 | 0.558 |
| 240.00 | 0.62 | 0.428 | 0.507 | 0.607 |
| 250.00 | 0.64 | 0.462 | 0.549 | 0.658 |
| 260.00 | 0.67 | 0.497 | 0.592 | 0.711 |
| 270.00 | 0.69 | 0.534 | 0.637 | 0.766 |
| 280.00 | 0.72 | 0.572 | 0.684 | 0.822 |
| 290.00 | 0.74 | 0.611 | 0.732 | 0.881 |
| 300.00 | 0.77 | 0.651 | 0.782 | 0.943 |
| 310.00 | 0.80 | 0.693 | 0.834 | 1.006 |
| 320.00 | 0.82 | 0.736 | 0.887 | 1.071 |
| 330.00 | 0.85 | 0.780 | 0.942 | 1.138 |
| 340.00 | 0.87 | 0.825 | 0.998 | 1.207 |
| 350.00 | 0.90 | 0.871 | 1.056 | 1.278 |
| 360.00 | 0.92 | 0.919 | 1.116 | 1.352 |
| 370.00 | 0.95 | 0.968 | 1.177 | 1.427 |
| 380.00 | 0.98 | 1.019 | 1.241 | 1.504 |
| 390.00 | 1.00 | 1.070 | 1.305 | 1.584 |
| 400.00 | 1.03 | 1.123 | 1.372 | 1.665 |
| 410.00 | 1.05 | 1.177 | 1.440 | 1.749 |
| 420.00 | 1.08 | 1.232 | 1.509 | 1.834 |
| 430.00 | 1.10 | 1.288 | 1.580 | 1.922 |
| 440.00 | 1.13 | 1.346 | 1.653 | 2.011 |
| 450.00 | 1.15 | 1.405 | 1.728 | 2.103 |
| 460.00 | 1.18 | 1.465 | 1.804 | 2.197 |
| 470.00 | 1.21 | 1.527 | 1.882 | 2.293 |
| 480.00 | 1.23 | 1.589 | 1.961 | 2.390 |
| 490.00 | 1.26 | 1.653 | 2.042 | 2.490 |
| 500.00 | 1.28 | 1.718 | 2.125 | 2.592 |
| 520.00 | 1.33 | 1.852 | 2.295 | 2.802 |
| 540.00 | 1.39 | 1.991 | 2.472 | 3.020 |
| 560.00 | 1.44 | 2.134 | 2.656 | 3.246 |
| 580.00 | 1.49 | 2.283 | 2.846 | 3.480 |
| 600.00 | 1.54 | 2.437 | 3.042 | 3.723 |
| 625.00 | 1.60 | 2.635 | 3.297 | 4.037 |
| 650.00 | 1.67 | 2.842 | 3.562 | 4.365 |
| 675.00 | 1.73 | 3.056 | 3.838 | 4.705 |
| 700.00 | 1.80 | 3.278 | 4.123 | 5.058 |
| 725.00 | 1.86 | 3.507 | 4.419 | 5.423 |
| 750.00 | 1.92 | 3.745 | 4.725 | 5.802 |
| 775.00 | 1.99 | 3.989 | 5.042 | 6.193 |
| 800.00 | 2.05 | 4.242 | 5.368 | 6.597 |
| 825.00 | 2.12 | 4.502 | 5.705 | 7.014 |
| 850.00 | 2.18 | 4.770 | 6.052 | 7.443 |
| 875.00 | 2.25 | 5.045 | 6.409 | 7.885 |
| 900.00 | 2.31 | 5.329 | 6.777 | 8.340 |
| 925.00 | 2.37 | 5.619 | 7.154 | 8.808 |
| 950.00 | 2.44 | 5.918 | 7.542 | 9.288 |
| 975.00 | 2.50 | 6.224 | 7.941 | 9.781 |
| 1,000.00 | 2.57 | 6.538 | 8.349 | 10.290 |
| 1,050.00 | 2.69 | 7.188 | 9.197 | 11.340 |
| 1,100,00 | 2.82 | 7.869 | 10.090 | 12.440 |

Pressure loss table for DN 800

| Q [//s] | DN 800 |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | v [m/s] | $\begin{gathered} \mathrm{k}_{\mathrm{k}}=0.1 \\ \mathrm{~J} \mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{k}=0.4 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{k}_{\mathrm{k}}=1.0 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ |
| 40.00 | 0.08 | 0.008 | 0.009 | 0.010 |
| 50.00 | 0.10 | 0.012 | 0.013 | 0.015 |
| 60.00 | 0.12 | 0.017 | 0.019 | 0.021 |
| 70.00 | 0.14 | 0.023 | 0.025 | 0.028 |
| 80.00 | 0.16 | 0.029 | 0.032 | 0.036 |
| 90.00 | 0.18 | 0.036 | 0.039 | 0.045 |
| 100.00 | 0.20 | 0.044 | 0.048 | 0.055 |
| 110.00 | 0.22 | 0.052 | 0.057 | 0.066 |
| 120.00 | 0.23 | 0.061 | 0.068 | 0.078 |
| 130.00 | 0.25 | 0.071 | 0.079 | 0.091 |
| 140.00 | 0.27 | 0.081 | 0.091 | 0.105 |
| 150.00 | 0.29 | 0.092 | 0.103 | 0.120 |
| 160.00 | 0.31 | 0.103 | 0.117 | 0.136 |
| 170.00 | 0.33 | 0.116 | 0.131 | 0.153 |
| 180.00 | 0.35 | 0.128 | 0.146 | 0.171 |
| 190.00 | 0.37 | 0.142 | 0.162 | 0.190 |
| 200.00 | 0.39 | 0.156 | 0.179 | 0.210 |
| 210.00 | 0.41 | 0.171 | 0.197 | 0.231 |
| 220.00 | 0.43 | 0.186 | 0.215 | 0.253 |
| 230.00 | 0.45 | 0.202 | 0.234 | 0.277 |
| 240.00 | 0.47 | 0.219 | 0.254 | 0.301 |
| 250.00 | 0.49 | 0.236 | 0.275 | 0.326 |
| 260.00 | 0.51 | 0.254 | 0.297 | 0.352 |
| 270.00 | 0.53 | 0.273 | 0.319 | 0.379 |
| 280.00 | 0.55 | 0.292 | 0.342 | 0.407 |
| 290.00 | 0.57 | 0.312 | 0.366 | 0.436 |
| 300.00 | 0.59 | 0.332 | 0.391 | 0.466 |
| 310.00 | 0.61 | 0.354 | 0.417 | 0.497 |
| 320.00 | 0.63 | 0.375 | 0.443 | 0.529 |
| 330.00 | 0.65 | 0.398 | 0.471 | 0.562 |
| 340.00 | 0.67 | 0.421 | 0.499 | 0.597 |
| 350.00 | 0.68 | 0.444 | 0.528 | 0.632 |
| 375.00 | 0.73 | 0.506 | 0.603 | 0.724 |
| 400.00 | 0.78 | 0.571 | 0.684 | 0.822 |
| 425.00 | 0.83 | 0.641 | 0.770 | 0.927 |
| 450.00 | 0.88 | 0.714 | 0.861 | 1.038 |
| 475.00 | 0.93 | 0.791 | 0.957 | 1.155 |
| 500.00 | 0.98 | 0.872 | 1.058 | 1.278 |
| 525.00 | 1.03 | 0.956 | 1.164 | 1.408 |
| 550.00 | 1.08 | 1.045 | 1.275 | 1.544 |
| 575.00 | 1.13 | 1.137 | 1.391 | 1.686 |
| 600.00 | 1.17 | 1.233 | 1.512 | 1.835 |
| 625.00 | 1.22 | 1.333 | 1.638 | 1.990 |
| 650.00 | 1.27 | 1.437 | 1.770 | 2.151 |
| 675.00 | 1.32 | 1.544 | 1.906 | 2.318 |
| 700.00 | 1.37 | 1.656 | 2.047 | 2.491 |
| 725.00 | 1.42 | 1.771 | 2.194 | 2.671 |
| 750.00 | 1.47 | 1.890 | 2.345 | 2.857 |
| 775.00 | 1.52 | 2.013 | 2.502 | 3.050 |
| 800.00 | 1.57 | 2.139 | 2.663 | 3.248 |
| 825.00 | 1.61 | 2.270 | 2.830 | 3.453 |
| 850.00 | 1.66 | 2.404 | 3.001 | 3.664 |
| 875.00 | 1.71 | 2.542 | 3.178 | 3.881 |
| 900.00 | 1.76 | 2.684 | 3.359 | 4.105 |
| 925.00 | 1.81 | 2.829 | 3.546 | 4.335 |
| 950.00 | 1.86 | 2.979 | 3.738 | 4.571 |
| 975.00 | 1.91 | 3.132 | 3.935 | 4.814 |
| 1,000.00 | 1.96 | 3.289 | 4.137 | 5.062 |
| 1,050.00 | 2.05 | 3.614 | 4.555 | 5.578 |
| 1,100.00 | 2.15 | 3.954 | 4.994 | 6.120 |
| 1,150.00 | 2.25 | 4.310 | 5.453 | 6.686 |
| 1,200.00 | 2.35 | 4.680 | 5.933 | 7.277 |
| 1,250.00 | 2.45 | 5.066 | 6.432 | 7.893 |
| 1,300.00 | 2.54 | 5.467 | 6.952 | 8.535 |
| 1,350.00 | 2.64 | 5.883 | 7.492 | 9.201 |
| 1,400.00 | 2.74 | 6.315 | 8.052 | 9.893 |
| 1,450.00 | 2.84 | 6.761 | 8.632 | 10.610 |
| 1,500.00 | 2.94 | 7.222 | 9.232 | 11.350 |
| 1,550.00 | 3.03 | 7.699 | 9.852 | 12.120 |
| 1,600.00 | 3.13 | 8.191 | 10.490 | 12.910 |
| 1,650.00 | 3.23 | 8.698 | 11.150 | 13.730 |
| 1,700.00 | 3.33 | 9.220 | 11.830 | 14.570 |
| 1,750.00 | 3.42 | 9.757 | 12.540 | 15.430 |
| 1,800.00 | 3.52 | 10.310 | 13.260 | 16.330 |
| 1,850.00 | 3.62 | 10.880 | 14.000 | 17.240 |
| 1,900.00 | 3.72 | 11.460 | 14.760 | 18.180 |
| 1,950.00 | 3.82 | 12.060 | 15.540 | 19.150 |
| 2,000.00 | 3.91 | 12.670 | 16.340 | 20.140 |

Pressure loss table for DN 900

| Q [//s] | DN 900 |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | v [m/s] | $\begin{gathered} \mathrm{ki}=0.1 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \hline \mathrm{ki}=0.4 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{ki}=1.0 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ |
| 50.00 | 0.08 | 0.007 | 0.007 | 0.008 |
| 60.00 | 0.09 | 0.010 | 0.010 | 0.011 |
| 70.00 | 0.11 | 0.013 | 0.014 | 0.015 |
| 80.00 | 0.12 | 0.016 | 0.018 | 0.020 |
| 90.00 | 0.14 | 0.020 | 0.022 | 0.025 |
| 100.00 | 0.15 | 0.025 | 0.027 | 0.030 |
| 110.00 | 0.17 | 0.029 | 0.032 | 0.036 |
| 120.00 | 0.19 | 0.034 | 0.038 | 0.043 |
| 130.00 | 0.20 | 0.040 | 0.044 | 0.050 |
| 140.00 | 0.22 | 0.045 | 0.050 | 0.057 |
| 150.00 | 0.23 | 0.052 | 0.057 | 0.065 |
| 160.00 | 0.25 | 0.058 | 0.065 | 0.074 |
| 170.00 | 0.26 | 0.065 | 0.072 | 0.083 |
| 180.00 | 0.28 | 0.072 | 0.081 | 0.093 |
| 190.00 | 0.29 | 0.080 | 0.089 | 0.104 |
| 200.00 | 0.31 | 0.087 | 0.099 | 0.114 |
| 210.00 | 0.32 | 0.096 | 0.108 | 0.126 |
| 220.00 | 0.34 | 0.104 | 0.118 | 0.138 |
| 230.00 | 0.36 | 0.113 | 0.129 | 0.150 |
| 240.00 | 0.37 | 0.123 | 0.140 | 0.163 |
| 250.00 | 0.39 | 0.132 | 0.151 | 0.177 |
| 260.00 | 0.40 | 0.142 | 0.163 | 0.191 |
| 270.00 | 0.42 | 0.152 | 0.175 | 0.206 |
| 280.00 | 0.43 | 0.163 | 0.188 | 0.221 |
| 290.00 | 0.45 | 0.174 | 0.201 | 0.236 |
| 300.00 | 0.46 | 0.185 | 0.214 | 0.253 |
| 310.00 | 0.48 | 0.197 | 0.228 | 0.270 |
| 320.00 | 0.49 | 0.209 | 0.243 | 0.287 |
| 330.00 | 0.51 | 0.222 | 0.258 | 0.305 |
| 340.00 | 0.53 | 0.234 | 0.273 | 0.323 |
| 350.00 | 0.54 | 0.247 | 0.289 | 0.342 |
| 375.00 | 0.58 | 0.281 | 0.330 | 0.392 |
| 400.00 | 0.62 | 0.318 | 0.374 | 0.445 |
| 425.00 | 0.66 | 0.356 | 0.421 | 0.501 |
| 450.00 | 0.70 | 0.396 | 0.470 | 0.561 |
| 475.00 | 0.73 | 0.439 | 0.522 | 0.624 |
| 500.00 | 0.77 | 0.484 | 0.577 | 0.691 |
| 525.00 | 0.81 | 0.530 | 0.634 | 0.761 |
| 550.00 | 0.85 | 0.579 | 0.695 | 0.834 |
| 575.00 | 0.89 | 0.630 | 0.758 | 0.911 |
| 600.00 | 0.93 | 0.683 | 0.824 | 0.991 |
| 625.00 | 0.97 | 0.738 | 0.892 | 1.074 |
| 650.00 | 1.00 | 0.795 | 0.963 | 1.161 |
| 675.00 | 1.04 | 0.854 | 1.037 | 1.251 |
| 700.00 | 1.08 | 0.915 | 1.114 | 1.345 |
| 725.00 | 1.12 | 0.979 | 1.193 | 1.442 |
| 750.00 | 1.16 | 1.044 | 1.275 | 1.542 |
| 775.00 | 1.20 | 1.111 | 1.360 | 1.646 |
| 800.00 | 1.24 | 1.181 | 1.447 | 1.753 |
| 825.00 | 1.27 | 1.252 | 1.538 | 1.863 |
| 850.00 | 1.31 | 1.326 | 1.630 | 1.977 |
| 875.00 | 1.35 | 1.402 | 1.726 | 2.094 |
| 900.00 | 1.39 | 1.479 | 1.825 | 2.214 |
| 925.00 | 1.43 | 1.559 | 1.926 | 2.338 |
| 950.00 | 1.47 | 1.641 | 2.029 | 2.465 |
| 975.00 | 1.51 | 1.725 | 2.136 | 2.596 |
| 1,000.00 | 1.55 | 1.811 | 2.245 | 2.730 |
| 1,050.00 | 1.62 | 1.989 | 2.472 | 3.008 |
| 1,100.00 | 1.70 | 2.175 | 2.709 | 3.299 |
| 1,150.00 | 1.78 | 2.370 | 2.958 | 3.604 |
| 1,200.00 | 1.85 | 2.572 | 3.217 | 3.922 |
| 1,250.00 | 1.93 | 2.783 | 3.487 | 4.254 |
| 1,300.00 | 2.01 | 3.003 | 3.768 | 4.600 |
| 1,350.00 | 2.09 | 3.230 | 4.060 | 4.958 |
| 1,400.00 | 2.16 | 3.466 | 4.363 | 5.331 |
| 1,450.00 | 2.24 | 3.709 | 4.677 | 5.716 |
| 1,500.00 | 2.32 | 3.961 | 5.001 | 6.115 |
| 1,550.00 | 2.39 | 4.221 | 5.337 | 6.528 |
| 1,600.00 | 2.47 | 4.490 | 5.683 | 6.954 |
| 1,650.00 | 2.55 | 4.766 | 6.040 | 7.394 |
| 1,700.00 | 2.63 | 5.051 | 6.409 | 7.847 |
| 1,750.00 | 2.70 | 5.344 | 6.787 | 8.313 |
| 1,800.00 | 2.78 | 5.645 | 7.177 | 8.793 |
| 1,850.00 | 2.86 | 5.954 | 7.578 | 9.287 |
| 1,900.00 | 2.94 | 6.272 | 7.990 | 9.794 |
| 1,950.00 | 3.01 | 6.598 | 8.412 | 10.310 |
| 2,000.00 | 3.09 | 6.931 | 8.845 | 10.850 |
| 2,050.00 | 3.17 | 7.274 | 9.290 | 11.400 |

Pressure loss table for DN 1000

| Q [1/s] | DN 1000 |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | v [m/s] | $\begin{gathered} \mathrm{k}_{\mathrm{k}}=0.1 \\ \mathrm{~J} \mathrm{~m} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{k}_{\mathrm{k}}=0.4 \\ \mathrm{Jm} / \mathrm{km}] \end{gathered}$ | $\begin{gathered} \mathrm{k}_{\mathrm{k}}=1.0 \\ \mathrm{~J}[\mathrm{~m} / \mathrm{km}] \end{gathered}$ |
| 60.00 | 0.08 | 0.006 | 0.006 | 0.007 |
| 70.00 | 0.09 | 0.008 | 0.008 | 0.009 |
| 80.00 | 0.10 | 0.010 | 0.010 | 0.012 |
| 90.00 | 0.11 | 0.012 | 0.013 | 0.014 |
| 100.00 | 0.13 | 0.015 | 0.016 | 0.018 |
| 110.00 | 0.14 | 0.018 | 0.019 | 0.021 |
| 120.00 | 0.15 | 0.021 | 0.022 | 0.025 |
| 130.00 | 0.16 | 0.024 | 0.026 | 0.029 |
| 140.00 | 0.18 | 0.027 | 0.030 | 0.033 |
| 150.00 | 0.19 | 0.031 | 0.034 | 0.038 |
| 160.00 | 0.20 | 0.035 | 0.038 | 0.043 |
| 170.00 | 0.21 | 0.039 | 0.043 | 0.049 |
| 180.00 | 0.23 | 0.043 | 0.047 | 0.054 |
| 190.00 | 0.24 | 0.047 | 0.053 | 0.060 |
| 200.00 | 0.25 | 0.052 | 0.058 | 0.067 |
| 210.00 | 0.26 | 0.057 | 0.064 | 0.073 |
| 220.00 | 0.28 | 0.062 | 0.069 | 0.080 |
| 230.00 | 0.29 | 0.067 | 0.076 | 0.087 |
| 240.00 | 0.30 | 0.073 | 0.082 | 0.095 |
| 250.00 | 0.31 | 0.079 | 0.089 | 0.103 |
| 260.00 | 0.33 | 0.085 | 0.095 | 0.111 |
| 270.00 | 0.34 | 0.091 | 0.103 | 0.119 |
| 280.00 | 0.35 | 0.097 | 0.110 | 0.128 |
| 290.00 | 0.36 | 0.104 | 0.118 | 0.137 |
| 300.00 | 0.38 | 0.110 | 0.126 | 0.146 |
| 325.00 | 0.41 | 0.128 | 0.146 | 0.171 |
| 350.00 | 0.44 | 0.147 | 0.169 | 0.198 |
| 375.00 | 0.47 | 0.167 | 0.193 | 0.227 |
| 400.00 | 0.50 | 0.188 | 0.218 | 0.257 |
| 425.00 | 0.53 | 0.211 | 0.245 | 0.290 |
| 450.00 | 0.56 | 0.235 | 0.274 | 0.324 |
| 475.00 | 0.59 | 0.260 | 0.304 | 0.361 |
| 500.00 | 0.63 | 0.286 | 0.336 | 0.399 |
| 525.00 | 0.66 | 0.314 | 0.370 | 0.440 |
| 550.00 | 0.69 | 0.342 | 0.405 | 0.482 |
| 575.00 | 0.72 | 0.372 | 0.441 | 0.526 |
| 600.00 | 0.75 | 0.403 | 0.479 | 0.572 |
| 625.00 | 0.78 | 0.436 | 0.519 | 0.620 |
| 650.00 | 0.81 | 0.469 | 0.560 | 0.670 |
| 675.00 | 0.84 | 0.504 | 0.603 | 0.722 |
| 700.00 | 0.88 | 0.540 | 0.647 | 0.776 |
| 725.00 | 0.91 | 0.577 | 0.693 | 0.832 |
| 750.00 | 0.94 | 0.615 | 0.741 | 0.889 |
| 775.00 | 0.97 | 0.655 | 0.790 | 0.949 |
| 800.00 | 1.00 | 0.696 | 0.840 | 1.011 |
| 825.00 | 1.03 | 0.738 | 0.893 | 1.074 |
| 850.00 | 1.06 | 0.781 | 0.946 | 1.140 |
| 875.00 | 1.09 | 0.825 | 1.002 | 1.207 |
| 900.00 | 1.13 | 0.870 | 1.059 | 1.276 |
| 925.00 | 1.16 | 0.917 | 1.117 | 1.348 |
| 950.00 | 1.19 | 0.965 | 1.177 | 1.421 |
| 1,000.00 | 1.25 | 1.064 | 1.302 | 1.573 |
| 1,050.00 | 1.31 | 1.169 | 1.433 | 1.733 |
| 1,100.00 | 1.38 | 1.278 | 1.570 | 1.901 |
| 1,150,00 | 1.44 | 1.391 | 1.714 | 2.076 |
| 1,200.00 | 1.50 | 1.510 | 1.864 | 2.259 |
| 1,250.00 | 1.56 | 1.633 | 2.020 | 2.450 |
| 1,300.00 | 1.63 | 1.761 | 2.182 | 2.649 |
| 1,350.00 | 1.69 | 1.893 | 2.351 | 2.855 |
| 1,400.00 | 1.75 | 2.031 | 2.526 | 3.069 |
| 1,450.00 | 1.81 | 2.173 | 2.707 | 3.291 |
| 1,500.00 | 1.88 | 2.320 | 2.894 | 3.520 |
| 1,550.00 | 1.94 | 2.472 | 3.088 | 3.758 |
| 1,600.00 | 2.00 | 2.628 | 3.288 | 4.003 |
| 1,650.00 | 2.06 | 2.789 | 3.494 | 4.255 |
| 1,700.00 | 2.13 | 2.955 | 3.707 | 4.516 |
| 1,750.00 | 2.19 | 3.126 | 3.926 | 4.784 |
| 1,800.00 | 2.25 | 3.301 | 4.151 | 5.060 |
| 1,850.00 | 2.31 | 3.481 | 4.382 | 5.344 |
| 1,900.00 | 2.38 | 3.666 | 4.619 | 5.635 |
| 1,950.00 | 2.44 | 3.855 | 4.863 | 5.935 |
| 2,000.00 | 2.50 | 4.050 | 5.113 | 6.242 |
| 2,050.00 | 2.56 | 4.249 | 5.370 | 6.556 |
| 2,100.00 | 2.63 | 4.453 | 5.632 | 6.879 |
| 2,150.00 | 2.69 | 4.661 | 5.901 | 7.209 |
| 2,200.00 | 2.75 | 4.874 | 6.176 | 7.547 |
| 2,250.00 | 2.81 | 5.092 | 6.458 | 7.892 |
| 2,300.00 | 2.88 | 5.315 | 6.745 | 8.246 |

9 - SEWAGE

### 9.1 Introduction

Safe and efficient management of sewage and industrial waste water is an essential element of every modern society. In environmentally protected areas in particular, it's very important to pass sewage water through safely and to minimize the risk of contamination in the long term. Every construction project interferes with the environment to a significant degree, which is why it's not enough just to depend on the reliability of the pipe network itself. Rather, the durability of the pipe material contributes to safe sewage management with the lowest maintenance costs. Ductile iron pipe systems from TRM have fulfilled these high demands for decades.

## Advantages of ductile iron pipe systems from TRM:

- One safe and reliable system made entirely of ductile iron
- Large fittings portfolio
- Simple and fast installation
- Maximum lifetimes for pipe networks
- Safe from ingrowing roots
- 100\% diffusion-resistant
- Self-healing outside coatings
- Self-healing cement linings


## What does TRM stand for?

- Optimum support in all stages of your project with our experienced and trained sales team.
- Maximum flexibility and delivery capacity due to an appropriate stock of standard goods
- ISO-9001 certificate
- GRIS certificate
- GSK certificate for fittings
- CE marking

Notes for sewage pipes made of ductile iron We supply ductile iron pipes for sewage water according to EN598:

- VRS ${ }^{\oplus}$-T positive locked joint DN 80 - DN 500
- BLS ${ }^{\oplus}$ positive locked joint DN 600 - DN 1000
- TYTON ${ }^{\oplus}$ push in joint according to DIN 28603 (Form A socket) DN 80 - DN 600
- TYTON ${ }^{\text {® }}$ push in joint according to DIN 28603 (Form B socket) DN 700 - DN 1000

TYTON ${ }^{\oplus}$ rubber gaskets can be supplied in NBR or EPDM. NBR gaskets can be detected easily through their yellow markings.

VRS ${ }^{\oplus}$-T-rubber gaskets can be supplied in EPDM (not available in NBR).

Allowable operation pressure (PFA):
Our ductile iron pipes made according to EN598 can be used for gravity pipelines as well as pressure pipelines for maximum pressure rates that conform to EN598. Higher pressure rates possible upon request.

Coatings

- Inside: standard high alumina cement lining for DN 80-1000 according to EN 598, ONORM B 2562 and DIN 2880.
Inside: alternative cement lining with sophisticated acrylate dispersion for DN 80 500 , specially used for mining penstocks
- Outside: according to EN598, active zinc coating $200 \mathrm{~g} / \mathrm{m}^{2}$ with red-brown finishing layer according to ÖNORM B2560 (PUR long-life polyurethane) or DIN 30674 part 3 (epoxy finishing layer)
- For very aggressive and/or stony soils, pipes can be supplied with premium coatings: ZMU (cement mortar coating according to EN15542) or PUR-TOP coating.

Pipelines at risk from frost above ground (e.g. bridge lines) or installed in ground with less soil coverage (e.g. at tunnel portals) can be optimally protected with our WKG insulation. Please see chapter 7 .
Higher allowable pressures, higher static loads and pipes with different wall thicknesses or our positive locked joints VRS ${ }^{\oplus}-\mathrm{T}$ and $\mathrm{BLS}{ }^{\oplus}$ upon request. Please contact our sales team at office@trm.at

### 9.2 Effluent disposal

Cement mortar lining
For transport of sewage water, our pipes use a high alumina cement lining according to EN 598 and ÖNORM B 2562.

Long-term tests with ductile iron pipe systems using high alumina cement lining for diluted acids and strong bases showed that pH values between 4.5 and 9 are not a problem during continuous operation. Furthermore, this area of application can be enlarged to pH 4-12 for communal sewage pipelines. Upon consultation with our engineering team, this area of application can be enlarged even further. Please contact us with more information (temperature, values of aggressive components, frequencies, etc.) at: office@trm.at

Biogenic sulfur acid corrosion (BSK)
The high alumina cement lining will be applied by centrifugal rotation. This guarantees a constant thickness over the whole pipe length. As a result of the high centrifugal forces during rotation, the cement lining is strongly compacted and a special fine-grained layer is formed on top.
Both factors also increase the high resistance against biogenic sulfuric acid corrosion (BSK) of high alumina cement mortar linings. BSK may occur at the crossover from pressure pipelines to gravity pipelines or pipelines with particularly high stagnation times. High temperatures increase BSK.

The cement lining meets the requirements of the association
"Güteschutzverbandes der Rohre im Siedlungswasserbau" and has GRIS 131 and GRIS 151 certification. As a result of the manufacturing process, hairline cracks may occur on the top of the cement mortar lining. Once the cement comes into contact with water again, it will swell and the hair cracks will close autonomously.

The maximum width of hair cracks according to EN 598:

| DN | Maximum width of hair cracks and maximum <br> radial ofset in mm |
| :--- | :---: |
| $40-300$ | 0,4 |
| $350-600$ | 0,5 |
| $700-1000$ | 0,6 |

The cement mortar lining withstands typical impacts during transport and installation. Ovalities of up to $4 \%$ are within the tolerance range and do not damage the cement mortar lining.

## Abrasion resistance

The strong compression of the cement mortar lining causes high abrasion resistance. The abrasion resistance independent of the pipe material can be verified using the "Darmstädter Kipprinnenversuch" (tip channeling test) according to DIN EN 295-3. Even flow velocities up to $20 \mathrm{~m} / \mathrm{s}$ that may occur in steep slopes can be handled easily. With regard to the abrasion resistance, the cement mortar lining exhibits the best values. The abrasion is between 0.8 and 1.22 mm after 1 million test cycles (equal to a statistic abrasion of 100 years). That's why ductile iron pipes with cement mortar lining are also the best choice for high flow rates. For special industrial applications with a high demand for abrasion resistance, our cement mortar lining can be boosted with a unique, sophisticated acrylate dispersion. In comparison with the standard high-alumina cement, this solvent-free, synthetically modified cement mortar lining exhibits significantly higher chemical and mechanical abrasive resistance, more elasticity and extraordinary adhesive strength, making it the best choice for mining penstocks (slurry transport lines). Damage when flushing the pipeline with high pressure jets up to 250 bar and when adding solid substances (such as gravel) also can be ruled out. The high quality standards of the base material as well as the cement mortar lining meet the requirements of the association "Güteschutzverbandes der Rohre im Siedlungswasserbau" and have GRIS 131 certification.


For drainage canals and pipelines, the operation roughness "kb" is defined in directive ATV A110. The operation roughness "kb" is made up of higher roughness values based on a blanket concept. The blanket concept leads to the same total loss of energy as the sum of individual single and local energy losses. The blanket concept for "kb" includes:

- inside roughness of the pipe material
- inaccuracies and changes in location
- splices of pipes
- intake fittings
- manhole structures

The effective inside pipe roughness of 0.1 is also included.

NOT INCLUDED in blanket concept for "kb" (to be evaluated and calculated separately):

- Difference between calculated and existing clear width
- Merging structures
- Inlets and outlets of throttled lines
- Impact of over-accumulation

Depending on the kind of canal, the values listed below for the "kb" blanket concept are recommended:

| kb <br> $[\mathrm{mm}]$ | Application | Remark |
| :--- | :--- | :--- |
| 0,25 | Throttled lines, pressure pipelines, culvert pipelines and relining <br> without manholes | All DN |
| 0,5 | Transport lines with manholes, collector lines with manholes | All DN up to DN <br> 1000 |
| 0,75 | Transport lines with special manhole structures, collector lines <br> with special manhole structures | All DN |
| 1,5 | Brick wall lines, in-situ concrete lines, other non standardi zed <br> pipes, pipes without verification of internal roughness | All DN |

Alongside the operation roughness "kb" defined in directive ATV A110, a "table book for hydraulic calculation of ductile iron pipes" and "calculation software" are also available on the FGR website www.eadips.org

## Static loads

Ductile iron pipes have the ability to handle massive static loads consisting of earth pressure and traffic loads. For example, the soil coverage can be from 0.3 m up to 9 m depending on the DN, load and installation. Table D. 1 in annex D of EN598 shows possible soil coverage levels. The usage of ductile iron pipes can usually be checked using the above-mentioned table and does not have to be calculated additionally. A separate static calculation according to ÖNORM B 5012 is only needed for special locations or loads (>SWL 60 loads, train or airplane loads). In this case, please contact our sales team at office@trm.at. We would be pleased to provide you with an auditable static calculation that can be double-checked and approved by any authorized structural engineer.

Heights of cover pressure pipes (EN598:2007):

| DN |  | $80-300$ | $350-450$ | $500-2000$ |
| :--- | :--- | :---: | :---: | :---: |
| $\mathrm{~K}(2)$ |  | $0,110\left(20^{\circ}\right)$ | $0,105\left(45^{\circ}\right)$ | $0,103\left(60^{\circ}\right)$ |
| $=0,5$ |  |  |  |  |
| Rural |  |  |  |  |
| areas | $\mathrm{E}^{\prime}=0$ | $0,3-5,0$ | $0,3-3,0$ | $0,4-2,2$ |
|  | $\mathrm{E}^{\prime}=1000$ | $0,3-5,8$ | $0,3-4,0$ | $0,3-3,5$ |
| $=0,75$ | $\mathrm{E}^{\prime}=2000$ | $0,3-6,6$ | $0,3-5,0$ | $0,3-4,7$ |
| Access | $\mathrm{E}^{\prime}=5000$ | $0,3-9,2$ | $0,3-8,0$ | $0,3-7,8$ |
| roads | $\mathrm{E}^{\prime}=0$ | $0,3-4,8$ | $0,5-2,8$ | $0,6-2,0$ |
|  | $\mathrm{E}^{\prime}=1000$ | $0,3-5,7$ | $0,4-3,9$ | $0,4-3,5$ |
| $=1,50$ | $\mathrm{E}^{\prime}=2000$ | $0,3-6,6$ | $0,3-4,9$ | $0,3-4,6$ |
| Main roads | $\mathrm{E}^{\prime}=5000$ | $0,3-9,1$ | $0,3-7,9$ | $0,3-7,8$ |
|  | $\mathrm{E}^{\prime}=0$ | $\mathrm{E}^{\prime}=1000$ | $0,6-4,5$ | 0 |

${ }^{a}$ Not recommended; a specific calculation for each case provides an adequate answer only.

Heights of cover gravity pipelines (EN598:2007):

| DN |  | $80-300$ | 350 |
| :--- | :--- | :--- | :--- |
| K (2) |  | $0,110\left(20^{\circ}\right)$ | $0,105\left(45^{\circ}\right)$ |
| $=0,5$ | $\mathrm{E}^{\prime}=0$ | $0,3-3,2$ | $0,3-9,9$ |
| Rural | $\mathrm{E}^{\prime}=1000$ | $0,3-4,1$ | $0,3-10,6$ |
| areas | $\mathrm{E}^{\prime}=2000$ | $0,3-5,0$ | $0,3-11,3$ |
|  | $\mathrm{E}^{\prime}=5000$ | $0,3-7,5$ | $0,3-13,4$ |
| $=0,75$ | $\mathrm{E}^{\prime}=0$ | $0,3-3,0$ | $0,4-3,4$ |
| Access | $\mathrm{E}^{\prime}=1000$ | $0,3-4,0$ | $0,3-4,4$ |
| roads | $\mathrm{E}^{\prime}=2000$ | $0,3-4,9$ | $0,3-5,4$ |
|  | $\mathrm{E}^{\prime}=5000$ | $0,3-7,5$ | $0,3-8,1$ |
| $=1,50$ | $\mathrm{E}^{\prime}=0$ | $0,3-2,2$ | $a$ |
| Main roads | $\mathrm{E}^{\prime}=1000$ | $0,3-3,5$ | $0,7-4,0$ |
|  | $\mathrm{E}^{\prime}=2000$ | $0,3-4,5$ | $0,6-5,0$ |
|  | $\mathrm{E}^{\prime}=5000$ | $0,3-7,3$ | $0,4-8,0$ |

a) Not recommended; a specific calculation for each case provides an adequate answer only.

Factor $K$ depends on soil stress distribution over the top of the pipe and on the support below. Usually, factor $K$ is between 0.11 (for $2 \mathrm{a}=20^{\circ}$ ) and 0.09 (for $2 a=120^{\circ}$ ). The value for $20^{\circ}$ corresponds to a pipe lying directly on a smooth floor without compaction. Factor $E^{\prime}$ depends on the kind of soil around the pipe and on the conditions during installation. The indication values for $\mathrm{E}^{\prime}$ in the table relate to the compaction of soil at $1,000 \mathrm{kN} / \mathrm{m}^{2}$ (minimal), $2,000 \mathrm{kN} / \mathrm{m}^{2}$ (sufficient) and $5,000 \mathrm{kN} / \mathrm{m}^{2}$ (good). $\mathrm{E}^{\prime}=0$ is the limit value for the worst conditions during installation and the soil (no compaction of soil, groundwater over the pipe, removed sheet pile walls after refilling the trench or the pipeline installed under dam conditions). Please also consider EN805, EN1610, DIN 50929 part 3, ÖNORM 2538 and DIN 30375 part2 for pipe trenches.

| Sewage pipes with positive locking joints $\mathrm{VRS}^{\oplus}-\mathrm{T}-/ \mathrm{BLS}^{\oplus}$ according to EN598 <br> DN 80-500 with push-in joint VRS ${ }^{\oplus}$-T <br> DN 600-1000 with push-in joint BLS ${ }^{\oplus}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inside High alumina cement lining (ZMA) according to ÖNORM B 2562 or DIN <br> coatings: 2880. Other linings upon request. <br> Outside Zinc-coating with finishing layer (DN 80-500 PUR long-life polyurethane <br> coating: coating acc. to ÖNORM B 2560, DN 600-1000 Epoxy coating acc. to DIN 30 <br> 674-3). Cement mortar coating or other coatings upon request. |  |  |  |  |  |  |
| Nominal diameter | Outside diameter | Dimensions [mm] |  | Weight [kg] ~ |  | Laying length |
| DN | $\emptyset \mathrm{d} 1$ | s1 | Cement <br> mortar <br> lining <br> s2 | perm pipe ${ }^{17}$ | per pipe ${ }^{2)}$ | [m] |
| 80 | 98 | 6 | 4 | 15,1 | 75,5 | 5 |
| 100 | 118 | 6 | 4 | 18,7 | 93,5 | 5 |
| 125 | 144 | 6 | 4 | 23,4 | 117 | 5 |
| 150 | 170 | 6 | 4 | 28,4 | 142 | 5 |
| 200 | 222 | 6 | 4 | 36,8 | 184 | 5 |
| 250 | 274 | 6 | 4 | 45,4 | 227 | 5 |
| 300 | 326 | 6,4 | 4 | 57,6 | 288 | 5 |
| 400 | 429 | 7,2 | 5 | 91,5 | 457,5 | 5 |
| 500 | 532 | 8 | 5 | 126 | 630 | 5 |
| 600 | 635 | 9,9 | 5 | 172,9 | 1037 | 6 |
| 700 | 738 | 10,8 | 6 | 224 | 1344 | 6 |
| 800 | 842 | 11,7 | 6 | 275,7 | 1654 | 6 |
| 900 | 945 | 12,6 | 6 | 334,2 | 2005 | 6 |
| 1000 | 1048 | 13,5 | 6 | 397 | 2382 | 6 |

${ }^{10}$ ) Theoretical weight per m pipe incl. cement mortar lining, zinc coating and finishing layer.
${ }^{2}$ ) Theoretical weight of one pipe incl. cement mortar lining, zinc coating and finishing layer. All stated weights are theoretical and standardized values. Higher weights are possible. Other laying lengths and outside coatings upon request.


| Nominal diameter |  | Dimensions [mm] |  |  | Weight[kg] ~ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| DN | dn | A | B | Lu | ductile iron body |
| 200 | 150 | 240 | 145 | 180 | 14,20 |
| $250-300$ | 150 | 240 | 150 | 180 | 14,40 |
| $400-500$ | 150 | 240 | 155 | 180 | 13,50 |
| $600-1000$ | 150 | 240 | 160 | 180 | 13,05 |
| 250 | 200 | 310 | 195 | 220 | 19,25 |
| 300 | 200 | 310 | 200 | 220 | 19,25 |
| $400-500$ | 200 | 310 | 205 | 220 | 19,10 |
| $600-800$ | 200 | 310 | 210 | 220 | 18,90 |

To connect other pipe materials please use junction couplings and gaskets.

Sewage pipes with TYTON ${ }^{\oplus}$ push-injoints (non positive locked) according to EN598 and DIN 28603
DN 150-600 socket A
DN 700-1000 socket B


Inside High alumina cement
coating: lining (ZMA)
Outside Zinc-coating with finishing layer (DN 80-500 PUR long-life polyurethane coating
coating: acc. to ÖNORM B 2560, DN 600-1000 Epoxy coating acc. to DIN 30 674-3).

| Nominal diameter | Outside diameter | Dimensions [mm] |  | Weight [kg] ~ |  | Laying length |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DN | Ød1 | s1 | Cement mortar lining s2 | per m pipe ${ }^{1}$ | per pipe ${ }^{2)}$ | [m] |
| 150 | 170 | 6 | 4 | 27,4 | 137 | 5 |
| 200 | 222 | 6 | 4 | 36,5 | 182,5 | 5 |
| 250 | 274 | 6 | 4 | 43,6 | 218 | 5 |
| 300 | 326 | 6,4 | 4 | 55,3 | 276,5 | 5 |
| 400 | 429 | 7,2 | 5 | 75,7 | 378,5 | 5 |
| 500 | 532 | 8 | 5 | 118,9 | 594,5 | 5 |
| 600 | 635 | 7,7 | 5 | 153 | 917 | 6 |
| 700 | 738 | 9,6 | 6 | 198 | 1184 | 6 |
| 800 | 842 | 10,4 | 6 | 242 | 1453 | 6 |
| 900 | 945 | 11,2 | 6 | 291 | 1745 | 6 |
| 1000 | 1048 | 12 | 6 | 344 | 2063 | 6 |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |

${ }^{12}$ )Theoretical weight per m pipe incl. cement mortar lining, zinc coating and finishing layer.
${ }^{2}$ ) Theoretical weight of one pipe incl. cement mortar lining, zinc coating and finishing layer. All stated weights are theoretical and standardized values. Higher weights are possible. Other laying lengths and outside coatings upon request.

## MMC ALL SOCKET TEE WITH $45^{\circ}$

branch according to EN 598
and TYTON ${ }^{\circledR}$-push-in joint


To connect other pipe materials please use junction couplings and gaskets.

| KPS CLEANOUT COVERS |
| :--- |
| in accordance with EN 598 |
| PFA 6 bars |
| Epoxy coated internally and externally |
| Galvanized steel clamping clips |
| Nominal diameter |
| DN |
| 200 |
| $250-300$ |
| $400-500$ |

KPS CLEANOUT FITTINGS
in accordance with EN598
PFA 6 bars, TYTON ${ }^{\text {® }}$ push-in joint
Epoxy coated internally and externally


| Nominal diameter | Dimensions [mm] |  |  | Weight [kg] ~ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| DN | Lu | A | B | ductile iron body | Cover |
| 150 | 680 | 500 | 140 | 31,25 | 11.0 |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
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|  |  |  |  |  |  |


| KUP TYTON ${ }^{\circ}$ COUPLINGS <br> in accordance with EN 598 PFA 6 bars TYTON ${ }^{\text {® }}$ push-injoint |  |  | $x$ |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
| $\frac{1}{2}$ |  |  |  |
| Nominal diameter | Dimensions[mm] |  | Weight [kg] |
| DN | D | Lu | ductile iron body |
| 150 | 210 | 160 | 8,0 |
| 200 | 262 | 165 | 11,5 |
| 250 | 315 | 180 | 14,5 |
| 300 | 370 | 200 | 20 |
| 400 | 480 | 210 | 32 |
| 500 | 590 | 225 | 45 |
| 600* | 695 | 250 | 56 |
| 700* | 810 | 305 | 97 |
| 800* | 920 | 325 | 128 |
| 900* | 1025 | 350 | 169 |
| 1000* | 1135 | 365 | 205 |

[^14]SAS TYTON ${ }^{\circ}$ MANHOLE CONNECTORS
in accordance with EN 598
TYTON ${ }^{\circledR}$ push-injoint
Epoxy coated internally
Plain metal external surface


| Nominal diameter | Dimensions [mm] |  | Weight [kg] ~ |
| :---: | :---: | :---: | :---: |
| DN | D | Lu | ductile iron body |
| 150 | 280 | 110 | 6,5 |
| 200 | 310 | 110 | 8 |
| 250 | 360 | 110 | 10 |
| 300 | 415 | 110 | 12,5 |
| 400 | 520 | 110 | 16,5 |
| 500 | 635 | 110 | 22 |
| $600^{*}$ | 730 | 120 | 26,5 |
| $700^{*}$ | 845 | 160 | 43 |
| $800^{*}$ | 950 | 160 | 49 |
| $900^{*}$ | 1055 | 175 | 61 |
| $1000^{*}$ | 1160 | 185 | 71,5 |

* Upon request

| SAS VRS ${ }^{\oplus}-\mathrm{T}$ MANHOLE CONNECTORS <br> in accordance with EN 598 <br> VRS®-T positive locked joint <br> Epoxy coated internally <br> Plain metal external surface |  |  |  |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
| Nominal diameter | Dimensions [mm] |  | Weight [kg]~ |
| DN | D | Lu | Cover |
| 80* | 240 | 145 | 6,0 |
| 100* | 260 | 150 | 7,5 |
| 125* | 290 | 160 | 9,0 |
| 150 | 320 | 170 | 12,0 |
| 200 | 380 | 180 | 17,0 |
| 250 | 440 | 190 | 23,0 |
| 300 | 500 | 195 | 30,5 |
| 400* |  |  |  |
| 500* |  |  |  |

* Upon request. Note: not held in stock. Please order in good time!


## GKS JUNCTION GASKET

To connecto other pipe materials with
TYTON ${ }^{\text {ºp }}$-push-injoint DN 150


| Material in DN 150 | Dimensions [mm] |  |  | Weight [kg] ~ ductile iron body |
| :---: | :---: | :---: | :---: | :---: |
|  | Nominal size | OD min. | $\begin{aligned} & \text { OD } \\ & \text { max. } \end{aligned}$ |  |
| Ductile iron pipe without socket | 160 | 158 | 162 | GKS-gasket |
| Ductile iron pipe | 170 | 167,1 | 171 | TYTON ${ }^{\text {® }}$-gasket |
| PVC-pipe | 160 | 160 | 160,5 | GKS-gasket |
| PE-HD pipe | 160 | 160 | 161,5 | GKS-gasket |
| GRP-pipe | 168 | 168 | 168 | TYTON ${ }^{\text {® }}$-gasket |
| Ceramic pipe | 186 | 184 | 188 | GKS-gasket ceramic pipes connector Tecotect-se-gasket |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |

UEB JUNCTION COUPLING ML/PVC/PE
To connect other pipe materials with
TYTON ${ }^{\text {º push-injoint DN } 200 ~}$


CV-Verbindung
ML/PE-Rohr


| Material in DN 150 | Dimensions [mm] |  |  | Weight [kg] ~ ductile iron body |
| :---: | :---: | :---: | :---: | :---: |
|  | Nominal size | OD min. | $\begin{aligned} & \text { OD } \\ & \text { max. } \end{aligned}$ |  |
| Ductile iron pipe without socket | 210 | 208 | 212 | junction coupling ML-PVC-PE, CE-connection, TYTON ${ }^{\circledR}$-gasket |
| Ductile iron pipe | 222 | 219 | 223 | TYTON ${ }^{\text {® }}$-gasket |
| PVC-pipe | 200 | 200 | 200,6 | junction coupling ML-PVC-PE, O-Ring, TYTON ${ }^{\text {® }}$-gasket |
| PE-HD pipe | 200 | 200 | 201 | junction coupling ML-PVC-PE, O-Ring, TYTON ${ }^{\text {® }}$-gasket |
| GRP-pipe | 220,5 | 220,5 | 220,5 | TYTON*-gasket |
| Ceramic pipe |  |  |  | junction coupling ML-PVC-PE, CE-connection, TYTON**gasket, ceramic pipes connector, Tecotect-se-gasket |


$90^{\circ}$ saddles


| DN ${ }_{1}$ | DN ${ }_{2}$ | Dimensions [mm] |  | Weight [kg]~ |
| :---: | :---: | :---: | :---: | :---: |
|  |  | To fit spigot end of vitrified clay pipes | $\begin{gathered} \emptyset d_{3} \\ \text { of bore in pipe } \end{gathered}$ |  |
| 250-300 | 150 | 186 | 172 | 10,3 |
| 350 |  |  |  | 9,8 |
| 400-600 |  |  |  | 9,3 |
| 700-1200 |  |  |  | 8,5 |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |

SI 45

| DN ${ }_{1}$ | DN ${ }_{2}$ | Dimensions [mm] |  | Weight [kg] |
| :---: | :---: | :---: | :---: | :---: |
|  |  | ø $\mathrm{d}_{2}$ cast | $\emptyset d_{3}$ of bore in pipe |  |
| 250-300 | 150 | 170 | 172 | 14 |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |

### 9.3 Installation instructions

1. Installation instructions for cleanout fitting and cleanout cover

## a) Cleanout fitting



## b) Cleanout cover



## Step1

Stick on the template. Please ensure that the template and pipe axis are parallel.


## Step 2

Use a disc grinder with a stone or diamond disc to cut along the white mark on the template. The cutting should be done vertically to the pipe surface. The white markings are the external edges. A cut can be made 5 mm over the marking in the longitudinal direction to remove the cover easily.


Simply make the notches by grooving with the disc several times.
Be careful not to make the notches too big (the square box screws may spin).

## Step 3

After removing the cover and waste inside the pipe, please remove the remaining template on the pipe. The cut area should be deburred (with the disc grinder or a coarse file) and sealed with a repair kit. Please see chapter 8 (page 70) for more details.


## Step 4

Put lubricant on the gasket and place it on the pipe. Plug the square box screws completely from the inside and ensure that the screws are prevented from spinning.


## Sealing of cut areas of sewage pipes, KAS, KPS, SI and SM fittings

All cut areas have to be sealed immediately to guarantee perfect corrosion protection. Therefore, we provide a repair kit (zinc-spray and painting) approved for sewage systems. Before processing, please ensure that the surface is free of oils, fat, dust and oxides. The pipe/fitting can be used once the sealed area is dry.

2. Connecting sewage pipes with 2 U -pieces

TYTON ${ }^{\circledR}$ or VRS ${ }^{\circledR}$-T joint DN 80 - DN 500


| DN | Lmin |
| :---: | :---: |
| 80 | 127 |
| 100 | 135 |
| 125 | 143 |
| 150 | 150 |
| 200 | 160 |
| 250 | 165 |
| 300 | 170 |
| 400 | 190 |
| 500 | 200 |

Incline tolerances in mm (in accordance with ÖNORM B 2503):

| DN/ID | Horizontal divergence $a_{\text {hmo }}$$\qquad$ real pipeline axis to designed axis | ```Vertical divergence a}\mp@subsup{a}{\mathrm{ max }}{ real incline (level) to designed incline }\mp@subsup{t}{\mathrm{ soll:}}{``` |  |  | Tolerated height divergence | Tolerated horizontal height divergence at |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | < $5 \%$ | $\begin{gathered} 5 \% \\ - \\ 20 \% \end{gathered}$ | > 20 \% |  |  |
| <200 | 40 | 10 | 15 | 20 | 10 | 10 |
| 200-400 |  | 10 | 15 | 20 | 10 | 10 |
| 400-900 |  | 12 | 17 | 25 | 15 | 15 |
| >900 |  | 15 | 20 | 30 | 20 | 20 |

Increase and decrease 111 in regard to the designed incline $\mid$ soll should not be bigger than $\mid$ soll $:: 20 \% 5 \mathrm{~mm} / \mathrm{m}$, and |soll $>20 \% 10 \mathrm{~mm} / \mathrm{m}$.
For all level planks the maximum tolerated height divergence of the level at the
splice (in the flow direction) is +2 mm and -5 mm . Counter splices should be avoided.
3. Manhole connections
a) Manholes with open wash

## Manhole connector with Tyton ${ }^{\text {® }}$ joint:



Manhole connectors from TRM with the TYTON ${ }^{\circledR}$ push-in joint can be used for all prefabricated and in-situ concrete manholes. The connectors can be installed at the concrete plant, directly on the construction site or in the in-situ concrete manhole.

Manhole connector with positive locked VRS ${ }^{\oplus}-$ T-joint:


Manhole connectors with VRS ${ }^{\text {- }}$ T positive locked joint are used mainly on steep slopes to connect the manhole to the pipeline in a positively locked manner.

## b) Manholes with closed wash

## TRM cleanout fitting for wash-out manhole



Starting with DN400/500 MMA can be used as gate for camera testing also.

MMA fitting for use at washing manholes (with a positive locked joint or non positive locked joint). Changes in direction can be made outside of the manhole.

TRM cleanout cover for wash-out manhole


Cleanout covers for washing or service, also suitable for pressure pipelines. Changes in direction can be made outside of the manhole. Can be used as a gate for camera testing.
4. Pipes through walls

6. Bridge lines


1. Discharge nozzles of ductile iron drains can be directly connected with ML-connectors. We recommend using CE-connectors made of CR-NI-steel. CV-connectors should not be used because of the aggressive environmental influences.
2. To install the pipeline on the bridge, different pipe clamps made of stainless or galvanized steel are available
3. Dewatering pipelines should have DN 50 minimum.

## 7. Compesation of elongation

Elongation caused by warping at the thrust blocks, pillars or installation on different floors can be compensated (arrangement can also be used for horizontal pipeline routes):


## 8. Pressure testing

Newly installed pipelines have to be pressure tested to verify the leak tightness of all pipes and fittings and to verify that the pipeline is safely positioned. Pressure testing for sewage systems should be performed in accordance with EN 805 and EN 1610

## Contact

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[^0]:    ${ }^{11}$ ) Tolerances are possible, ${ }^{2)}$ PFA: allowable operating pressure; PMA $=1.2 \times$ PFA; PEA $=1.2 \times$ PFA +5 - higher PFA's on enquiry, ${ }^{3)}$ Plus high-pressure lock if required with DN 80 to DN 250 sizes; ${ }^{4)}$ Higher tractive forces on enquiry,
    ${ }^{5)}$ Min. radius of curves ( $5 \mathrm{mpipe} / 6 \mathrm{mpipe}$ ), which results from the angular deflection possible at the sockets - applies to both open trench and trenchless laying, ${ }^{6}$ Approx. assembly time of the joint not including any protection it may be given

[^1]:    ${ }^{1)}$ Tolerances are possible. ${ }^{2)}$ PFA: allowable operating pressure; PMA $=1.2 \times$ PFA; PEA $=1.2 \times$ PFA $+5-$ higher PFA's on enquiry. ${ }^{3)}$ Higher tractive forces on enquiry
    ${ }^{4}$ ) Min. radius of curves, which results from the angular deflection possible at the sockets - applies to both open trench and trenchless laying.
    ${ }^{5)}$ Approx. assembly time of the joint. not including any protection it may be given, ${ }^{6}$ ) Wall-thickness class K 10 under EN 545:2006

[^2]:    ${ }^{1}$ PFA: allowable operating pressure; $\mathrm{PMA}=1.2 \times$ PFA; PEA $=1.2 \times P F A+5-$ higher PFA's on enquiry, ${ }^{2}$ Theoretical weight per m pipe incl. cement mortar lining, zinc (zinc-aluminium) and epoxy finishing layer, ${ }^{33}$ Theoretical weight per $m$ pipe incl. cement mortar lining \& coating and zinc, ${ }^{4} \mathrm{~s}_{1}=\mathrm{min}$. dimension, $\mathrm{s}_{2} / \mathrm{s}_{3}=$ nominal dimensions. Tolerances are possible

[^3]:    * To manufacturer's standard

[^4]:    $L_{u}=$ laying length in the locked state
    $z=$ mean laying length (when used without a welded bead)

    * Take note of the PFA of the VRS ${ }^{\text {º }}$-T joint

[^5]:    * Take note of the PFA of the VRS*-T joint

[^6]:    ${ }^{1)}$ Standard value; *smaller $D$ upon request

[^7]:    ${ }^{1)}$ Not including screw ring and bolted gland ring of the respective joints

[^8]:    ${ }^{11}$ To manufacturer's standard; ${ }^{22}$ Screwed socket joint; weight not including screw ring

[^9]:    bolted gland ring respectively

[^10]:    ${ }^{1}$ Maßenach EN 1092-1

[^11]:    ${ }^{1)}$ Sleeves are supplied already cut to the specified length and fitted with a sealing strip.
    Tape material in the form of 30 m rolls is available on enquiry for DN 250 to DN 1000 size

[^12]:    Total weight; other nominal sizes, insulating layers of other thicknesses and trace heating are

[^13]:    Other nominal sizes, insulating layers of other thicknesses and trace heating are available on
    enquiry. Other types of fitting have to be insulated by the installer.

[^14]:    * Upon request

